



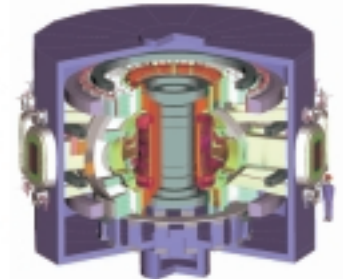
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# Advanced Magnets and Implications for BPX-I

*J.H. Schultz, P. Titus, J.V. Minervini*  
M.I.T. Plasma Science and Fusion Center

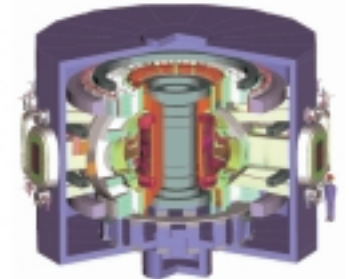
**Burning Plasma Science Workshop II**  
**General Atomics**  
**San Diego, CA**  
**May 1–3, 2001**





## Issues in BPX Advanced Magnet Systems

1. Magnet System Goodness Factors
2. Progress in BPX Magnets
3. Progress in BPX Magnet Materials





## Tokamak Magnet Systems are Scaleable

$$B = \text{Const}$$

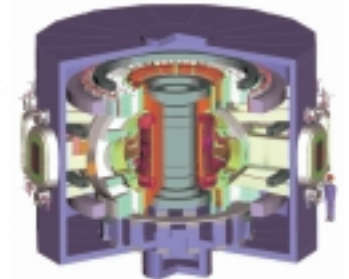
$$\sigma = \text{Const}$$

$$J = R^{-1}$$

$$t = R^2$$

☺ Any advanced magnet system can be scaled-up to FIRE or ITER

☹ There are no advanced magnet systems, not even close





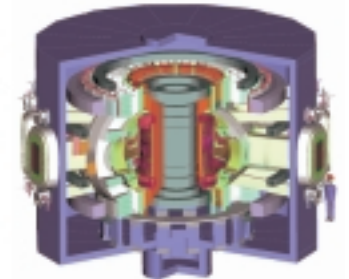
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# **IpA/R as Tokamak Magnet System Goodness Factor**

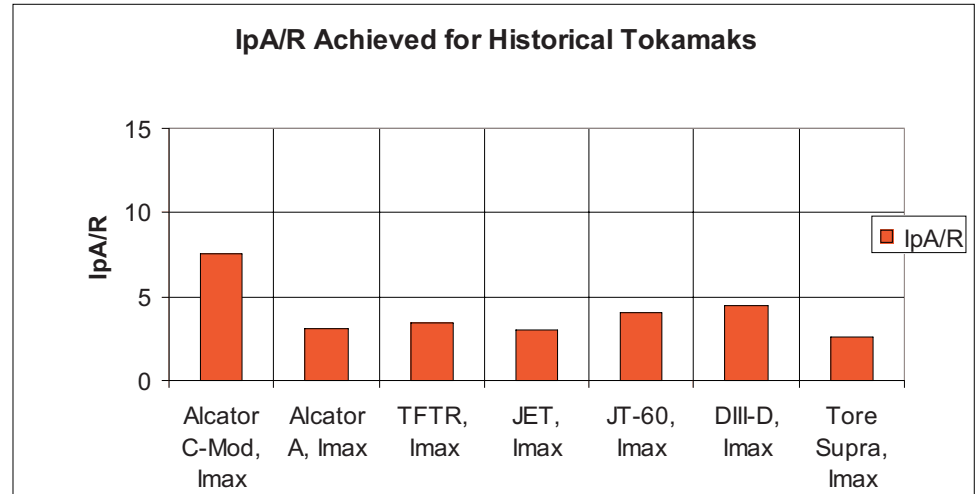
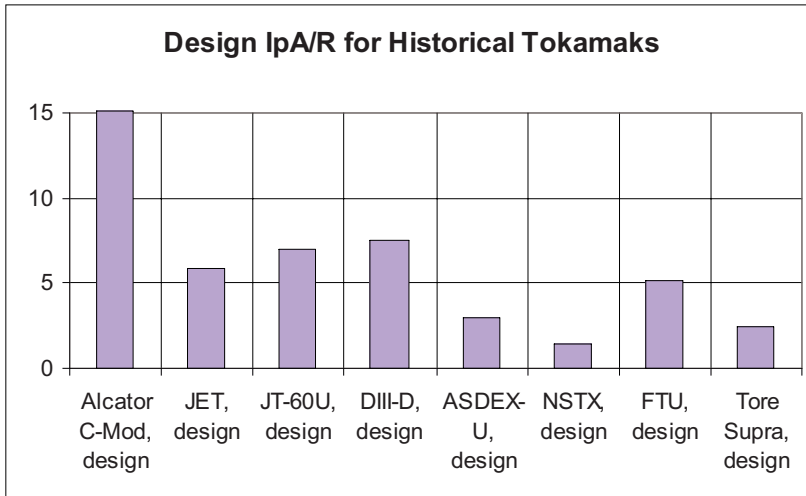
**Dimensionally same as Bt, but:**

Feature	IpA/R	Bt
Scaleable	Yes	Yes
CS/TF Interface	Yes	No
In-plane vs. OOP Forces	Yes	No
$K, \Delta$	Yes	No





