Implications of Li divertor and other liquid-metal technologies

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Outline of Talk

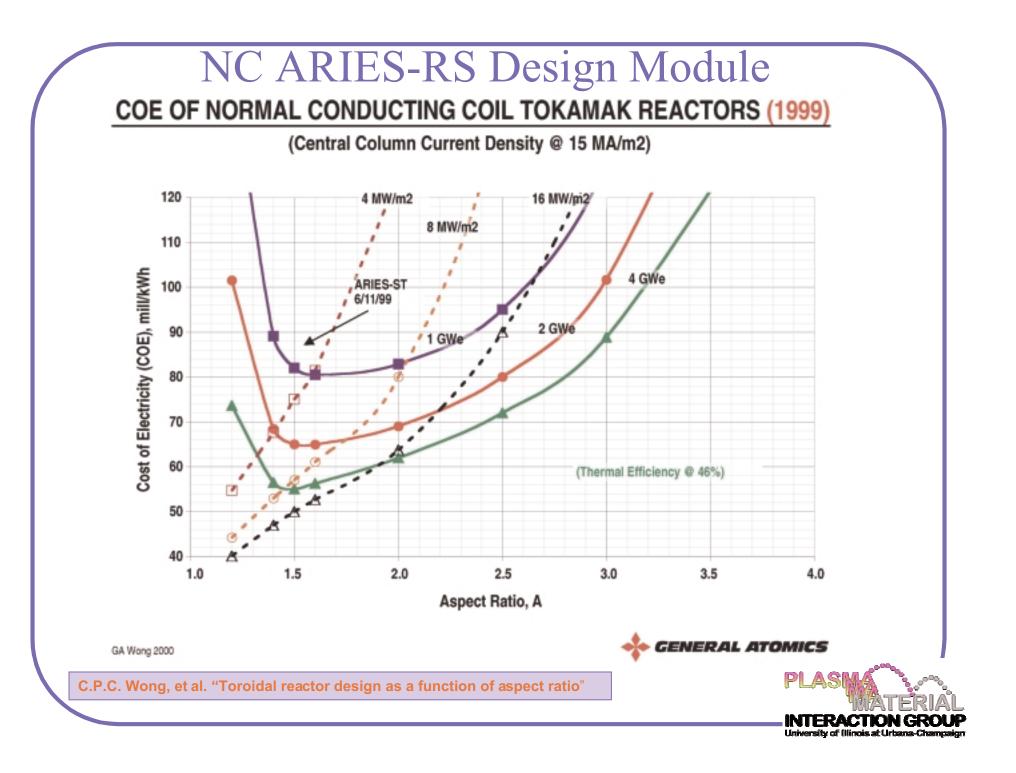
The walls as the problem The walls as the solution Current efforts in plasma facing component science and technology Enabling technologies for existing/future fusion devices **1** Conclusions Acknowledgements



Many of fusion's problems involve plasma wall interactions

- Cheaper electricity means higher power density and therefore more power to walls.
- Disruptions (unplanned and planned) severely limit lifetime and therefore desirability.

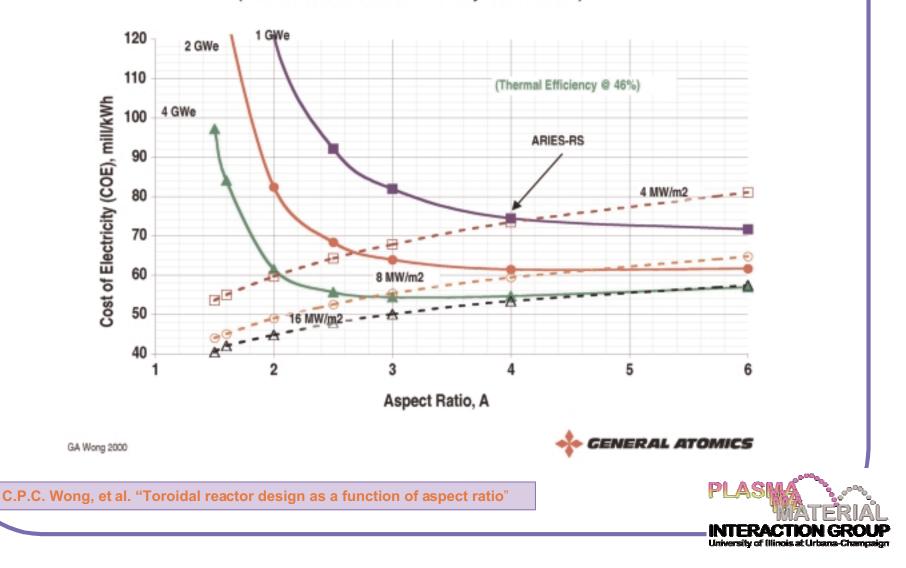




SC ARIES-RS Design Module

COE OF SUPERCONDUCTING COIL TOKAMAK REACTORS (1999) CONSTANT BORE RADIUS

(Central Column Current Density @ 31 MA/m2)



Lithium on surfaces could solve these problems and have other benefits

- h Flowing liquid plasma-facing systems can rapidly remove heat.
- Continuous recovery of damaged surfaces exposed to large heat fluxes due to off-normal events as well as disruptions.
- h TFTR Li pellet and DOLLOP experiments
- Possible stabilization of MHD modes by substituting a moving conducting wall for plasma rotation



TFTR Results: Li conditioning

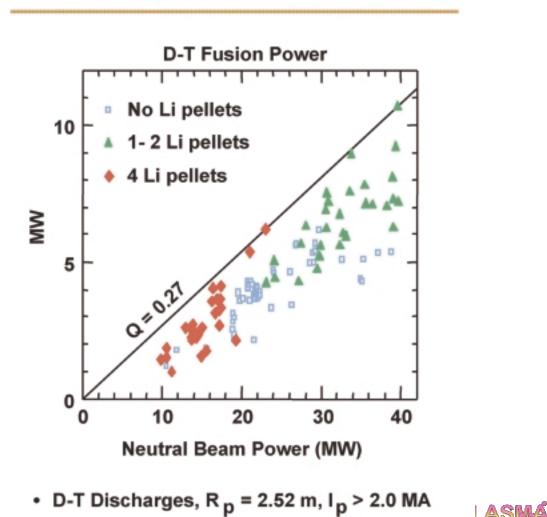


Li 🔶 Enhanced D-T Fusion Power

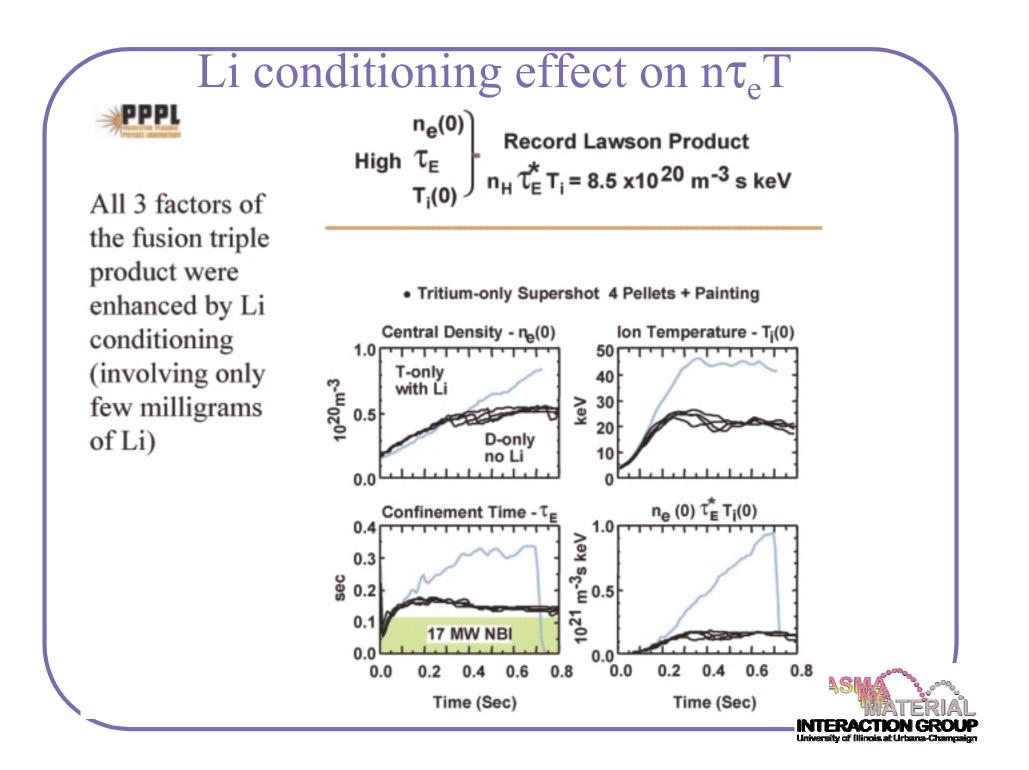
Li conditioning improved overall DT fusion power.

