

**Current Drive and Heating
on ARIES-RS/AT, and FIRE-AT**

T.K. Mau

University of California, San Diego

(With Input from C. Kessel)

Heating and Current Drive Breakout Session

Burning Plasma Workshop II

May 1-3, 2001

General Atomics

OUTLINE

- ARIES-RS and ARIES-AT H&CD Scenarios
 - RF system requirements
 - Choice of wave launchers
- RFCD assessment for FIRE AT modes, based on ARIES experience:
 - without wall stabilization, moderate beta normal
 - with wall stabilization, high beta normal
- Issues and Conclusions

Heating and Current Drive Analysis Objectives for ARIES

- Determine and understand **current drive power** requirement, a critical element in systems analysis for the power plant economics.
- Select most **viable current drive schemes** for maintaining high performance, MHD-stable plasma equilibria, according to:
 1. **Core accessibility**
 2. **Current drive efficiency**
 3. **Profile control capability**
 4. **Experimental data base and physics understanding**
 5. **Power generation efficiency**
 6. **Dual capability of current drive and auxiliary plasma heating**
 7. **Core compatibility of in-vessel components.**
- Determine current drive source and power launcher requirements, e.g., **frequency and spectrum for RF launchers,**
beam energy and injection angle for NBI systems,
and select launcher configuration compatible with fusion core.
- Identify (and resolve) issues and areas for further research.

Physics Models Used in RF Heating and Current Drive Analysis for ARIES

Main analysis tool is the **CURRAY** ray tracing code (developed with GA), with state-of-the-art features:

- **Wave absorption physics:**
 - Cold ion ($k_x \rho_i \ll 1$), warm electron dispersion relation
 - Thermal ion and electron effects in field polarization terms when calculating linear damping decrement along rays
 - **Energetic ion species (e.g., alphas) are treated either as hot Maxwellian or having slowing down distribution**
 - Calculates absorption profiles, due to cyclotron resonance, Landau and TTMP processes, for all species
- **Current drive physics:**
 - Calculates local driven electron currents
 - **Developed normalized j/p efficiency formulas** due to Ehst-Karney and Chiu-Mau (relativistic correction)
 - Self-driven current [= bootstrap + diamagnetic + Pfirsch-Schluter] is calculated for multiple ion species for all collisional regimes on exact equilibrium and self-consistent (p, n, T) profiles.
 - Developed algorithm to maximize alignment of driven to equilibrium j-profile
- Coupled to high-precision equilibrium geometry (JSOLVER)

Current Drive Scenarios for ARIES-RS/AT 1-GWe Power Plants

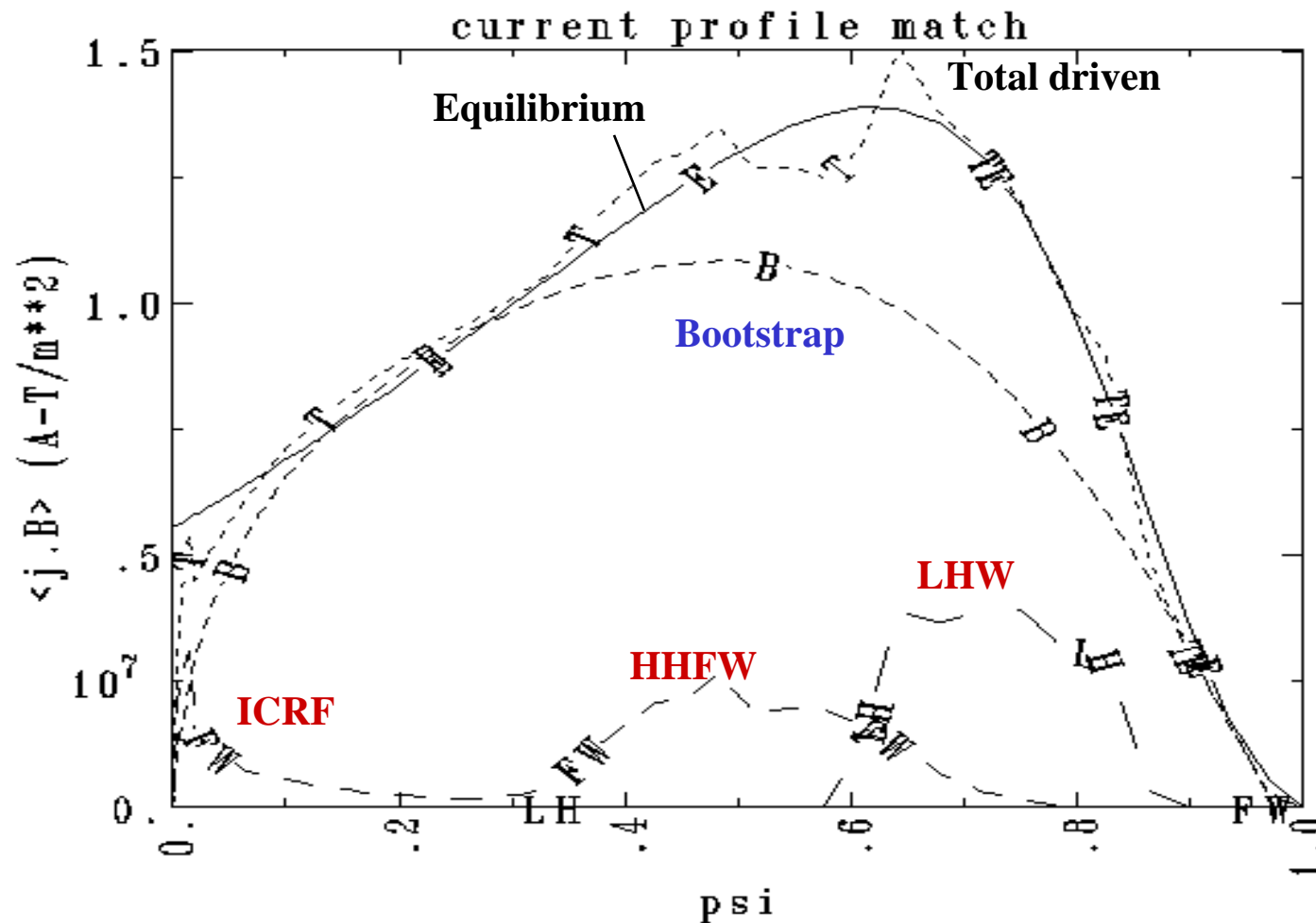
ARIES-AT requires much less current drive power than ARIES-RS because of much better bootstrap alignment.

