Progress in Direct-Drive Inertial Confinement Fusion Research



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Summary

These are exciting times for inertial confinement fusion

- Experiments on Nova (previously) and OMEGA are developing the target-physics understanding.
- Recent OMEGA experiments have demonstrated ignition-relevant areal densities.
- New concepts will extend ignition possibilities.
- This talk will review direct-drive ICF progress.*
- After 35 years, the ICF community is ready to exploit advances in physics understanding and drivers, leading to ignition experiments on the National Ignition Facility (NIF).



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Ablation is used to generate the extreme pressures required to compress a fusion capsule to ignition conditions



10 keV and the core fuel areal density to exceed ~300 mg/cm².

A "Lawson's criterion" in terms of burn-averaged ρR and T_i shows the requirements for ignition

 Simple scaling relations for ignition condition from Zhou et al.* and Herrmann et al.**

$$\langle \rho R \rangle_n > 1.3 \left(\frac{4}{\langle T_i \rangle_n (\text{keV})} \right)^{2.4} \left(\text{g/cm}^2 \right)$$

- Fitting the results of 1-D simulations with Gain = 1 yields an ignition condition that depends on the burn-averaged *ρR* and ion temperature without alpha deposition.
- For sub-ignited implosions $T_{i(no-\alpha)} \cong T_i$

LILAC fit



Both T_i and ρR can be measured experimentally.

- R. Betti and C. Zhou (CO5.00001).
- * C. Zhou and R. Betti, Phys. Plasmas <u>14</u>, 072703 (2007).
- ** M. C.Herrmann, M. Tabak, and J. D. Lindl, Nucl. Fusion <u>41</u>, 99 (2001).

The fundamental physics of direct- and indirect-drive **ICF** implosions is the same



E64260

The 1.8-MJ National Ignition Facility (NIF) will demonstrate ICF ignition and modest energy gain



OMEGA experiments are integral to an ignition demonstration on the NIF.

The NIF is on track for completion in FY09





The OMEGA laser is designed to achieve high irradiation uniformity with flexible pulse-shaping capability



Laser-beam smoothing is critical to ICF ignition

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Ignition requires smooth cryogenic DT targets

• Thick (>50 μ m) DT ice layers are required for ignition.

• β -layered 50:50 DT cryogenic targets have measured ice-roughness nonuniformities <1- μ m rms, meeting ignition specifications.



Multiple views are essential for full characterization.

D. R. Harding (YO5.00001).

D. R. Harding, to be published in *IFSA* 2007.

About 80% of the DT capsules created to date have produced layers with sub-1- μ m rms roughness



- High-mode (l > 20) roughness is minimal for "single-crystal" layers
- Low-mode roughness (l < 6) is due to asymmetries in the triple-point isotherm
- Mid-mode roughness (6 < l < 20) is likely related to outer-surface features (glue for silks)
- The best layers are achieved at the triple point

DT layer quality meets ignition requirements.

LLE has learned how to reliably field cryogenic capsules



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Improvements in the ice-layer quality and target position have proceeded in parallel with implosion experiments.

The fuel areal density and hot-spot ion temperature determine ignition performance

- Areal density (ho R)
 - shock timing and strength

- preheat
- compressibility
- hydrodynamic instabilities
- Ion temperature (T_i)
 - implosion velocity
 - hydrodynamic instabilities
 - absorption/drive coupling

Our strategy is to first increase ρR and then T_i

The laser power is tailored to drive the target on a low fuel adiabat, including adiabat shaping*



- High outer α reduces the RTI growth rates through higher ablation velocity $\gamma_{\text{RTI}} = 0.9 \sqrt{\text{kg}} - 3 \text{kV}_a^{\dagger}$ $k = 2\pi/\lambda$ $V_a \sim \alpha_{\text{out}}^{0.6}$
- High $\langle \alpha \rangle$ increases the shell thickness and reduces feedthrough, $\Delta \sim \langle \alpha \rangle^{0.6}$
- Low inner α reduces the shell kinetic energy required for ignition, $E_{iqn} \sim \alpha_{in}^{1.8^{\ddagger}}$

ICF ignition targets have α_{in} ~ 1 to 3, α_{out} ~ 3 to 6, and α_{avg} ~ 2 to 3.

*V. N. Goncharov *et al.*, Phys. Plasmas <u>10</u>, 1906 (2003). [†]H. Takabe *et al.*, Phys. Fluids <u>28</u>, 3676 (1985). [‡]W. K. Levedahl and J. D. Lindl, Nucl. Fusion <u>37</u>, 165 (1997).