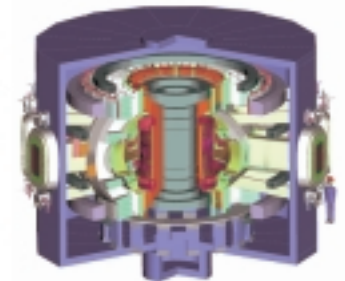
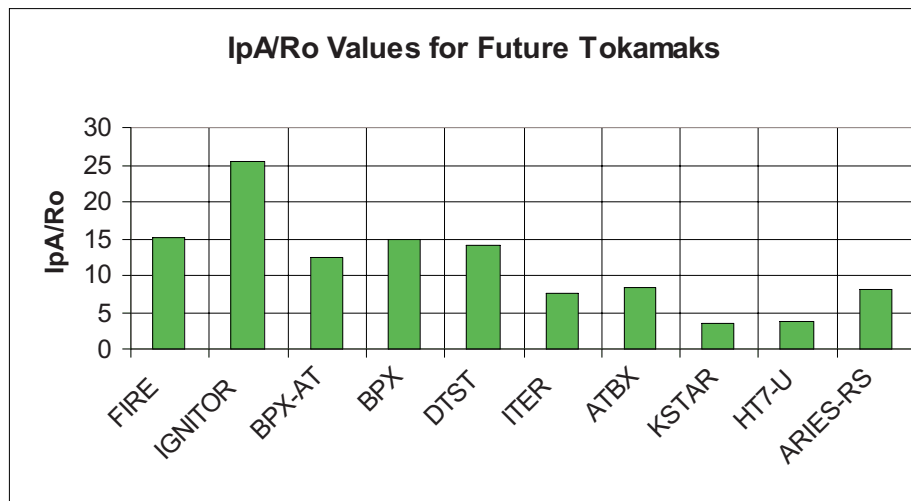
# IpA/R Historical Survey