Device	ARIES-RS	ARIES-AT
R (m)	5.5	5.2
A	4.0	4.0
	1.89	2.18
	0.77	0.84
I_p (MA)	11.3	12.8
(%)	5.0	9.2
I_{bs} / I_p	0.88	0.915
On-axis CD*	ICRF/FW	ICRF/FW
Off-axis CD*	HHFW,LHW	LHW
Power (MW)	82.0	41.6

* ECCD can be localized at all radii, but was not used here due to low current drive and source efficiencies.

Current Drive Scenario for ARIES-RS

- **3 RF schemes** are required to drive the seed currents on ARIES-RS:
 - (1) **ICRF fast waves** for on-axis drive: 23.2 MW @ 98 MHz
 - (2) **LH waves** for off-axis drive: 47.1 MW @ 3.5 - 4.6 GHz
 - (3) **HHFW** ($\sim 20 f_{cD}$) for mid-radius drive: 37.6 MW @ 1 GHz



ICRF Fast Wave Drives On-axis Seed Current

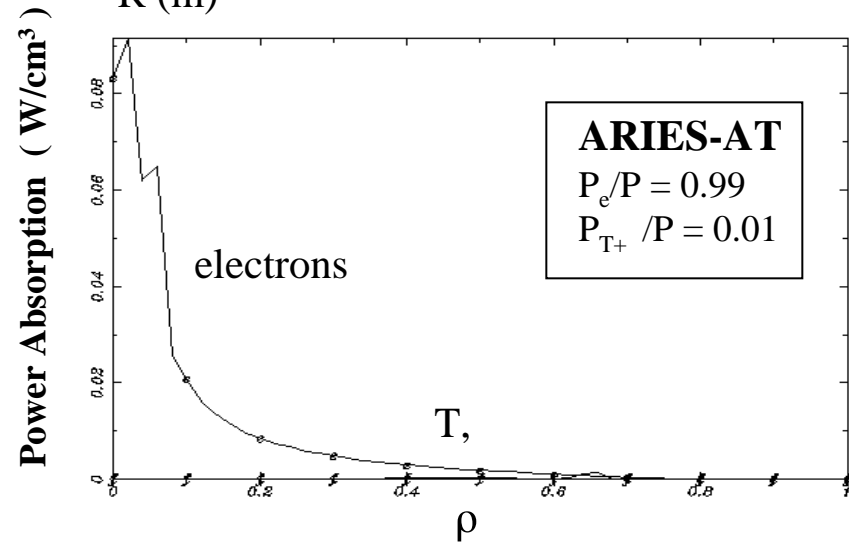
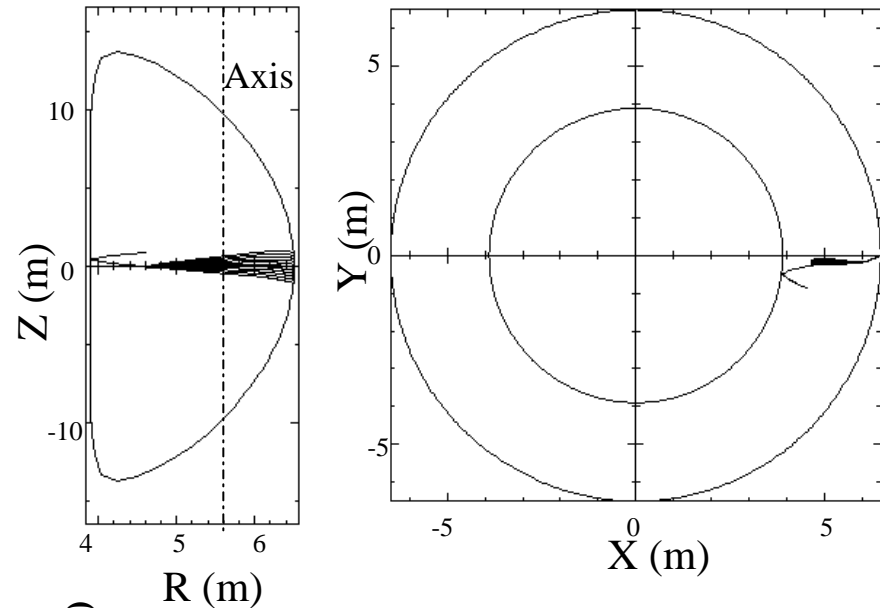
- Wave frequency is chosen to place $4f_{cT}$ resonance at $R > R_o + a$, and $2f_{cD}$ resonance at $R \ll R_{axis}$, to minimize ion and a absorption.
- Launcher is located on outboard midplane with $N_{||} = 2$ spectrum for best current profile alignment.
- Plasma & wave parameters :