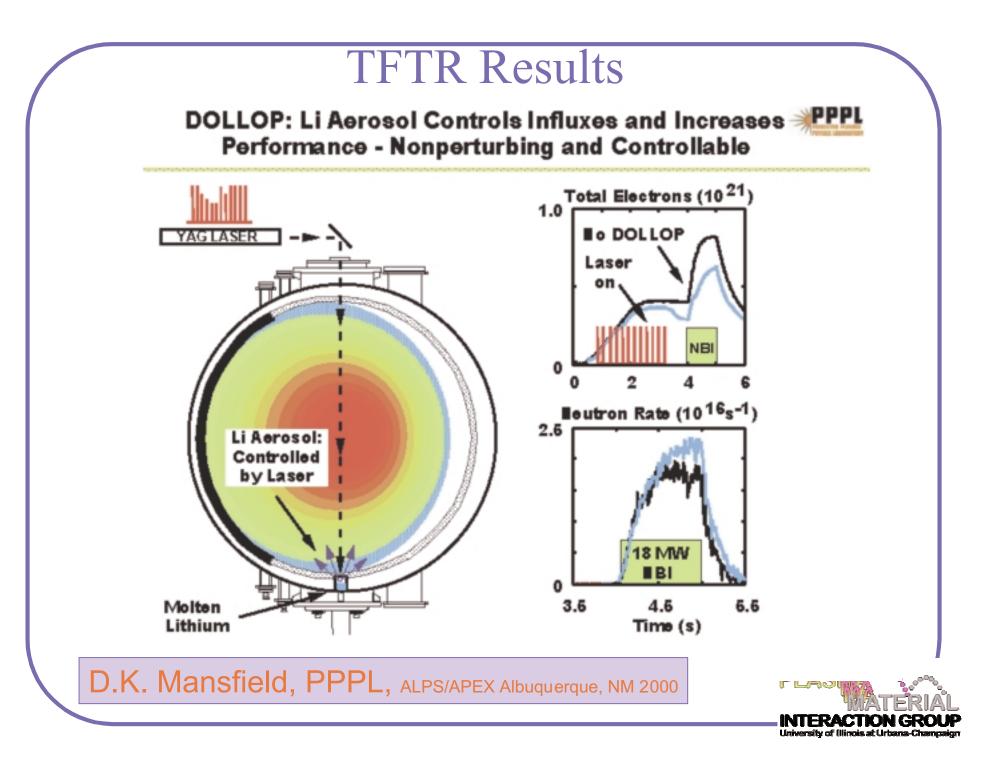
TFTR record fusion power shot was designed using precise Li conditioning.

Use of less Li at higher power was because of MHD high-beta disruption limits in TFTR.



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TFTR DOLLOP Results



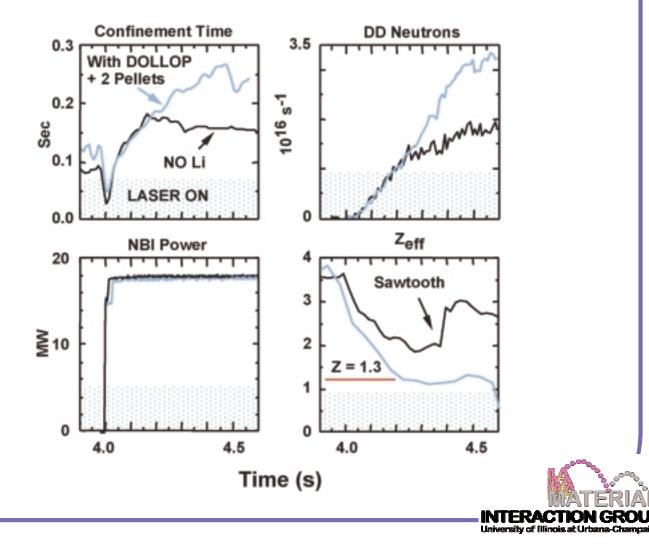
DOLLOP Has Led to Enhanced and Sustained Performance with No Harmful Effects

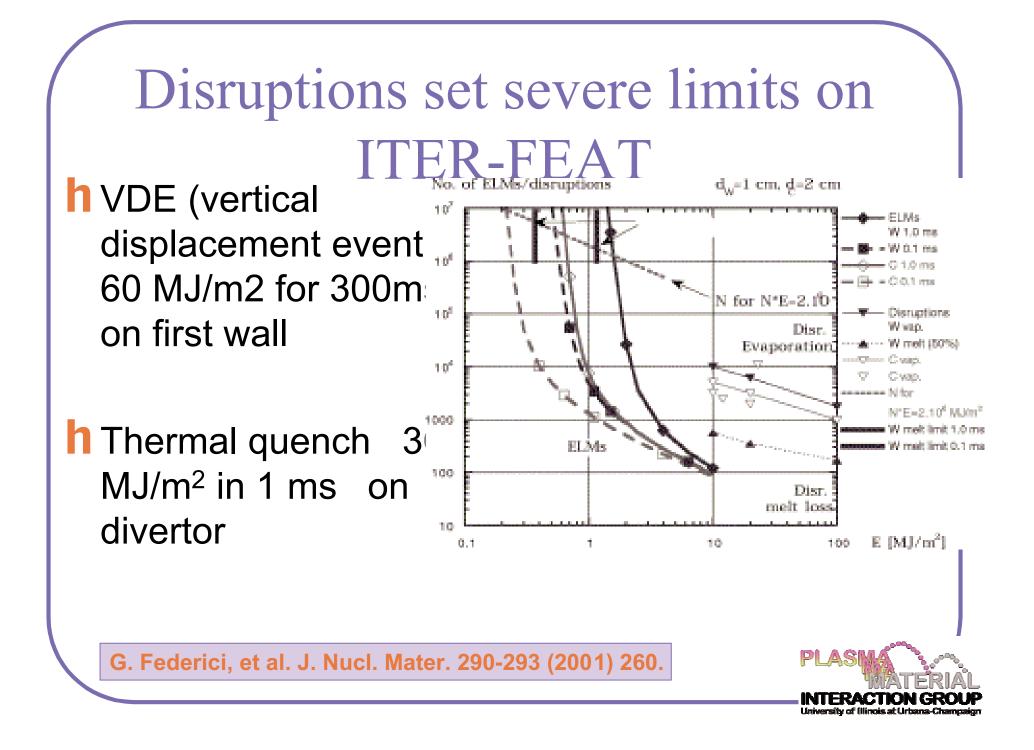
Three TFTR records were achieved (with NO optimization of DOLLOP)

Highest DD energy confinement (no rollover);

Highest Q DD;

Lowest Zeff.





