Science and Technology Issues and Opportunities for a Burning Plasma Science Experiment

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Science and Technology Considerations for a BPSX*

- Foreseeable near-term BPSX's will be tokamaks
- Plasma performance (nTτ) significantly above that achievable in present tokamaks is required
 - Enhanced or new technologies are required
- This presentation examines several key generic BPSX requirements and the resulting 'BP' technology needs
- A BPSX can also provide a unique stimulus/opportunities to develop and test generic future MFE technologies

*generic Burning Plasma Science Experiment



Selected Topics and Organization

- High-field/long-pulse TF and PF magnets
- PFCs: power loading and pulse duration, T-retention and disruption resistance/tolerance (also Session 1)
- BP-compatible/enabling H/CD (also Session 2)
- AT-enabling H/CD, etc. (Session 2)
- BP- and AT-compatible diagnostics (Session 5)

Framework for Consideration:

BP Science Ops

Science — BP Technologies

Fusion Tech Ops



Acknowledgements and Cautions

- The analyses presented here are supported by General Atomics internal funding: opinions expressed are those of the author alone
- Methodologies adopted derive from a long succession of [would-be] first-of-kind burning plasma experiments: INTOR, FED, ITER-CDA, ITER-EDA, CIT, BPX,
- Qualitative parameters are based on public-accessible machine concept data and do not necessarily constitute a fully accurate or equivalent comparison basis. Small distinctions among concepts in computed parameters are not necessarily meaningful
- Don't attempt BPSX comparisons like this at home, at least without taking adequate protective measures!



BP Regime Access Requirements

- Maximum $\langle n \rangle \langle T \rangle \tau_E$ in tokamaks increases approximately as $(I^*A)^2$
- Stellarator and [sparse] ST data fall on the same scaling (and hence tend to confirm the A dependence of the tokamak scaling, which spans a range A = 2.5 - 5)
- There are factor-of-2 variations (±) among the tokamak data (profiles, other significant parameters, optimization,). IA is not the <u>only</u> performance predicting parameter
- BP regime (Q ~ 10) typically requires $\langle n \rangle \langle T \rangle \tau_E \ge 2.4 \ x \ 10^{21} \ m^{-3} \ keV s$ (varies owing to assumptions about profiles, impurities, self-consistent He,)
- BP requires IA ≥ 30 MA (eg. ≥ 10 MA at A = 3; cf. JET-EFDA IA = ~12 MA)
- IA \ge 40 MA provides modest margin; IA \ge 60 MA yields 'ignition' (Q \ge 25) and/or a 'reactor-prototype' device





Magnet and shielding requirements set BPSX size



• Minimum size and A are also constrained by OH solenoid requirement



High B_{max}, Low A and No Shielding Yield Smallest R₀



• B_{max} ≥ ~16 T pushes to (or above) 'pure-Cu' stress limit



Pulse Duration (with inductive/OH current drive)

- Compact inertially-cooled designs are thermal and OH-limited
- Larger designs with steady-state TF are OH-limited (OH V-s swing)
- Absolute pulse duration increases strongly with R_o, but confinement-normalized duration increase is ~ 10-x weaker:







BPSX Magnet Technology Summary

- A variety of resistive (copper) and superconducting (SC) magnet technologies to support Q \ge 10 BPSX's have been identified
- Concepts separate into two categories based on TF magnet cooling (inertial or steady-state) and at-magnet peak field:
 - 1) cryo-precooled copper (typically with some alloying), inertially cooled, with 15-22 T peak fields, or
 - 2) steady-state resistive pure copper or SC, with peak fields 10-12 T
- Machine size (R₀) decreases strongly with higher B_{TF} and/or weakly with lower A. But OH requirement sets a limit on minimum A
- TF structural limitations apply to all concepts and are important configuration drivers, especially for compact designs
- For both inertial and steady-state concepts, OH solenoid flux swing sets an V-s limited plasma current/burn duration
- For compact inertial-Cu designs, TF thermal and OH duration limits are similar; for steady-state TF designs, OH duration limit sets burn duration
- Reliable magnet operation will be critical: all BPSX designs will require essentially full-field, full-current operation (for ??? pulses)
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BPSX Plasma Facing Component Requirements

- A BPSX will require a larger scale (size and/or field strength) and higher power (aux + alpha) device than the largest present tokamaks. PFCs, VVs, etc. will also be exposed to significant volumetric neutron heating
- Increase in 'scale' and plasma power (plus neutron heating) results in an increase in the effective plasma wall loading P_{th}/A_{FW} and also in the plasma specific energy W_{th}/A_{FW}
- These increases plus the effects of neutron irradiation on material and structure properties and PFC maintenance impact BPSX PFC selection, design and operation planning
- In addition, BPSX PFC's *must* be selected to minimize T retention (in co-deposited layers). Use of carbon may be constrained or prohibited
- Finally, in almost all cases, BPSX primary PFCs will operate in thermal steady state and require active cooling. Provision will also be needed to replace eroded or damaged PFCs on a regular basis