$$T_{eo} = 29 \text{ keV}, n_{eo,20} = 2.95,$$

$$Z_{eff} = 1.8$$

$$f = 96 \text{ MHz}, N_{||} = -2.0.$$

$$P_{cd} = 4.7 \text{ MW}$$

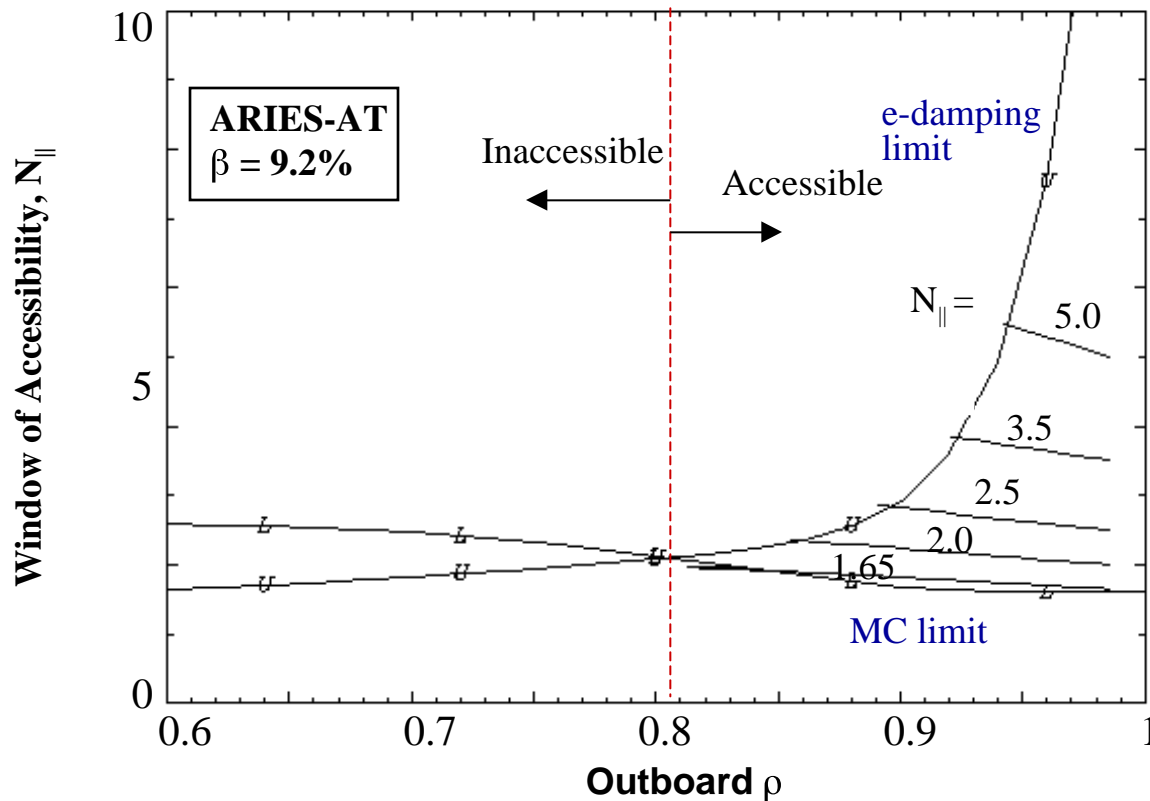


LH Wave Penetration is an Issue in High- β Plasmas

- Frequency = 3.6 GHz [$> 2 \times f_{LH} (r=0.8)$]
 - Less than 1% absorption, even though $f=9.3$ GHz to eliminate a-damping.
- There is a window in N_{\parallel} for accessibility to the core:

$$[1 + (f_{pe}/f_{ce})^2]^{1/2} + f_{pe}/f_{ce} < N_{\parallel} < 7.0/T_e^{1/2} \text{ (keV)}$$
- Penetration is limited to $\rho > 0.8$ for the high- β AT equilibrium. [$\beta \sim (f_{pe}/f_{ce})^2$]