Net erosion of ITER divertor

	Case	Peak net erosion rate (cm/burn-yr)	Tritium codeposition rate ⁴ (g T71000 s pulse)
1.	Reference ^b	49	14
2.	No fast-molecule chemical sputtering	49	13
З.	Y _{msl} =0.01	49	24
4.	No chemical sputtering (physical sputtering only)	9	2
5.	Carbon erosion reduced due to beryllium (from wall) mixing	47	11
6.	Beryllium divertor coating	30	2
7.	Tungsten divertor coating	<0.1	~0
8.	'Shallow detached' plasma [13]	23	17

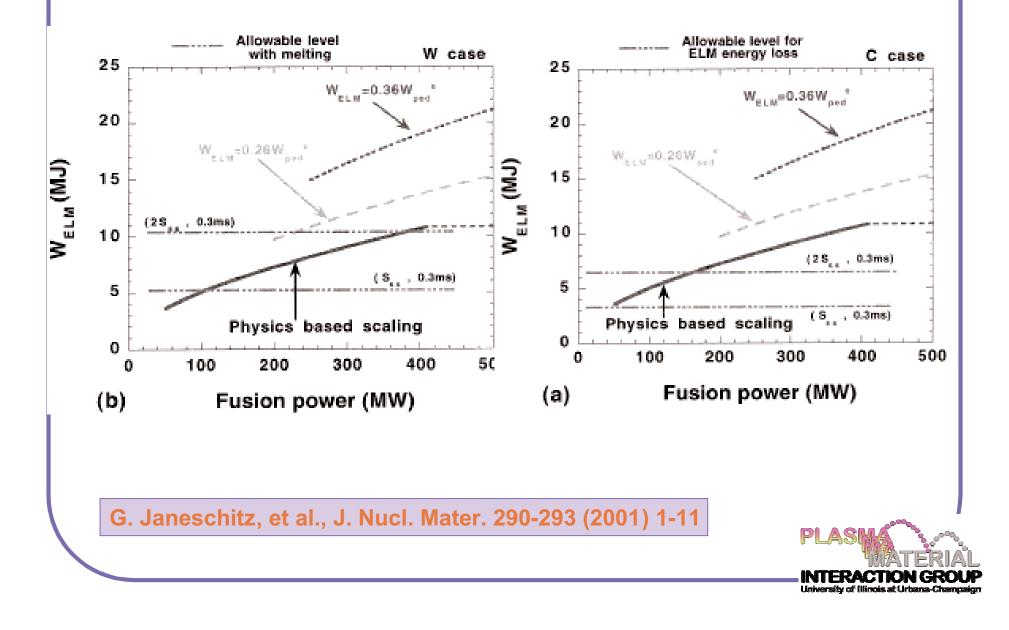
Total (inner + outer divertor) resulting from vertical target sputtering.

^bReference: carbon coating, Case 98-semi-detached plasma, physical and chemical sputtering, non-thermal D–T molecule sputtering yield $\Upsilon_{msi} = 0.001$. •With TPE H/Be trapping ratio data [9].

J. Brooks, D. Alman, G. Federici, D.N. Ruzic and D.G. Whyte J. Nucl. Mater. 266-269 (1999) 58.



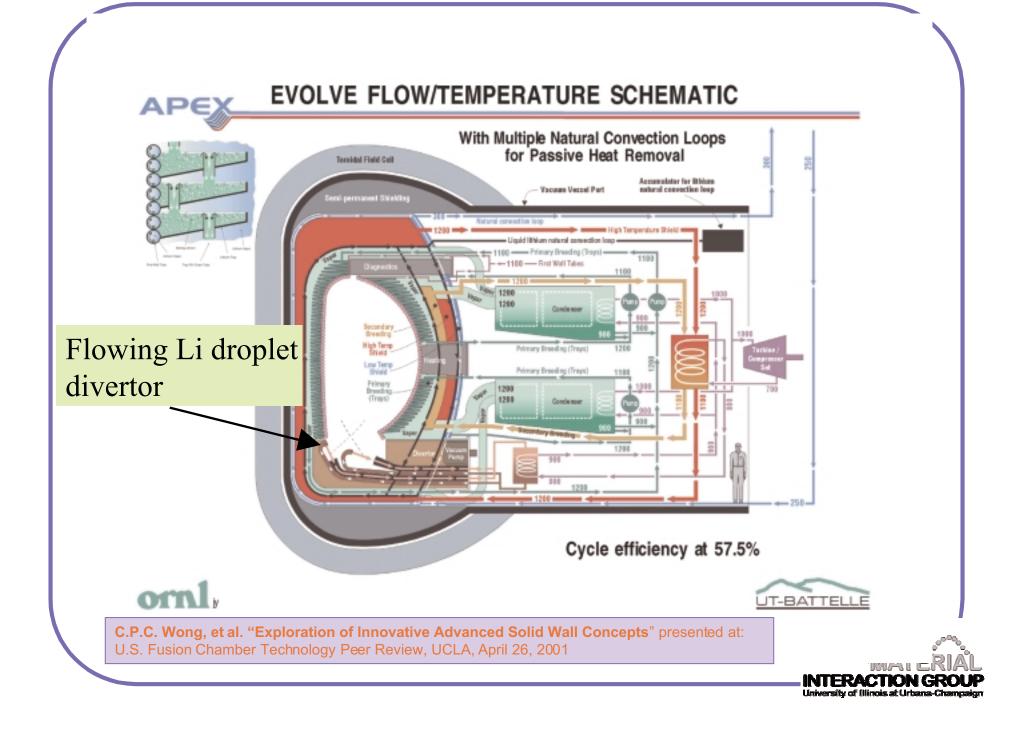
ELMs set power limit even for W



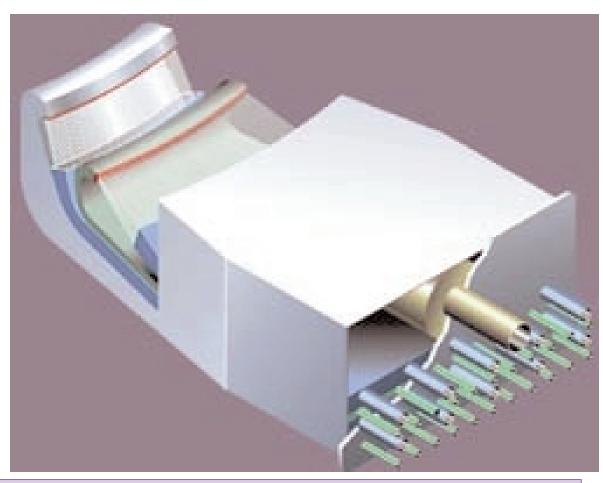
Plasma Facing Component Science and Technology Program

- Integrated concepts
- Lab-scale investigations
- Modeling efforts
- Near-term experiments