FIRE IpA/Ro 2x as high as world record

IGNITOR IpA/Ro 70% higher than other designs

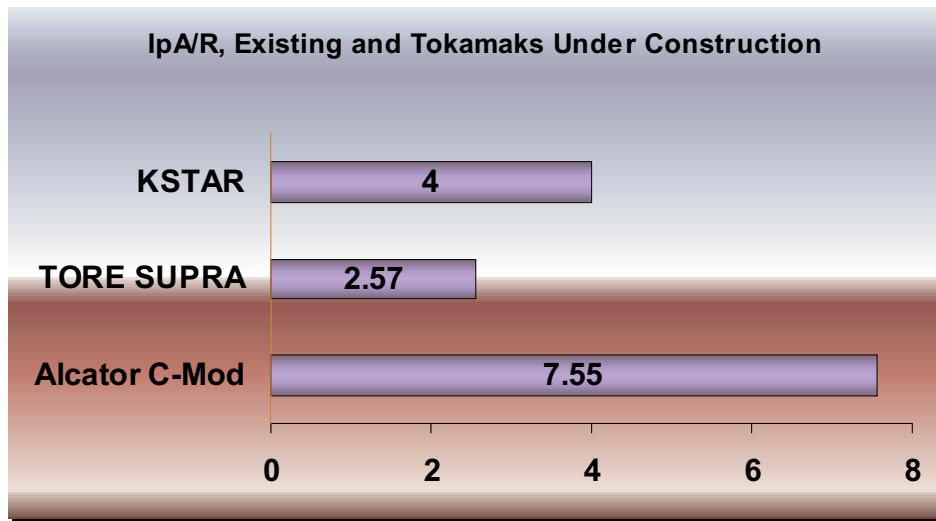
FIRE IpA/Ro 2x as high as ITER



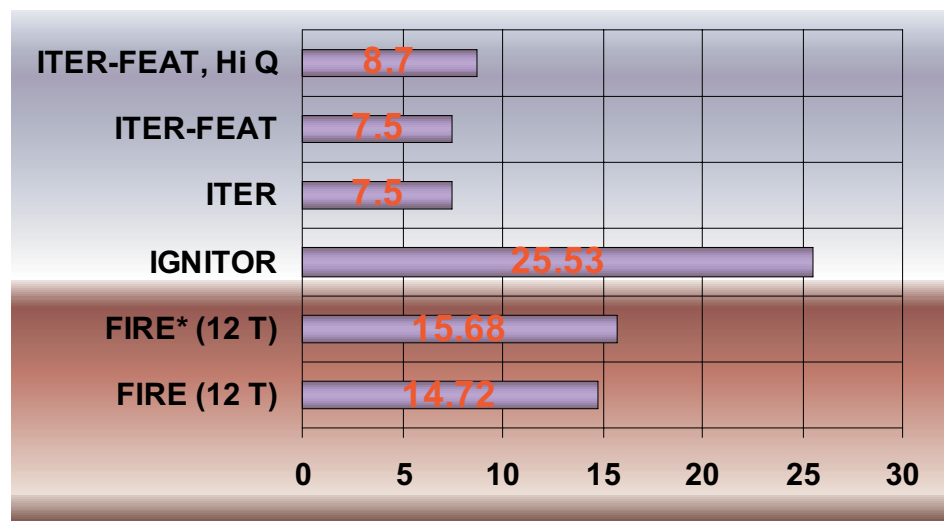


# The Superconducting Shortfall (and the Absence of Scale Models)

Existing and Tokamaks Under Construction

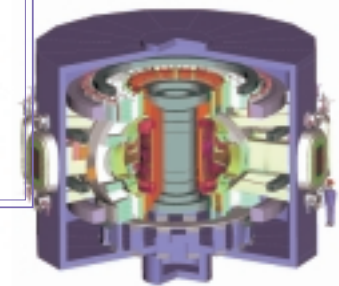


Tokamaks Under Design



**Tore Supra: World's Best Superconducting Tokamak, IpA/R only 1/3 that of Alcator C-Mod**  
**KSTAR: 56 % improvement,**  
**C-Mod IpA/R still 89 % better than KSTAR**

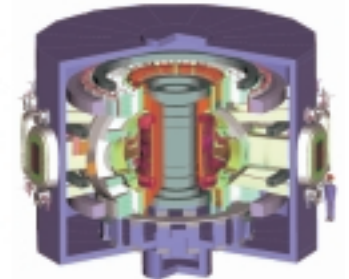
**ITER/ITER-FEAT: 88 % improvement on KSTAR,**  
**= CMod**  
**IpA/R half as good as FIRE,**  
**27 % of Ignitor**





## Why is FIRE higher- $I_p A/R$ than existing (esp. Alcator) tokamaks?

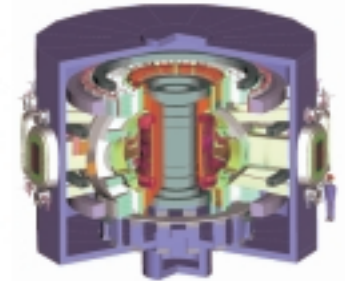
- 1) Plate construction, adiabatically nitrogen-cooled (e.g. Alcator)
- 2) Bucking/Wedging
- 3) Compression Rings
- 4) Zero-turn loss scarf joints





## Why is IGNITOR higher- $I_p A/R$ than FIRE?

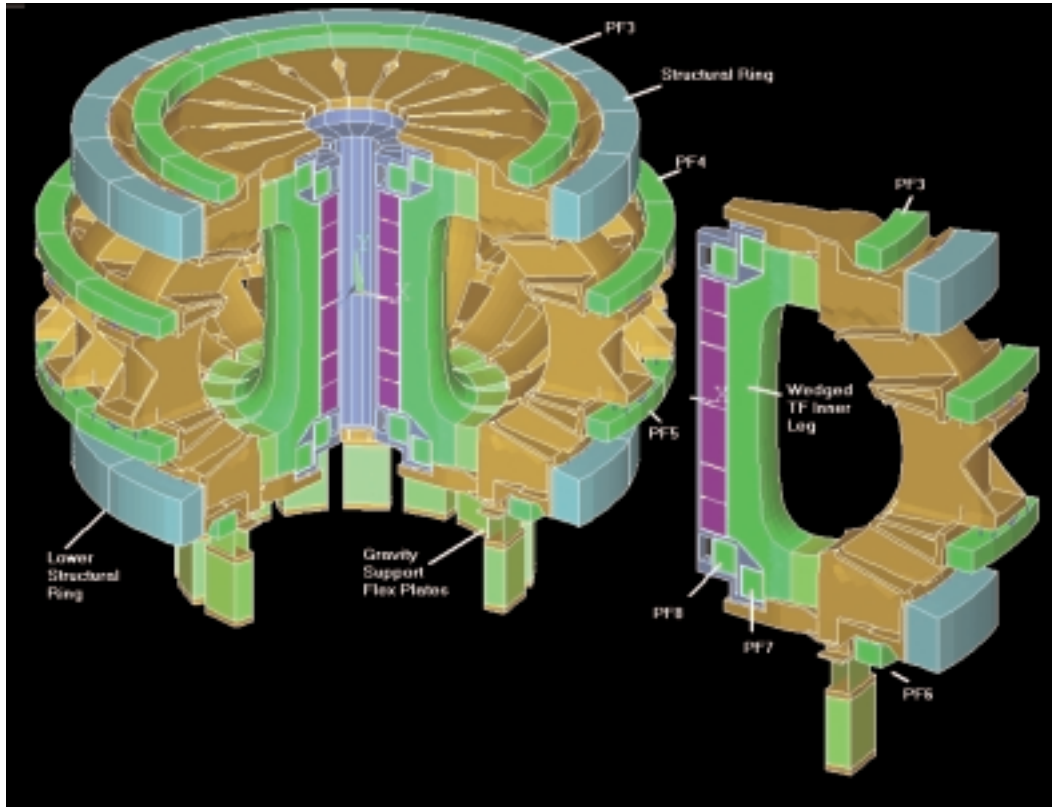
- 1) No divertor, plasma optimized for low OOP
- 2) Active clamping
- 3) Recool to 30 K







## Buck/Wedged Design with Copper Inner Leg (FIRE)



Bladder preinserted before assembly  
- epoxy shims injected after assembly  
(high reliability with reasonable tolerances)