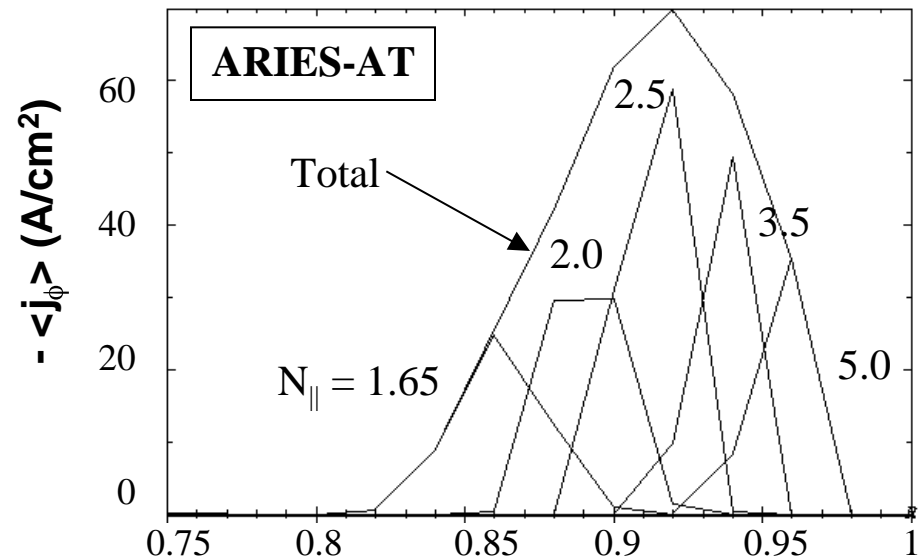
Low N_{\parallel} rays encounter mode conversion to fast wave at $r > 0.8$;
 higher N_{\parallel} rays get totally damped before reaching $\rho = 0.8$.



Off-Axis Current Drive Requires Tailored LH Power Spectrum

- Five waveguide modules, each launching a different N_{\parallel} spectrum, are used to drive the required off-axis seed current profile. These are located about 90° ($\sim 2\text{m.}$) below the outboard midplane.
- Extended physics model found absorption to be negligible for off-axis drive at > 0.8 . Frequency can be lowered for high N_{\parallel} launch at outer plasma region, thus easing design of waveguide launcher.
- The tailored LH spectrum has following parameters:

$\underline{f}(\text{GHz})$	$\underline{N}_{\parallel}$	$\underline{P}(\text{MW})$	$\underline{I}_{\text{cd}}/\underline{I}_{\text{sd}}$
3.6	1.65	3.06	0.15
3.6	2.0	4.40	0.20
3.6	2.5	8.22	0.30
3.6	3.5	8.87	0.20
2.5	5.0	12.39	0.15



ARIES and FIRE have Different Design Features

ARIES

- **Single mode of operation**
- **RF power exclusively for CD**
- **Large size and high β**
→ **strong single-pass damping**
- **Incorporate innovative concepts for launchers**
- **Minimal launcher port size**

FIRE

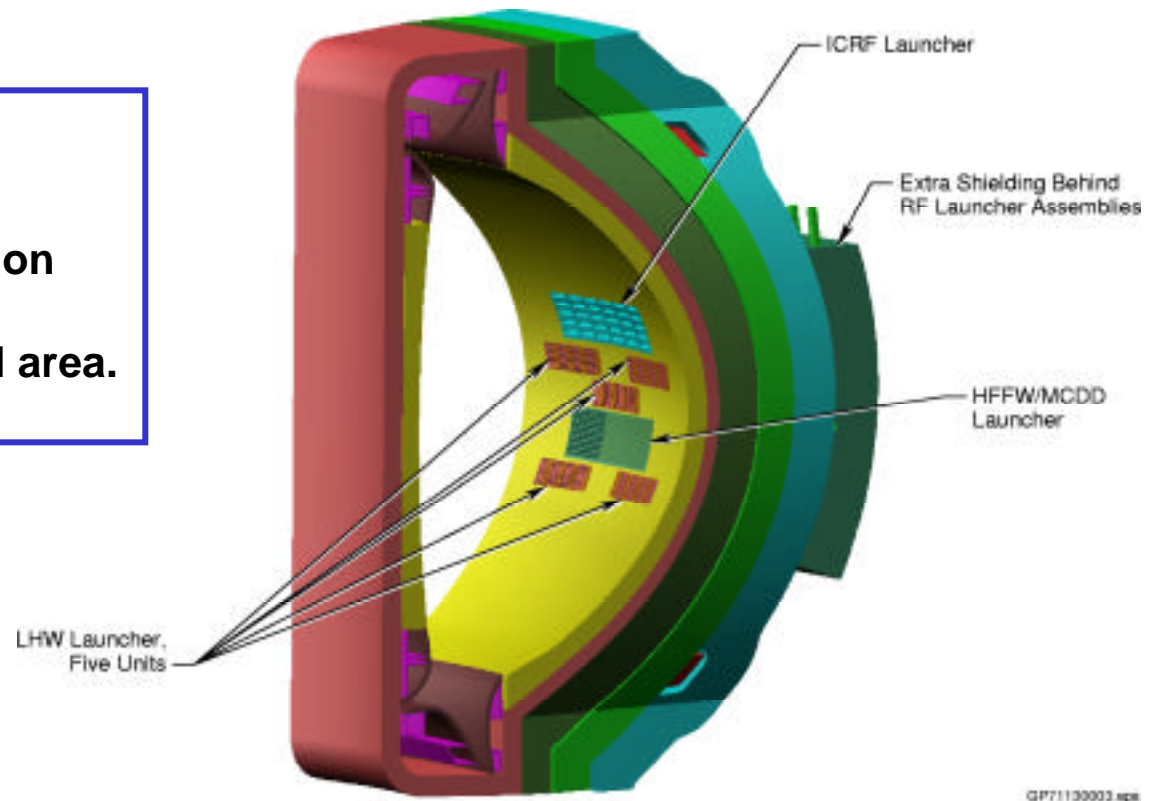
- **Multiple Modes (Elmy-H, AT with and w/o wall stabilization, D and DT)**
- **RF power heat ions and drive current at same time; depends on operating mode**
- **smaller size and lower β**
→ **weaker single-pass damping**
- **Use conventional launchers**
- **Port size not crucial consideration**