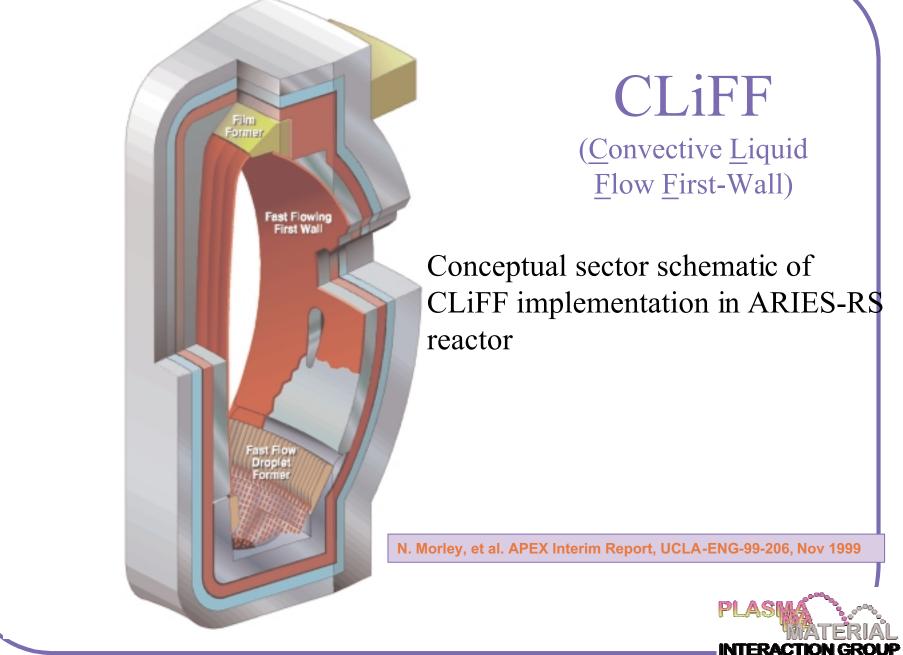


Flowing lithium droplet divertor cassette



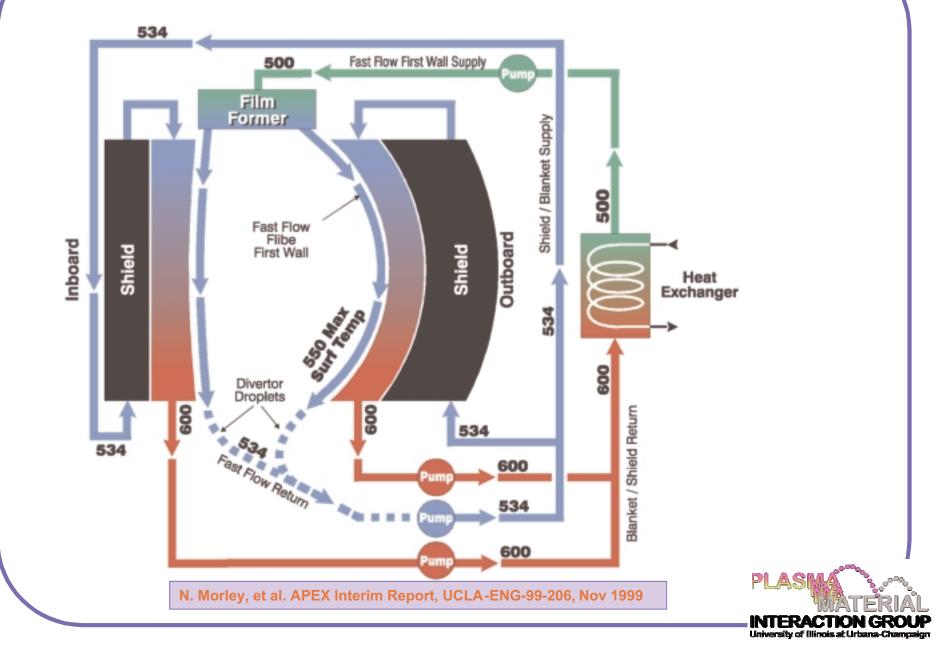
R.F. Mattas, "ALPS – advanced limiter-divertor plasma-facing systems" Fusion Engineering and Design 49-50 (2000) 127-134

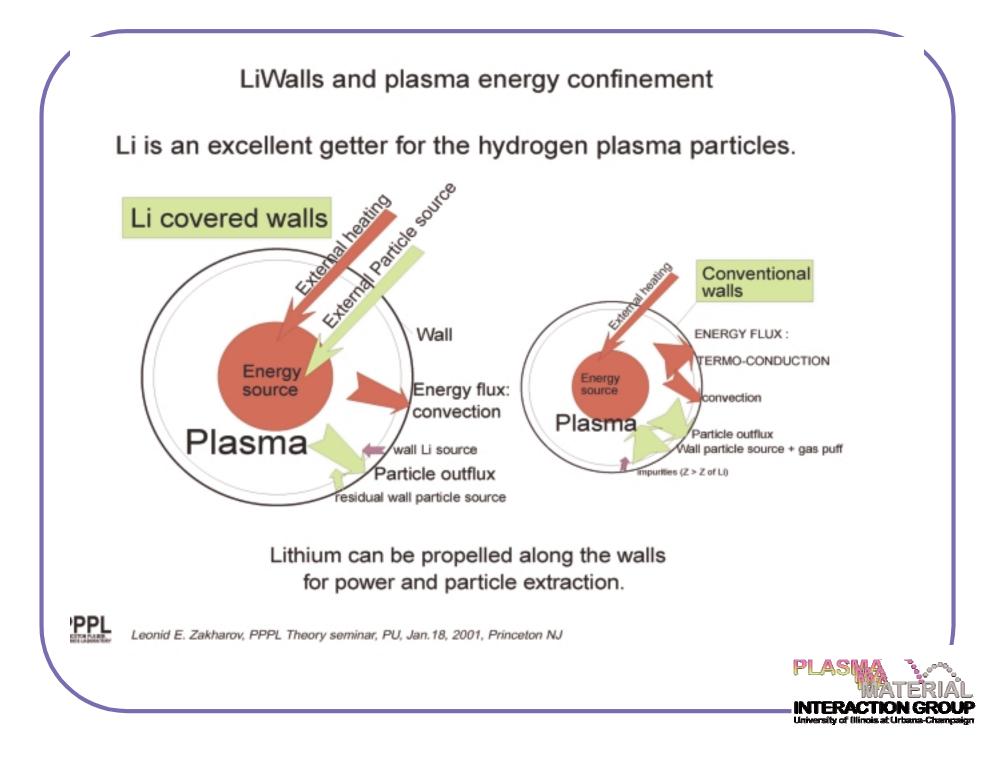




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CLiFF – Flow/Temperature Schematic





6 LiWalls and plasma energy confinement (cont.)

Improved energy confinement is extremely for igniting the plasma $n_{DT} \cdot T_{DT} \cdot \tau_E > 5 \times 10^{21} \ m^{-3} \cdot keV \cdot s, \quad n_{DT} \cdot T_{DT} \cdot \tau_E \propto \tau_E^2$

Plasma profiles are determined by the particle continuity equation

$$\Gamma \equiv Snv = const = (\Gamma)_a$$

and by the energy balance

$$\frac{5}{2}\Gamma T - S(\kappa_T \nabla T + \kappa_n \nabla n) = \int_0^r P_E dv$$

With perfectly absorbing walls plasma does not know the temperature of the (cold) walls and leaves no room for thermo-conduction

$$\left(\frac{5}{2}\Gamma T\right)_{edge} = \int_0^a P_E dv, \quad T_{edge} = \frac{\int_0^a P_E dv}{\frac{5}{2}\Gamma} \quad P_E$$
- heat source.

Thus, the major energy loss channel, i.e., thermoconduction, can be eliminated with this absorbing wall boundary condition (S. Krasheninnikov, PFSC at MIT, now at UCSD).