Cu replaces 68 % IACS BeCu

Main benefit to power supply

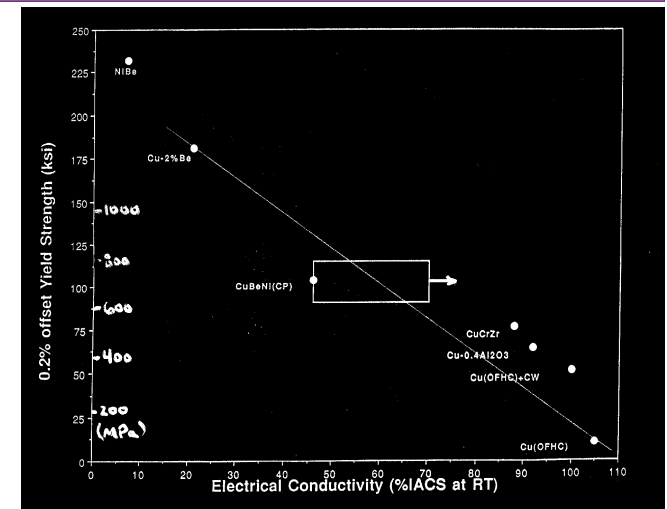
Stress in inner leg reduced x 2

Expect IpA/R improve by 20 % ( $2^{1/4}$ )

IpA/R improvement only 10 % in FIRE

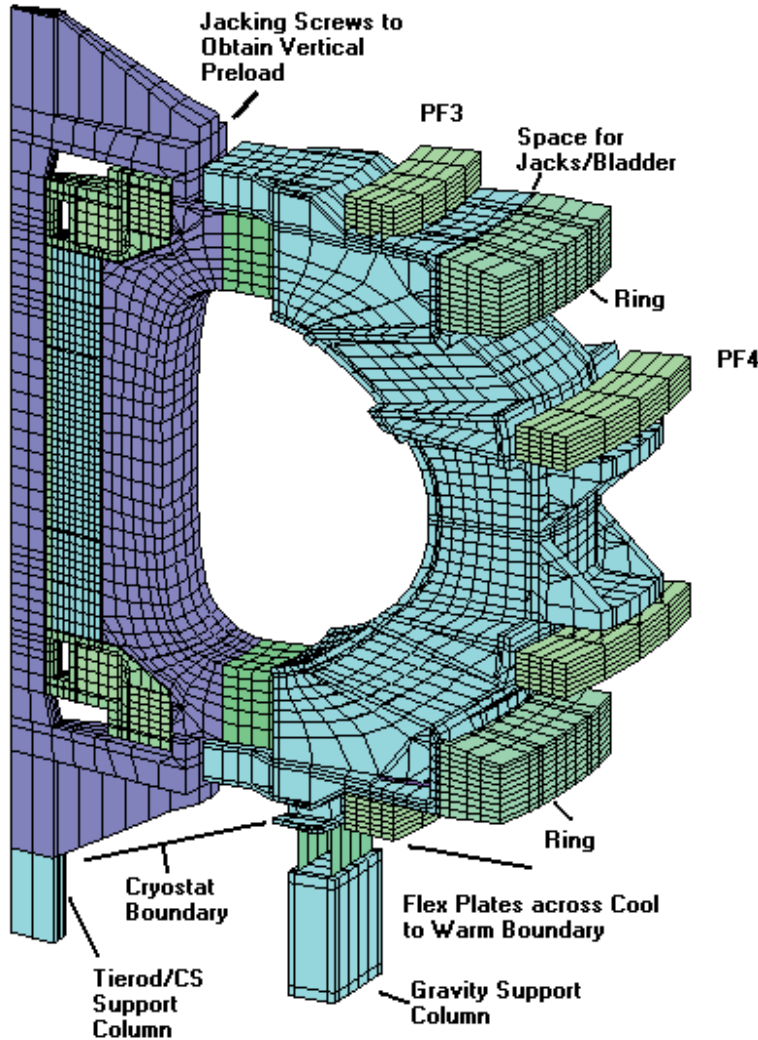
- desensitized by Copper Alloy selection

	$B_{max}$ (T)	$t_{flat, nonuc}$ (s)	$t_{flat, nuc}$ (s)
<b>Buck and Wedge</b>	10	51	62
<b>Buck and Wedge</b>	11.5	44.5	36
<b>Wedge</b>	10	21	18.5
<b>Wedge</b>	12	15	12





# The FIRE Compression Rings

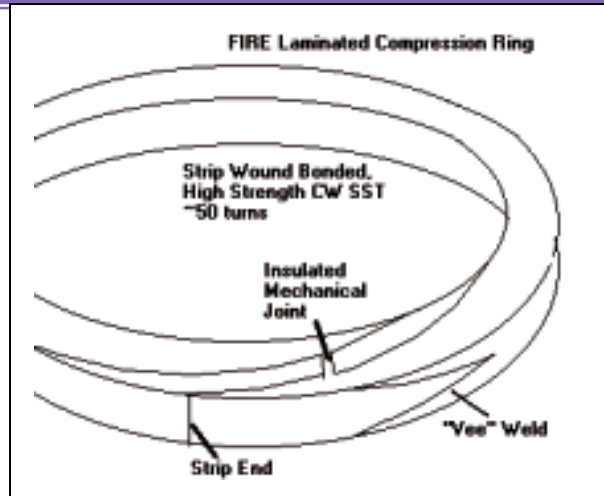


External rings prevent excessive shear between TF plates,  
due to OOP moments

Add compression to bond between insulating sheets and cases

Without compression rings, insulation shear allowables are exceeded at ~ 1/10 IB product