ALL RF Launchers Fit in One Blanket Sector on ARIES

- To minimize intrusion in power core requires RF launchers with high power density (MW/m^2) capabilities.
 - ICRF/FW : **Folded waveguide [ORNL]**
 - LHW : **Active/passive waveguide grille [ITER-EDA]**

In ARIES-RS:

Total first-wall penetration
= 2.53 m^2
= 0.6% of wall area.



Implications for FIRE: Use loop antennas for ICRF/FW, as port size is not a crucial consideration.

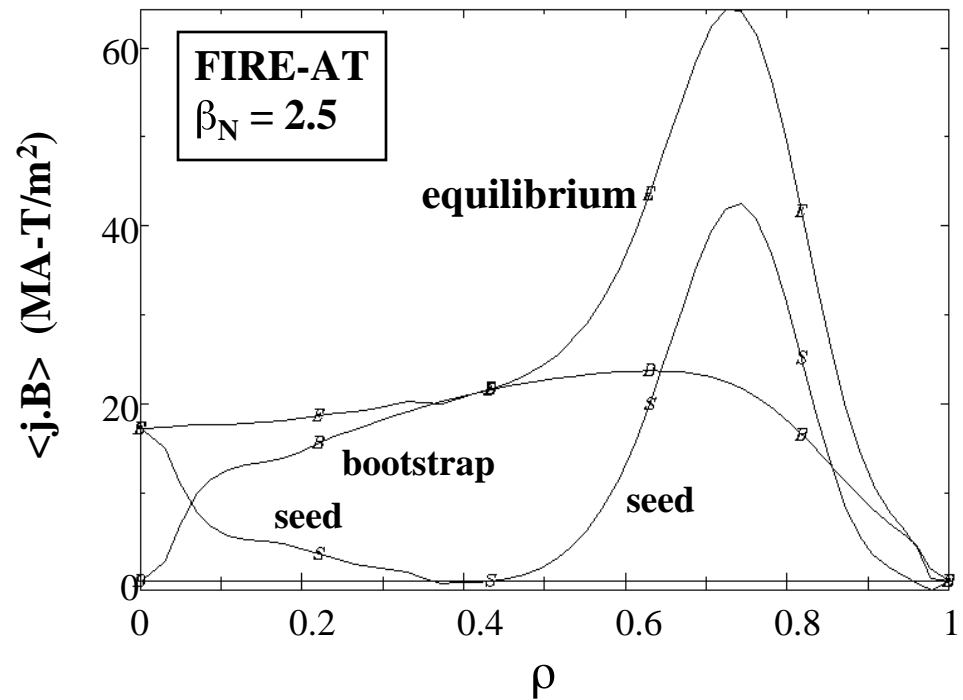
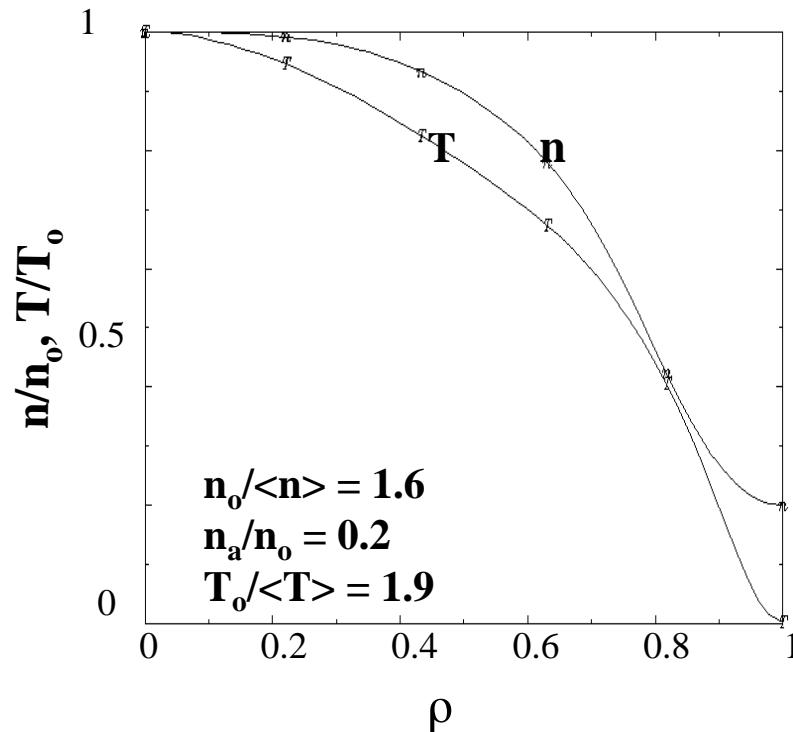
CD Requirements are Substantial for FIRE-AT w/o Wall Stabilization