The shock and isentropic compression must be precisely timed to reach the areal density required for ignition

- Accurate shock and compression wave timing sets the proper $\alpha_{\rm in}, \rho {\it R} \sim \alpha_{\rm in}^{-0.6}$



V. N. Goncharov (GI1.00001).

A nonlocal model is required to correctly predict electron thermal transport



• A more accurate model based on the solution of the Fokker–Planck equation predicts a time-dependent flux limiter.

Accurate modeling of electron thermal transport is crucial for shock timing and setting the shell adiabat



The fuel areal density and hot-spot ion temperature determine the compression performance of ICF targets

- Precise pulse shaping, including a picket, sets the target on the appropriate adiabat
- Current experiments have demonstrated ignition-relevant areal densities
 - shock timing and strength
 - preheat
 - compressibility
 - hydrodynamic instabilities
- Future experiments will increase the ion temperature
 - implosion velocity
 - hydrodynamic instabilities
 - absorption/drive coupling

Understanding cryogenic dynamics is a key to successful ICF ignition.

Implosions demonstrate compression of cryogenic fuel to ignition-relevant areal densities

- Cryogenic targets are energy scaled from NIF ignition designs
- Target designs are being refined based upon these experiments



• A systematic experimental scan of fuel adiabat and drive intensities has been conducted

$$\label{eq:rescaled_states} \begin{split} \rho R & \left\{ \begin{array}{l} 2 < \alpha < 10; \, \alpha = \text{fuel pressure/Fermi-degenerate pressure} \\ I_L = 0.25 \text{ to } 1.5 \times 10^{15} \, \text{W/cm}^2 \\ I_L = 0.25 \text{ to } 1.5 \times 10^{15} \, \text{W/cm}^2 \\ \end{array} \right. \\ \left\{ \begin{array}{l} V_{\text{imp}} = 2.5 \text{ to } 4.0 \times 10^7 \, \text{cm/s} \\ \text{In-flight aspect ratio: 30 to 50} \\ \text{Number of perturbation e-folds ~5 to 7} \end{array} \right. \end{split}$$

Areal Density

Downshifted secondary proton spectra measure* the compressed fuel areal density



*F. H. Séguin et al., Rev. Sci. Instrum. <u>74</u>, 975 (2003).

Areal Density

A severe degradation of ρR , up to 40% of 1-D predictions, was observed in <u>high-intensity</u> mid- and low-adiabat cryogenic implosions on OMEGA



The nonlocal thermal-transport model improves the agreement between 1-D simulation and experimental areal densities



• The measured areal densities remain somewhat lower than 1-D simulations with nonlocal heat conduction.

The remaining discrepancies between measured and simulated areal density may be due to hot-electron preheat

- There are two plausible explanations for the reduction of the experimental areal density relative to the 1-D simulations
 - preheat by hot electrons generated by the two-plasmon-decay instability (discussed next)
 - measured nuclear burn histories can be different from 1-D simulations due to hydrodynamic instabilities*
 - protons may sample lower areal densities
 - a similar effect has been seen in warm plastic-target implosions
 - statistics need to be improved to measure this in cryogenic implosions

Hot-electron preheat generated by laser–plasma interactions can significantly degrade the final areal density



- Low- α designs $T_0 \sim 20 \text{ eV}$
- 20% ρR reduction for $\Delta T_{shell} \sim$ 6 eV
- For OMEGA experiments, *E*_{preheat} ~ 10 to 20 J (~0.1% of laser energy)

$3/2\omega$ light and hard x rays* indicate the presence of the two-plasmon-decay instability



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Preheating by hot electrons from the two-plasmon-decay instability is a candidate for additional cryo ρR degradation



• Measured $T_{hot} > 50 \text{ keV} - \text{electron range is greater than the D}_2$ thickness

*C. Stoeckl et al. Phys. Rev. Lett. 90, 235002 (2003).

**A. Simon et al., Phys. Fluids 26, 3107 (1983).

^{*}B. Yaakobi et al., Phys. Plasmas <u>12</u>, 062703 (2005).