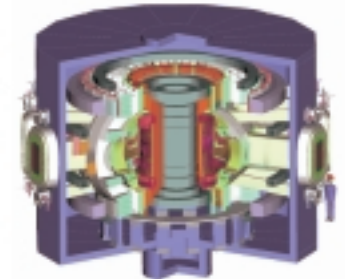
i.e. 4 T x 2 MA (TPX) vs. 12 T x 7.7 MA



50 turns, welded 1 cm  
304 SS plate

Turns, insulated,  
bonded

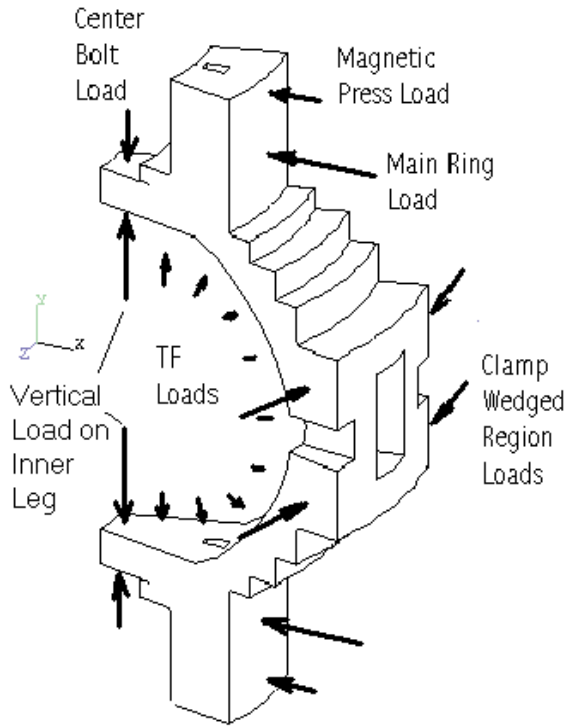
Mechanical connection  
from inside-outside



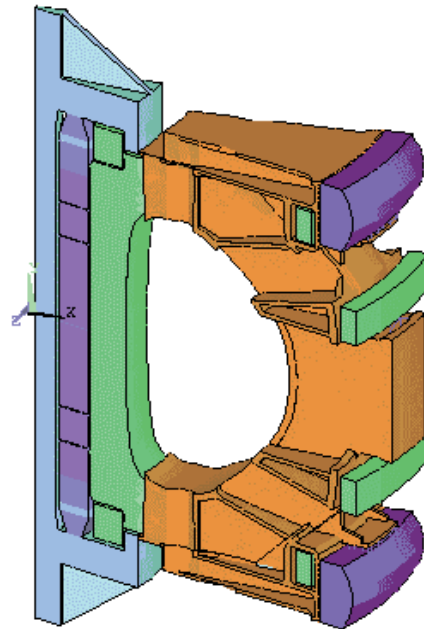


# Active Compression Rings

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In IGNITOR the Main Ring and Mag. Press Overcome Radially Outward Loads and Cause a Vertical "Pinching" of the Inner Leg.



FIRE with Radial Compression Rings, and Vertical Preload using a Tierod

In FIRE, The Proposed Rings are Intended to Augment Wedging Pressures in the TF Inner Leg Corners to Help Support OOP Loads.

Clamp Function Can be Chosen based on Ring Vertical Position with Respect to the Horizontal Leg.