- Based on a FIRE-AT mode equilibrium (from Kessel), amount of **current to be driven is 2.29 MA**, for the following parameters:

$R = 2 \text{ m}$, $a = 0.52 \text{ m}$, $B_0 = 8.5 \text{ T}$, $I_p = 5.34 \text{ MA}$,

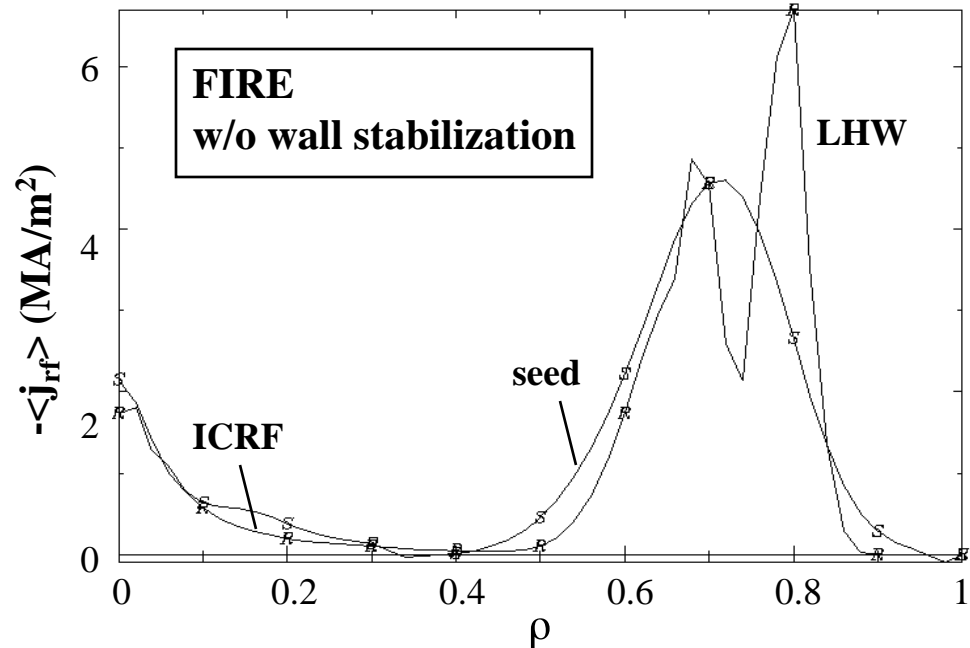
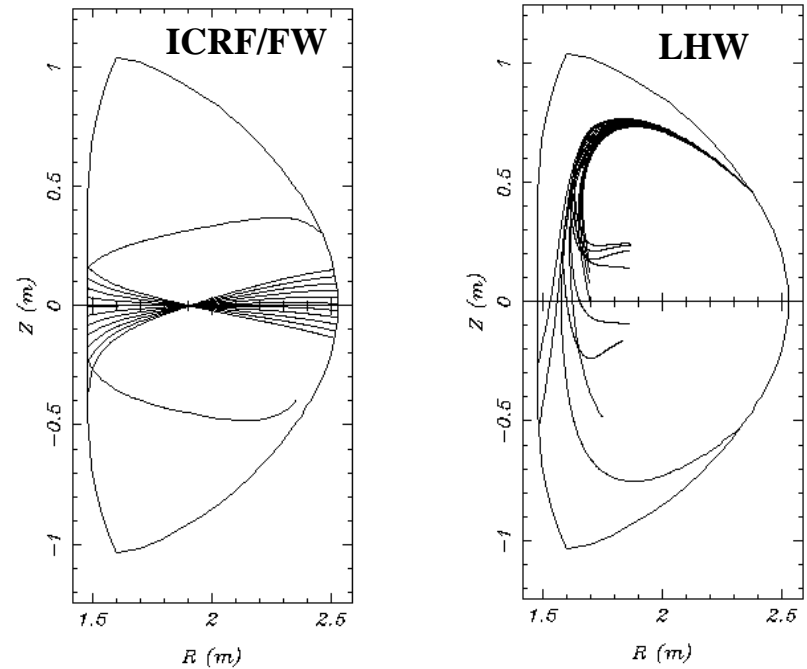
$T_{e0} = 19.9 \text{ keV}$, $n_{e0} = 3.34 \times 10^{14} \text{ cm}^{-3}$, $Z_{\text{eff}} = 1.41$ (1.3% Be, 17.2% He)
 $= 2.98\%$, $\beta_N = 2.54$ (w/o wall stabilization of kink), $I_{\text{BS}}/I_p = 0.57$