IIAX (Ion-surface InterAction eXperiment)

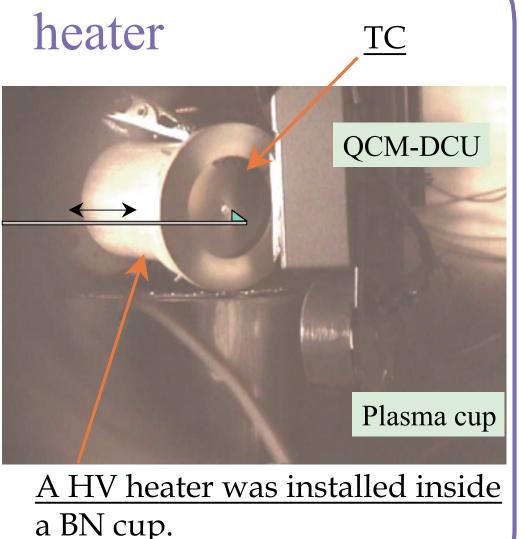




In-situ cleaving arm design and HV

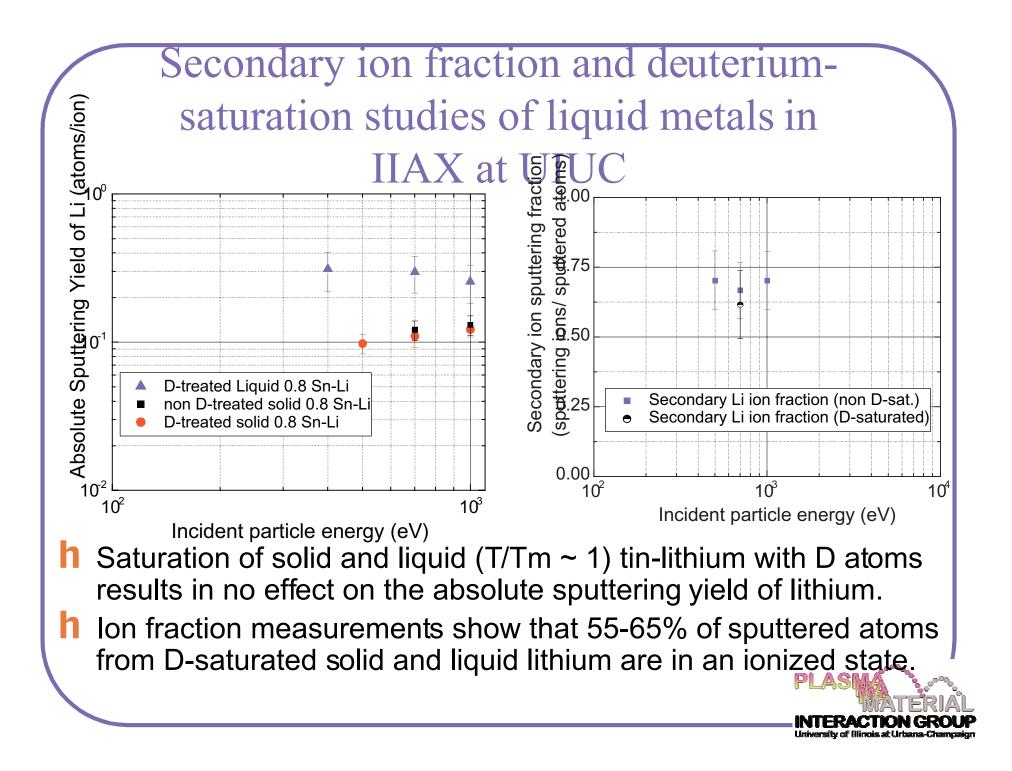
Cleaving arm is designed to remove thin oxide layer formed on Li layer of liquid tin-lithium or liquid lithium sample **1** Surface composition experiments show that Li segregates to the liquid Sn-Li

surface¹



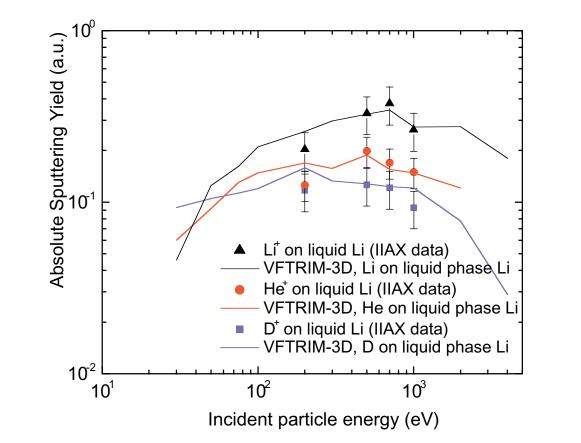
1. B. Bastasz J. Nuclear Mater. 290-293 (2001) 19.





IIAX experimental and modeling data on liquid lithium erosion

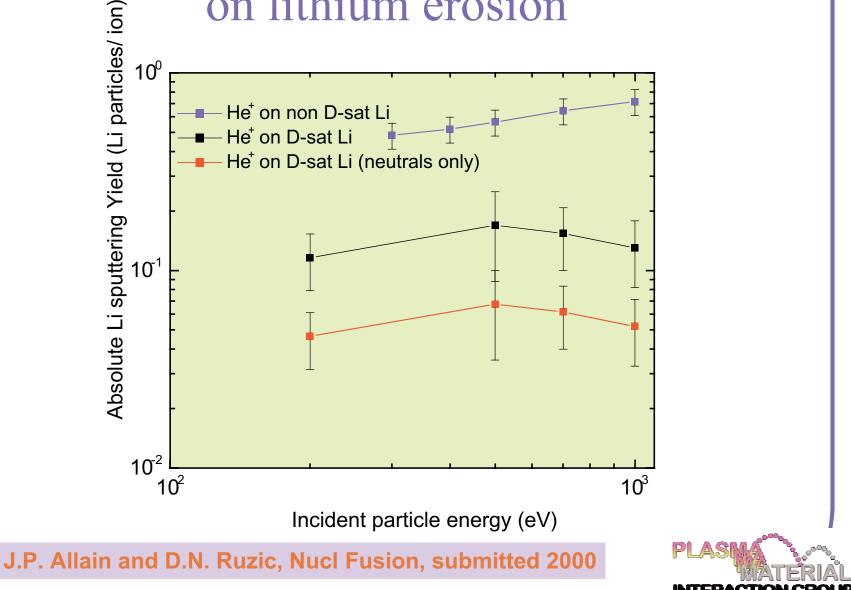
- D treated lithium yields are well below unity
- Data taken at
 45 deg.
 Incidence and
 200 C surface
 temperature



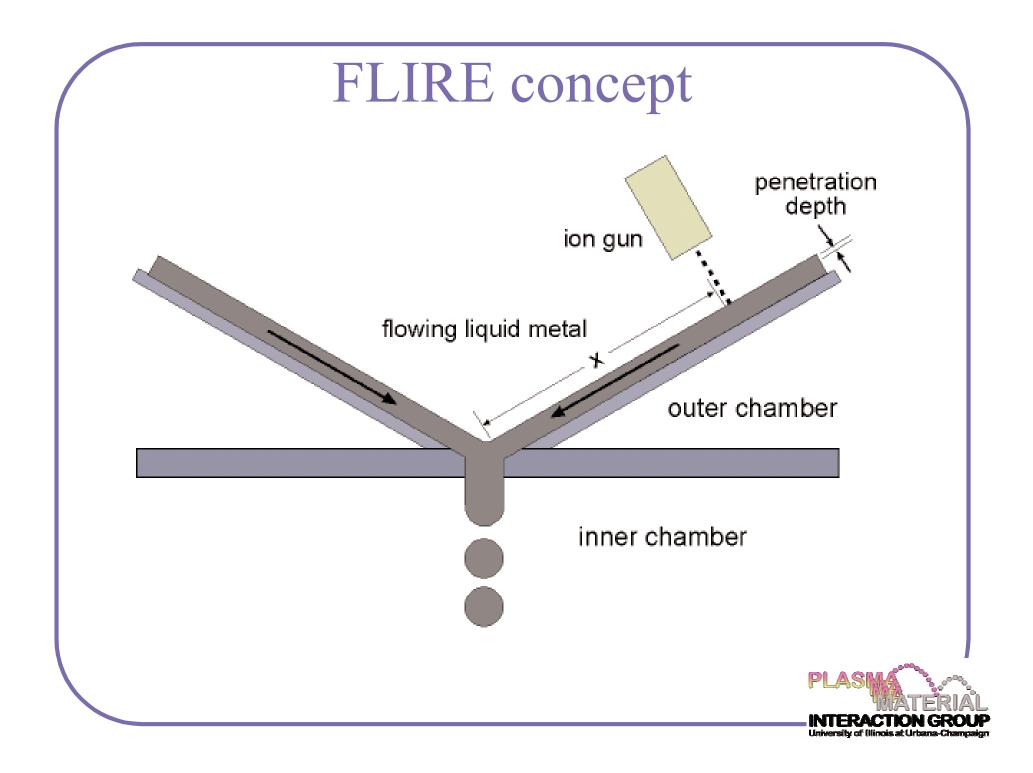
J.P. Allain, M.R. Hendricks and D.N. Ruzic, J. Nucl. Mater. 290-293 (2001) 180