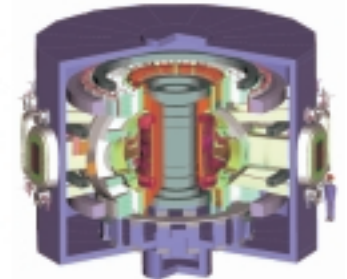
## Ignitor Magnetic Press

**Reduces/eliminates primary membrane stress in nose**

**Active - can track thermal and Lorentz stresses: e.g. FIRE: peak stress after assembly, not operation**

**Can match "shear advantage" for special case of PF field lines nearly parallel  $I_{TF}$**

**Advantage of 13 % over FIRE compression ring**



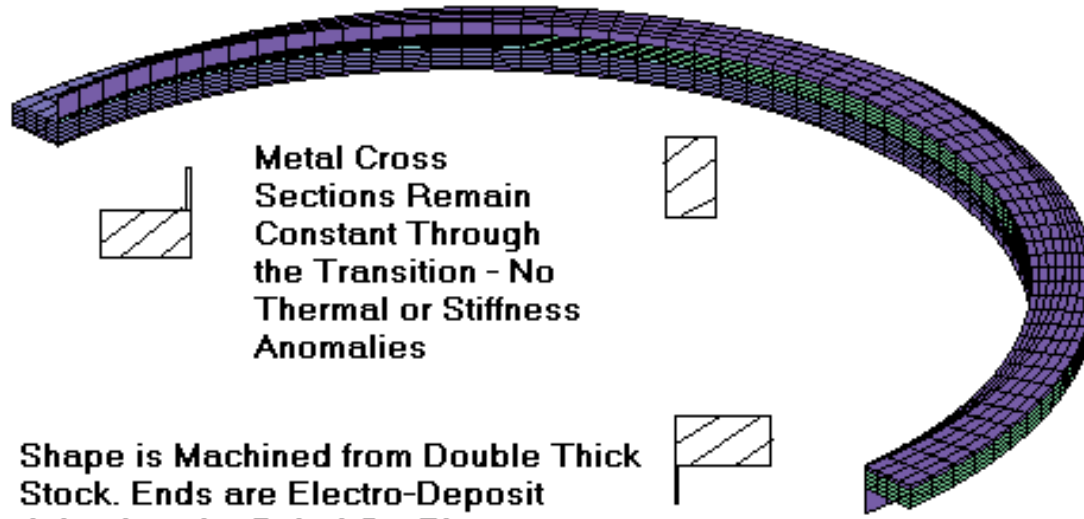


## Zero Turn Loss Scarf/Transition Joint

Zero Turn Loss Scarf /Transition Joint

Peak local stress reduced x 2

I<sub>p</sub> improvement ~ 10 %

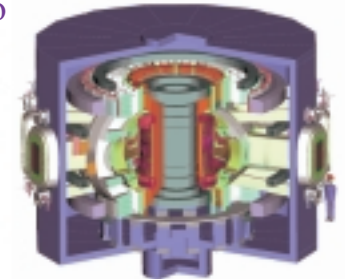


**Metal Cross Sections Remain Constant Through the Transition - No Thermal or Stiffness Anomalies**

**Shape is Machined from Double Thick Stock. Ends are Electro-Deposit Joined to the Spiral Cut Plate.**

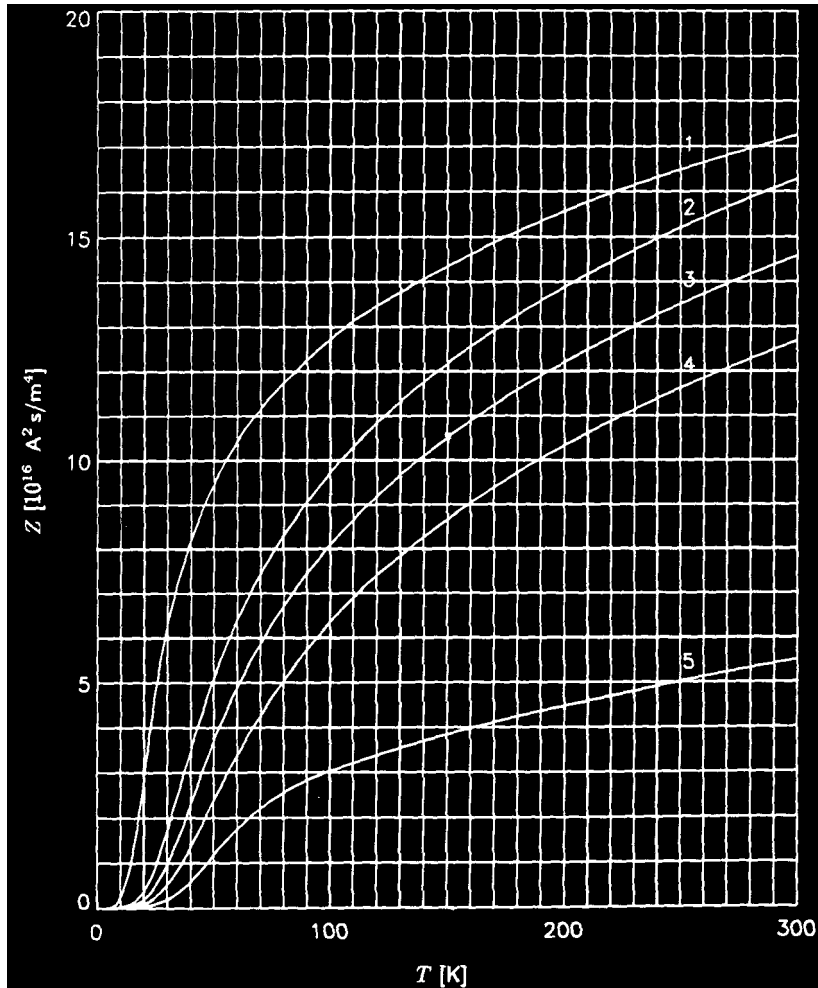
### Inner Joint for Pancake Wound Coils

- No Stress or Stiffness anomaly - Working Stress is the Same as for the Winding.
- No Thermal Anomaly in Normal Conductor Coils - No Differential Thermal Strains
- No Turn Loss
- No Projection into the Bore
- Electrodeposited joint as strong as base metal