High edge density : $n_e(a) / n_{e0} = 0.2$



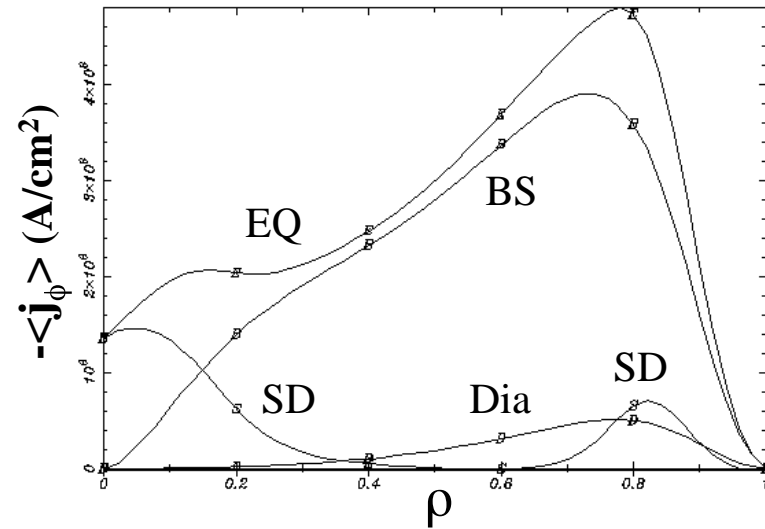
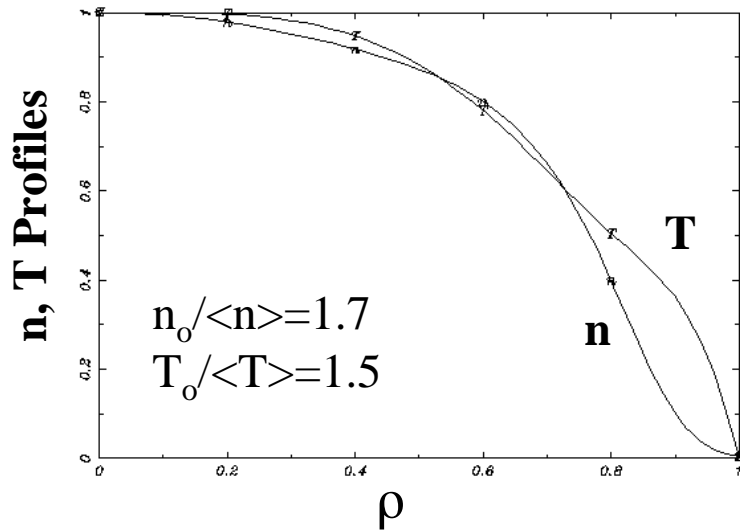
CD Power Requirement is Substantial

- **On-axis CD:**
 ICRF/FW @ 3.6 MW
 100 MHz, $N_{||} = 2$
 $P_{Be}/P = 0.23$, $P_T/P = 0.16$
- **Off-axis CD:**
 LHW @ 17.7 MW, $P_{\alpha}/p = 0.03$
 4.6 MHz
 $N_{||0} = 1.85$
 $\Delta N_{||} = 0.3$
 Launched from 60°
 above midplane*
 - * Above midplane launch is required for deeper penetration.
- Reasonable alignment with seed current profile is obtained.
 - Total Power ~ 21 MW
 - Efficiency is $\gamma_{cd} \sim 0.44$.