Effect of deuterium surface treatment an lithium erosion

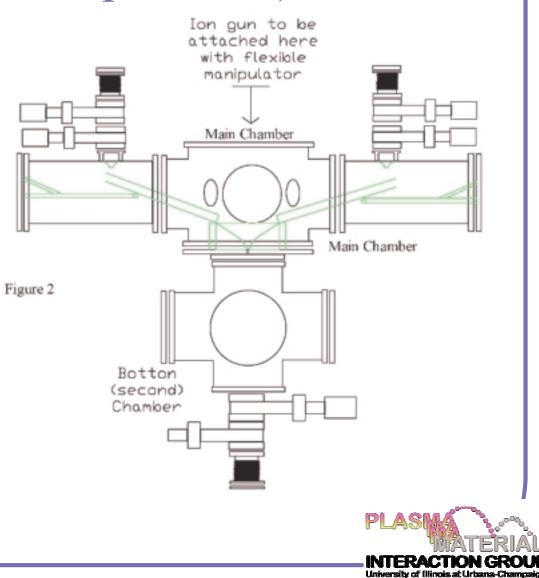


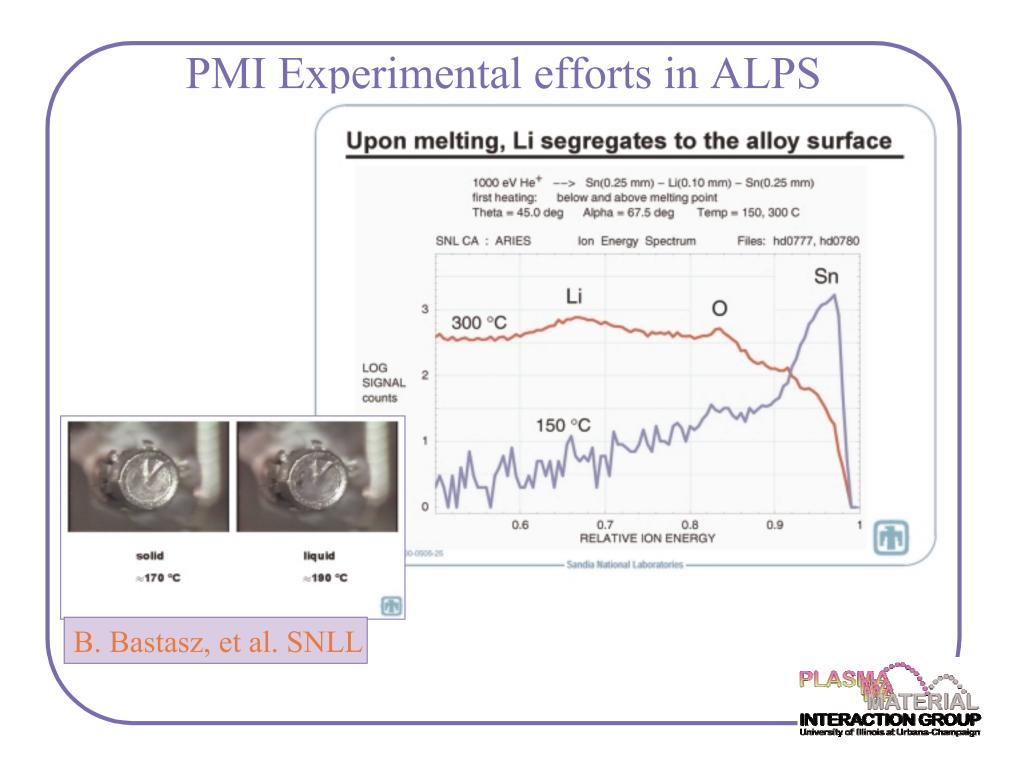
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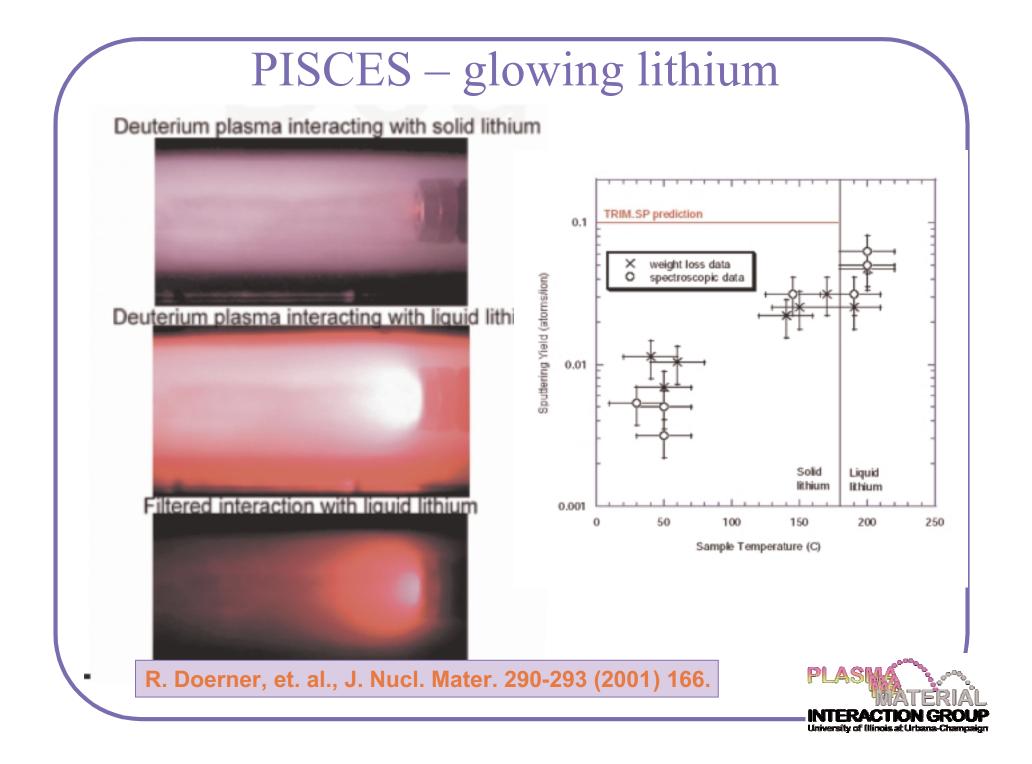