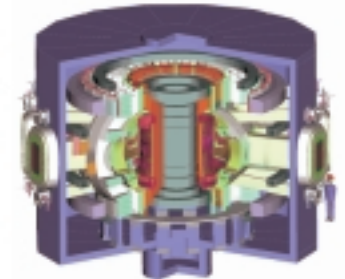


# Subcooling in Ignitor



- $T_{init, Ignitor} = 30 \text{ K}$ ;  $T_{init, FIRE} = 77 \text{ K}$
- Entropy generations  $\sim$  equal, lower temperature vs. smaller size
- 5 hr cooldown, Ignitor; 3 hr, FIRE
- Neither has activated IN2
  - FIRE flushes with He gas, after IN2 cooldown
- 40 % improvement in  $J^2t$ 
  - 20 % in  $J_{cu}$ , 10 % in  $I_p A/R$

$Z(T_p)$  functions: 1. Silver (99.99%); 2. Copper (RRR 200); 3. Copper (RRR 100);  
4. Copper (RRR 50); 5. Aluminum (99.99%)





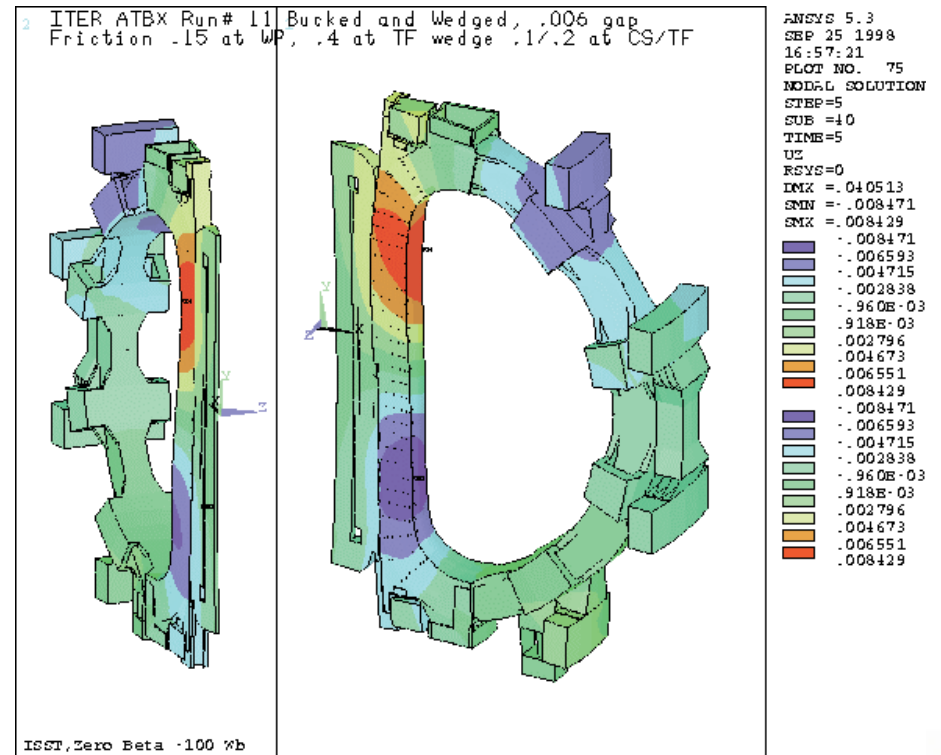
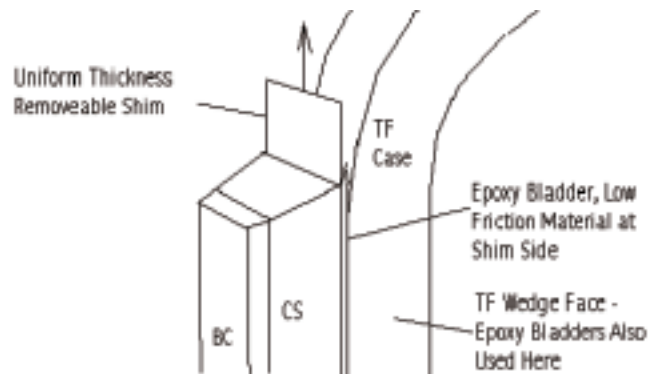


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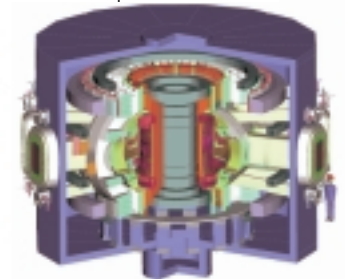
Advanced Structural Concepts for Global Machine Behavior

Bucked and Partially Wedged - ATBX -  
 FDR ITER concept with partial  
 wedging to control CS torsion.



**IpA/R ATBX was 12 % higher than ITER**

OOP displacements of the toroidal field coil are imposed on CS. Torsional shear stress in the CS is reduced by partially wedging the TF case. Set gap obtained with inflatable and removable shims.