CD Power Assessment for FIRE High- β_N AT Mode

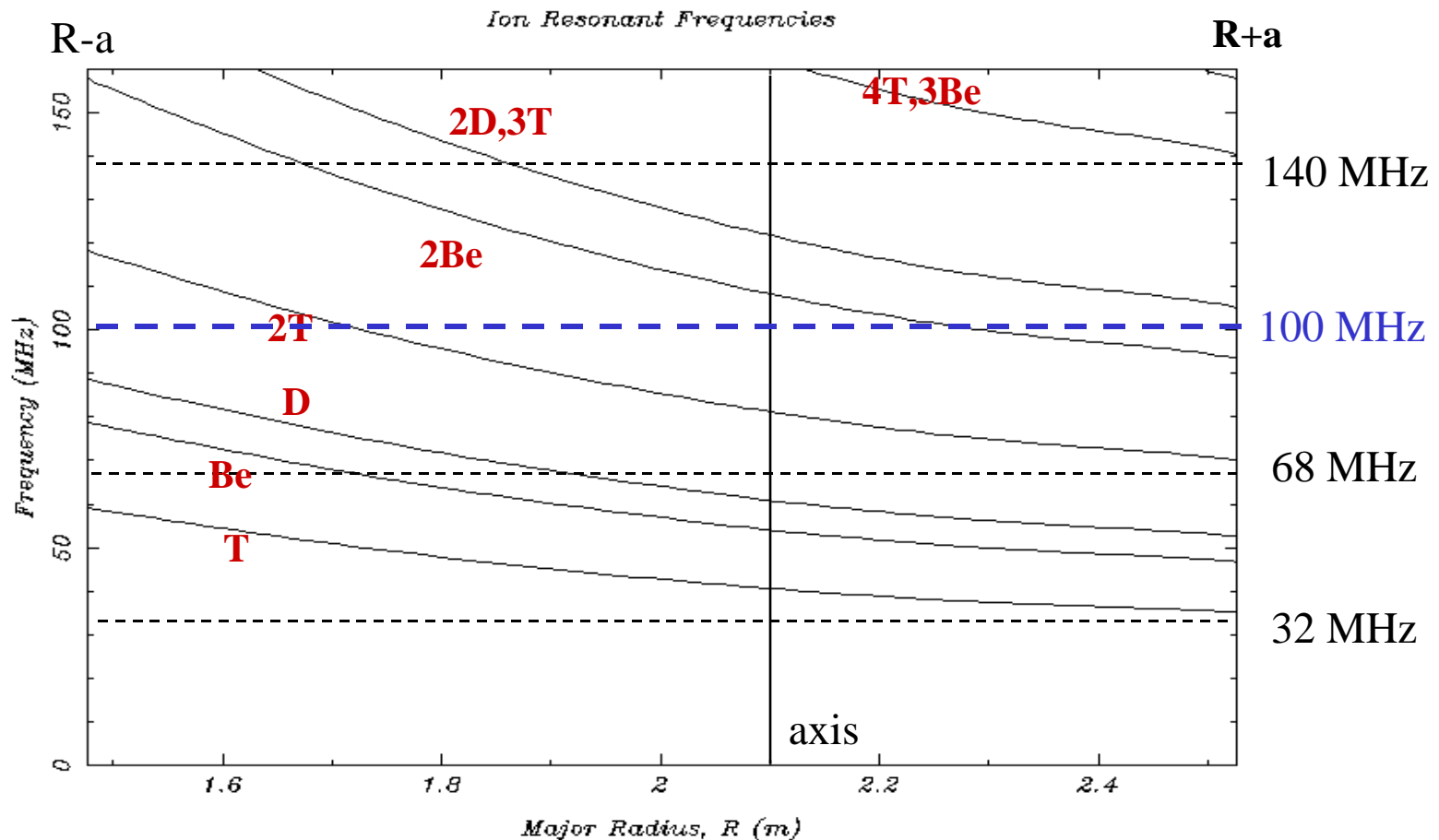
- Based on a FIRE DT-burning AT mode equilibrium (from Kessel):
 $R = 2$ m, $a = 0.52$ m, $B_o = 6.75$ T, $I_p = 4.50$ MA,
 $T_{eo} = 13.9$ keV, $n_{eo} = 5.10 \times 10^{14}$ cm $^{-3}$, $n_{ea}/n_{eo} \sim 0$, $Z_{eff} = 1.38$,
 $= 5.62\%$, $\beta_N = 4.38$ (with wall stabilization of kink)
 $I_{BS}/I_p = 0.93$, $I_{seed} = 0.35$ MA



- Using ICRF to drive on-axis seed (0.1 MA), and LHW to drive off-axis seed (0.25 MA), **total CD power can be as low as 7.3 MW !!**
 -The CD power will rise as edge density is raised.

Frequency Windows for Fast Wave Heating and CD

- In the ICRF, fast wave power is absorbed by both electrons and ions (D, T, H, Be, α), because of weak single-pass absorption, and 1-3% Beryllium present.
 - Partition of power among electron and ion species varies with frequency and N_{\parallel} .
- Antennas used for both H & CD should be designed for a finite frequency range of operation, which should be carefully determined.



CD and Profile Control Issues for FIRE AT Modes

- Realistic edge n, T profiles are required to accurately assess LH off-axis CD power. Linear results should be benchmarked with QL analysis.
- Species heating and current profile control while accessing flattop AT modes is critical, and modeling in conjunction with transport codes will be useful.
- The effect of beryllium impurity (1-3%) should be taken into account when assessing ICRF fast wave H & CD.
- For LH off-axis CD, interaction with energetic alphas should be studied in more detail.

Conclusions and Discussions

- RFCD power was assessed for example FIRE-AT equilibria both with and without wall stabilization.
 - For $N = 2.5$ case, $P_{cd} \sim 20$ MW.
 - For $N = 4.4$ case, $P_{cd} > 7$ MW depending on edge conditions.
- It appears that ICRF/FW and LHW are adequate for sustaining the target equilibria. The required power is dominantly LH.
- Antennas used for both heating and CD should be designed for for operating in a chosen range of frequencies.
- Current profile control during transients for AT flattop is critical and should be investigated and modeled.
- More experimental data base on Alcator C-Mod that involves access to AT mode with LHW will be useful.