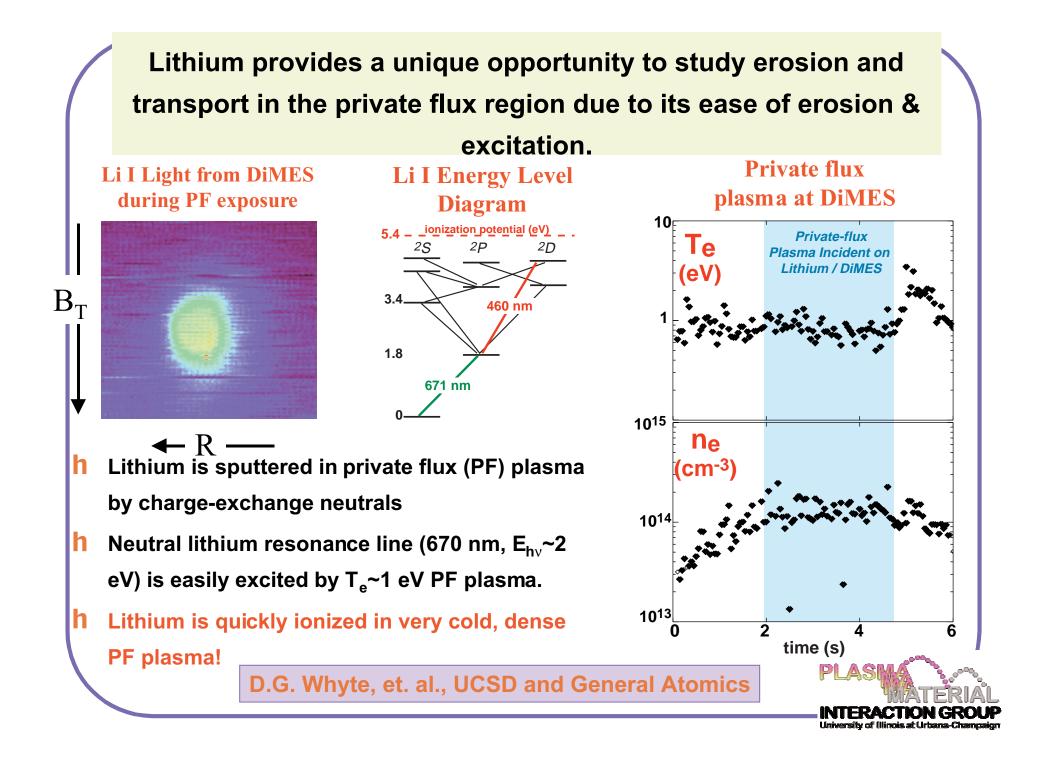
FLIRE (Flowing Liquid Surface Illinois Retention Experiment)

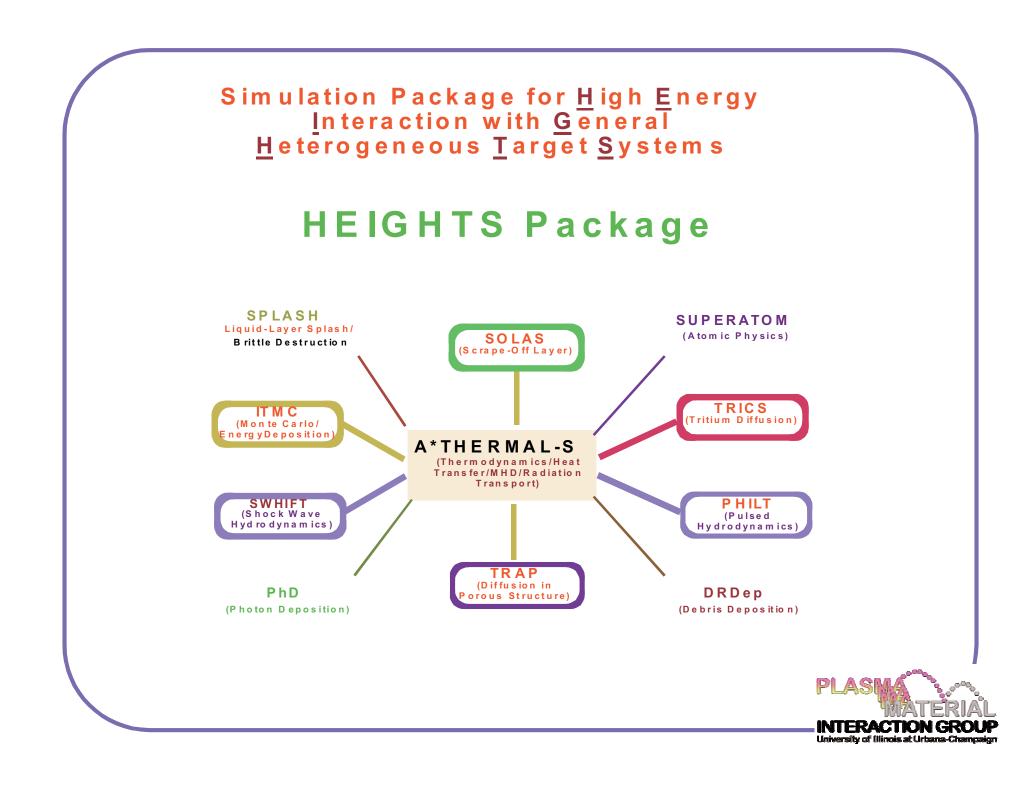
FLIRE will provide fundamental data on the retention and pumping of He, H, and other gases in flowing liquid surfaces.