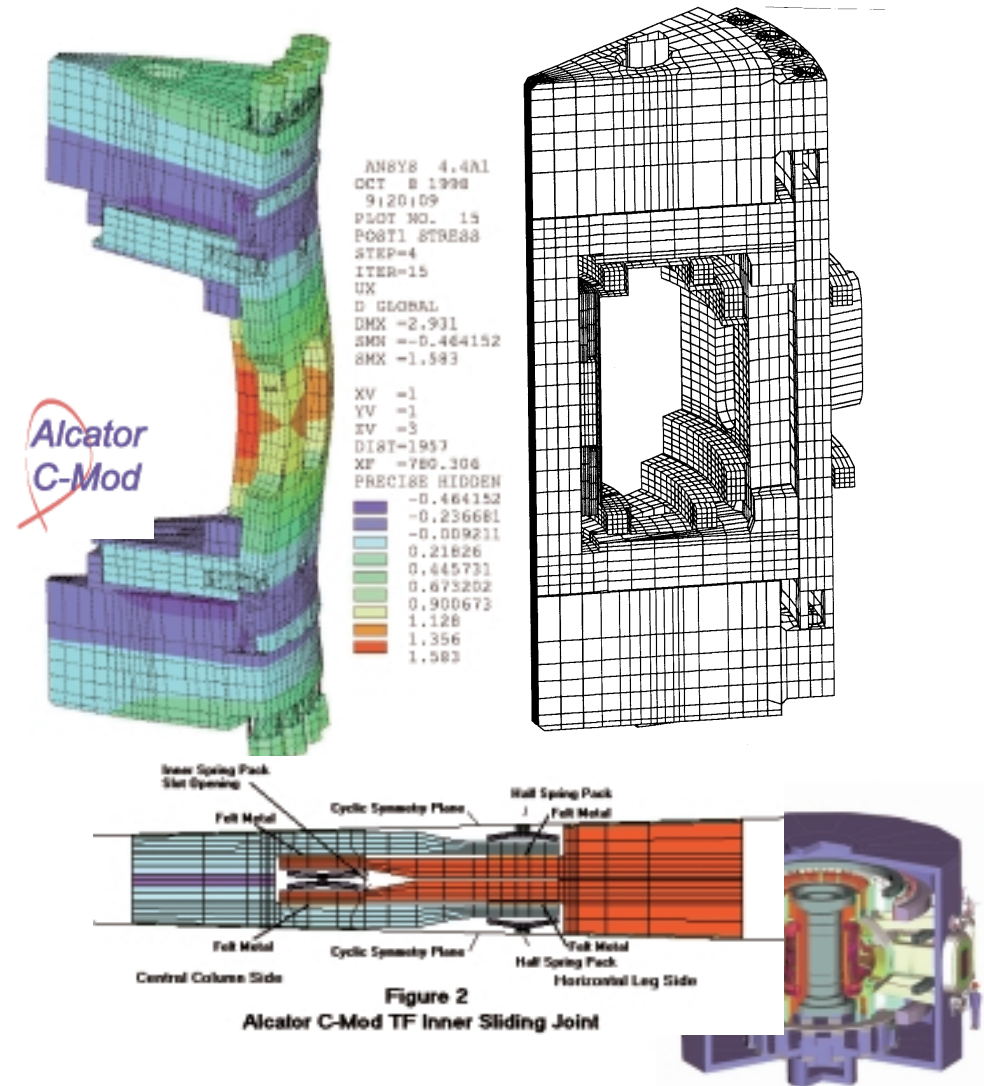
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Advanced Structural Concepts for Global Machine Behavior

Sliding Joint Picture frame TF Coils.  
 (NSO C-Mod Scale-up Studies)  
 (Ron Parker Proposed Steady Burn Experiment, SBX)  
 The in-plane behavior of the Inner Leg of C-Mod is structurally decoupled from the rest of the machine.

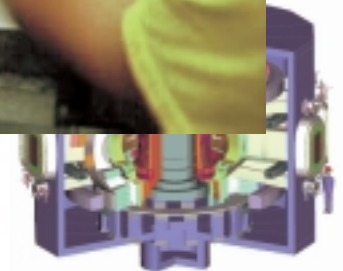
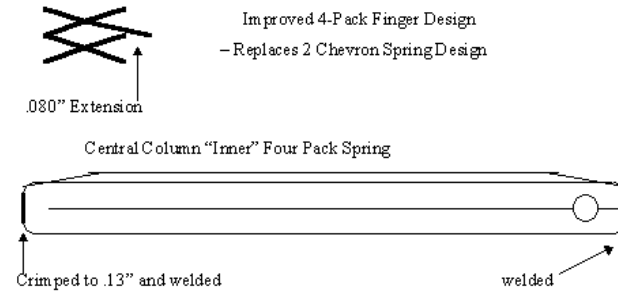
Upgrade to 2.5 MA planned  
 Original 3.0 MA design  $I_p A/R = \text{FIRE}$





## TF Finger Spring Upgrade

- Felt Metal was degraded
- Failure Analysis Yielded no Clear Cause
- Increased Spring Plate Pressure and Extension Improved FM Contact
- “4 Pack” Replaced “2 Pack”
- C-Mod has Worked OK Since







# Conclusions-I

1)  $I_p A/R > 15$  MA/m tokamaks appear available for BPX's

- not yet demonstrated x factor of 2, C-Mod can come close
- superconducting tokamaks need to catch up

2) Key to high  $I_p A/R$  to tokamaks is topology, not materials

Buck-wedge, Compression Rings, Magnetic Press, Scarf Joints, Sliding-Joints, Subcooling

3) Beyond Ignitor and C-Mod?

- Ignitor topology highly optimized - but possible extension to 30-370 K
- Further optimization of C-Mod topology possible