The two-plasmon-decay threshold is exceeded when the laser burns into the D_2 fuel

- $I_{14}L_{\mu m}$ Above-threshold parameter^{*} for 2 ω_p instability $\eta =$ 230 T_{keV}
- Instability develops when $\eta > 1$



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An improved agreement between simulated and measured ρR is observed for low intensity implosions*

250 • Peak $I < 3 \times 10^{14} \, \text{W/cm}^2$ ■ *I* ~ 10¹⁵ W/cm² 200 $ho R_{
m exp}~(
m mg/cm^2)$ 150 100 50 0 50 100 150 200 250 0 $\rho R_{1-D} (mg/cm^2)$

All simulations use nonlocal thermal-transport model

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^{*}V. A. Smalyuk *et al.*, Anomalous Absorption (2007); and to be published in Phys. Rev. Lett. D. Shvarts *et al.*, Anomalous Absorption and IFSA (2007).

Hard x rays due to energetic electrons from the two-plasmondecay instability increases rapidly with laser intensity

 Hard x-ray signals produced by bremsstrahlung radiation from fast electrons may indicate preheating*



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Hard x rays from energetic electrons are reduced by increasing the CD thickness. **Areal Density**

Ignition-relevant areal densities (~200 mg/cm²) are achieved by accurate shock timing and mitigating fast-electron preheat

• Target design tuned to be insensitive to the thermal transport model and has low hard x-ray signal.



10-μm CD cryogenic implosion proton spectrum X-ray pinhole camera



 D_2 fuel density reaches ~100 g/cc (500× liquid density)

These are, by far, the highest areal densities measured in ignition-relevant laboratory implosions—very important for direct- and indirect-drive ignition.

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Areal Density

Predictive capability for the shock timing is validated by adjusting picket timing



V. N. Goncharov (GI1.00001).

Good agreement between simulated and measured ρR is observed for implosions with low hard x-ray signals



All simulations use nonlocal thermal-transport model

Areal Density

2-D DRACO simulations of cryogenic high- ρR shots confirm experimentally observed areal densities



• Target offset from target chamber center by 20 μ m

 Observed yield is one third of 2-D prediction

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Path to T_i

Direct-drive research is on a path to ignition on the NIF

- Ignition-relevant areal densities have been achieved





Path to T_i

Future experiments will increase the ion temperature while mitigating preheat and hydro-instabilities

- T_i increases with implosion velocity, $T_i \sim V_{imp}^{1.3}$
- Increase the implosion velocity to $4\times 10^7~\text{cm/s}$
 - thinner ice layer (60- μ m D₂)
 - higher intensity
 - re-time shock waves with the nonlocal model
- Doped ablators (Si and Ge) can minimize energetic electron preheat and Rayleigh–Taylor growth rate



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Path to T_i

Initial experiments with high-Z doped plastic shells show reduced hard x-ray production



High-Z dopants reduce hot-electron generation

• High-Z dopants reduce Rayleigh–Taylor growth rates*

Polar Drive

Direct drive can achieve ignition conditions while NIF is in the x-ray-drive configuration



The polar-drive point design achieves a yield of 17 MJ with all current levels of NIF nonuniformities included in the calculation



New ignition concepts separate compression (ρR) and heating (T_i)—two-step ignition

- In the current hot-spot ignition, the driver provides both compression (ρR) and heating (T_i).
- Both fast ignition and shock ignition use a second drive to provide heating (T_i) .



• Measured cryogenic target areal densities are relevant to these schemes.

Two-step ignition offers lower driver energies with the possibility of higher gain.

Fast and shock ignition can trigger ignition in massive (slow) targets leading to high gains



Launching a spherically convergent shock wave at the end of the laser pulse can trigger ignition at lower driver energies

 Low-velocity implosions can be shock-ignited to yield moderately high gains (~50 to 70) at relatively low UV driver energies (~400 to 500 kJ).

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- 2-D simulations indicate that shock ignition survives the detrimental effects of laser imprinting for UV driver energies in the 500-kJ range.
- Implosion experiments on thick CH shells filled with 4- to 25-atm D₂ show that pulse shapes with shock spikes give higher neutron yields and higher areal densities than standard pulse shapes.



Shock-ignition pulse shapes lead to higher compression and more favorable ignition conditions



TC7868a

Initial shock-ignition research on OMEGA is encouraging



W. Theobald (GI1.00002).

Plastic-shell implosions with a shock-ignition pulse shape show larger yield and higher compressibility



- YOC is the measured yield divided by the 1-D predicted yield.
- Hot-spot convergence ratio: ratio of the original target radius to the compressed hot-spot radius.

High-energy petawatt lasers will extend ignition capabilities



*D. D. Meyerhofer (TO6.00001). [†]M. Key, ECLIM (2006).

Summary/Conclusions

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- Recent OMEGA experiments have demonstrated ignition-relevant areal densities.
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The achievement of ICF ignition will change the fusion landscape.