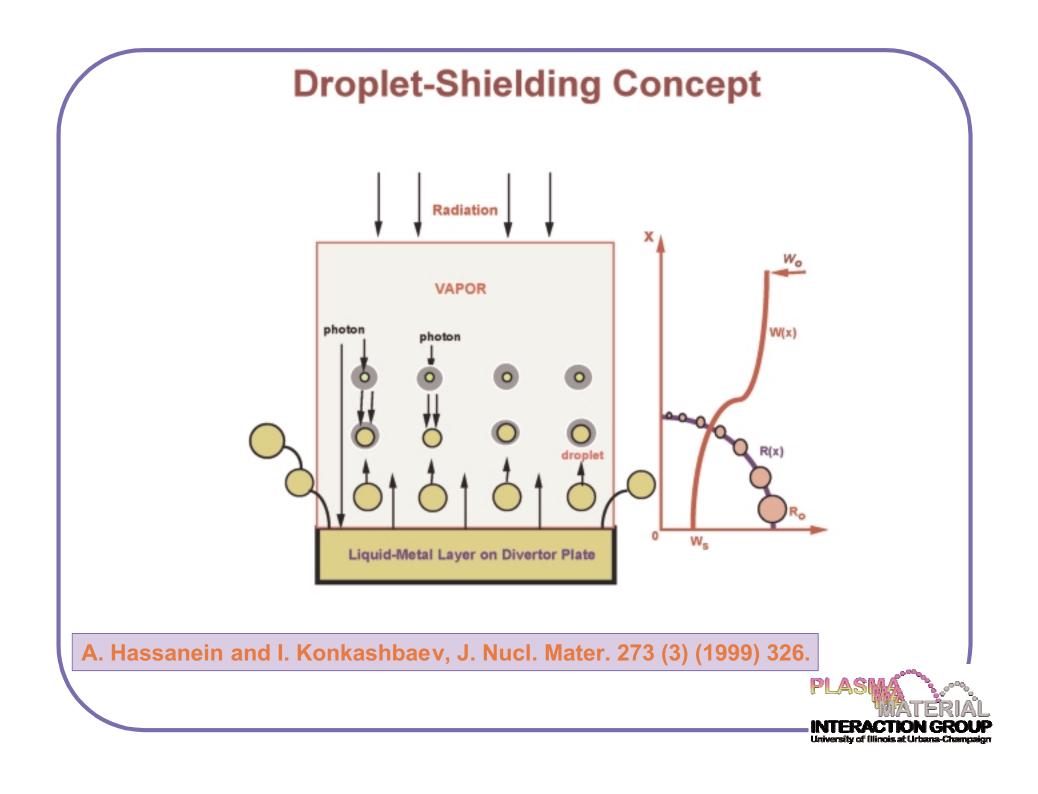


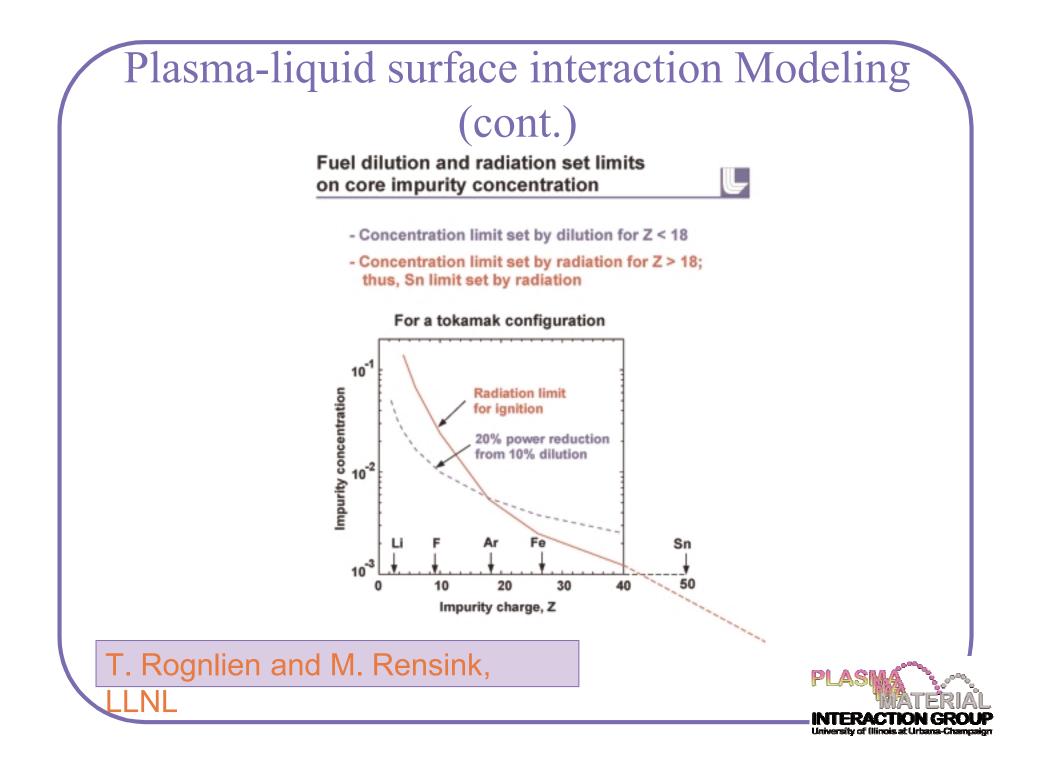


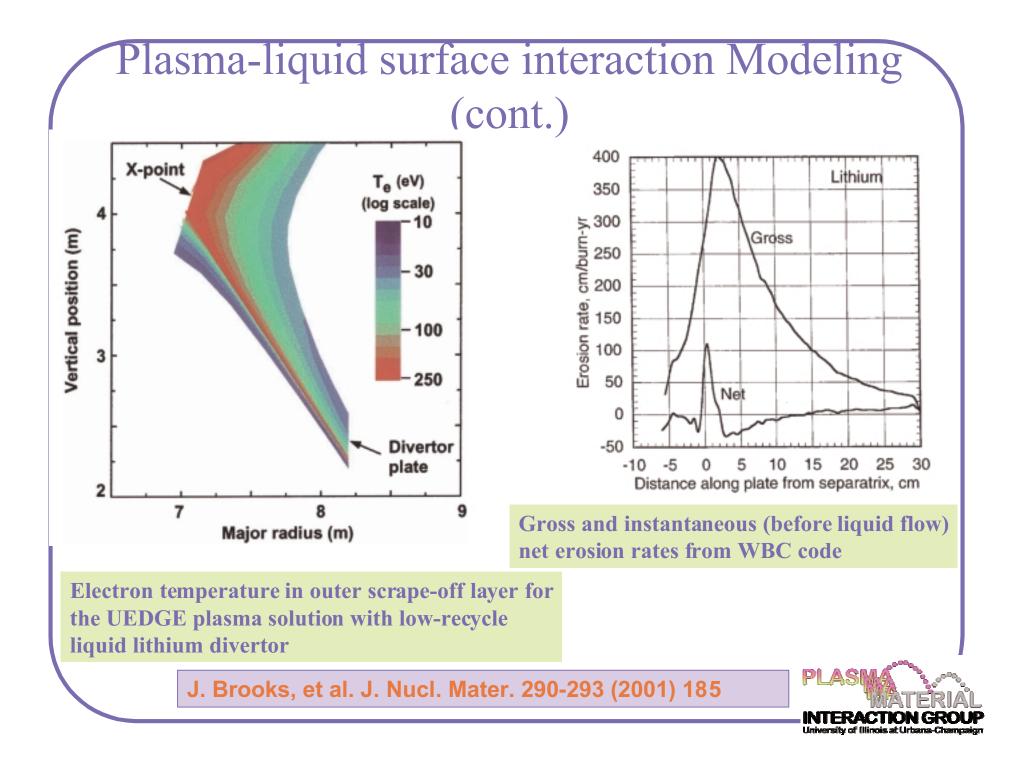






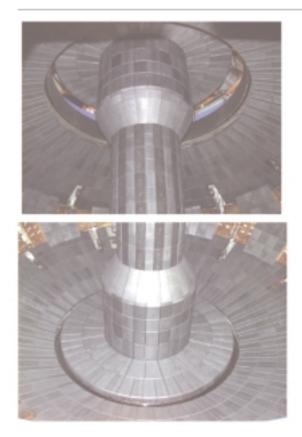


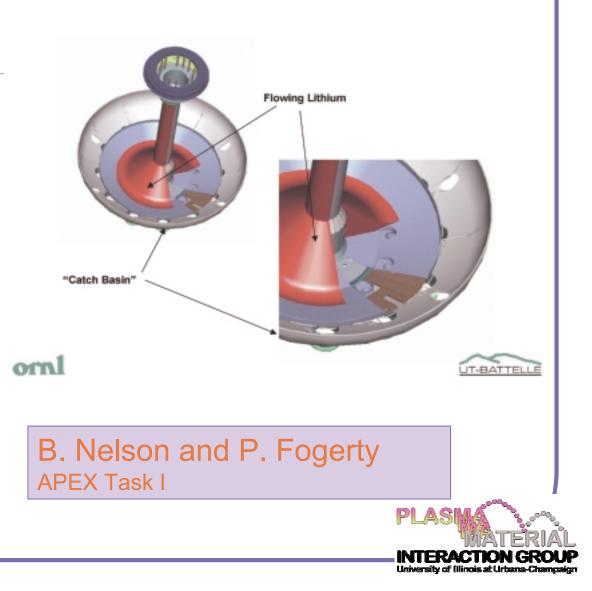




NSTX: application of flowing liquid metal (i.e. ALIST)

NSTX Device configuration





Conclusions

- Plasma interactions with the surfaces limit the desirability of fusion power
- Advances in fusion science and performance often follow new surface-related discoveries
- Wall concepts involving Li show great potential to solve many known problems
- ALPS and APEX programs are actively engaged in pursuing these solutions
- Planned burning plasma devices should consider including these – they may just be what makes it work.



Acknowledgements

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