BPSX PFC Parameters (Estimated)

- A BPSX requires a larger scale (size and/or field strength) and higher (aux + alpha) power device than the largest present tokamaks
- PFC 'steady-state' power/area (MW/m²) and disruption energy (MJ/m²) are appreciably higher than in present 'long-pulse' (~10 s) tokamaks:

Device	ITER-FDR	ITER-FEAT	FIRE-10T	FIRE*-10T	IGNITOR	M-Cu-10
Α	2.91	3.10	3.81	3.60	2.81	3.16
I (MA)	21.0	15.2	6.6	7.7	11.5	15.0
R _o (m)	8.14	6.20	1.98	2.15	1.32	5.00
P _{fus} (MW)	1500	410	150	150	180	325
Ρ _α (MW)	300	82	30	30	37	65
P _{aux} (MW)	0	40	15	15	18	33
P_{tot}/A_{wall} (MW/m ²)	1.19 ^(a)	0.61	2.4	1.9	5.0	0.94
P/A _{div}	39 ^(b)	21	24	22	44 ^(c)	27
W _{th} (MJ)	1100	325	27	35	~10	235
W_{th}/A_{div} (MJ/m ²)	70	28	7.2	8.5	4.0	25

(a) Basis: total power = neutron + alpha + auxiliary, uniformly spread over first wall

(b) Basis: 0.67*(alpha + aux) power to divertor; 10-x SOL expansion; SOL = 0.01 m (R ind.)

(c) Basis: same divertor geometry and SOL as others: design is with a limited plasma





BPSX Divertor Thermal and Disruption Loadings

- <u>Thermal loading</u>: present BPSX's except IGNITOR(div)] have 'raw' (without radiative mitigation) power loadings ~25 MW/m² (ITER-EDA R&D goal/achievement)
- All BPSX's will need radiative PFC power mitigation for 'routine' operation ($P_{div} \le 10 \text{ MW/m}^2$)
- <u>Disruption loading</u>: all BPSX's have 'raw' (without plasma shielding) divertor loadings ≥ 10-x PFC surface vaporization threshold. Disruption-affected PFC's will be consumable components. Disruption avoidance (frequency reduction) is needed; will pay off!



BPSX Auxiliary Heating and Current Drive

- All BPSX's will require, provide substantial auxiliary heating/CD
- Port power density ($A_{port} \le 0.05 A_{wall}$) increases with decreasing R_0





BPSX Auxiliary Heating and/or Current Drive

• H/CD selection and installed power mix (or possibly installable mixes) varies among BPSX candidates; constrained by H/CD technologies, plasma access and parameters and H/CD cost(s)

Device	ITER-FDR	ITER-FEAT	FIRE-10T	FIRE*-10T	IGNITOR	M-Cu-10
R _o (m)	8.14	6.20	1.98	2.15	1.32	5.00
$P_{aux} (Q = 10) (MW)$	NA	40	15	15	10-20	40 (~FEAT)
Install'd P _{H/CD} (MW)	100	70 (100)	45?	55	10-20?	70 (?, ~FEAT)
NI-NBI (tang) (MW)	50	33	???	???	NA	40 (~FEAT)
PI-NBI (⊥)						???
ICRF	50 ^(a)	20 ^(b)	30	30	10-20	~FEAT
LHRF (MW/m ²)	50 ^(a)	0 ^(b) (20)	15?	25	?	~FEAT
ECRF	50 ^(a)	20 ^(b)	NA	NA	NA	~FEAT

(a) maximum option; final mix in addition to NBI TBD

(b) initial selection; other options added later

- High-field/compact candidates: ICRF with LHRF option/addition; NBI or EC likely 'not applicable'; port power densities higher for all
- Low-field: NBI with ICRF/LHRF/ECRF options/additions; lower port power densities and/or more available ports/mix options



Summary (Objective)

- BPSX feasibility and cost-effectiveness depends on three key technologies: HP-magnets, HP-PFCs, and magnet/concept-compatible H/CD
- Magnet technology is the concept driver. Options has been identified and design concepts have been correspondingly optimized to address various embodiments of the basic Q = 10 'BPS mission'. All proposed magnet technologies have been or likely can be shown to be 'feasible'
- There is a correlation among TF cooling (inertial or steady-state) and peak field (10 -22 T), device major radius and energy-confinement-normalized fusion burn duration. Smaller (larger) designs trade compactness (cost) for increasingly longer normalized burn duration. In the large device category, both SC and steady-state resistive Cu options with similar OH-limited burn duration are feasible.
- Divertor PFC power loadings and vaporization-energy normalized disruption loadings are similar and equally challenging across the whole spectrum of BPSX's. T-retention will constrain material choices
- Choice of peak/plasma TF field determines H/CD options/mix. Compact high-B options focus on IC and LH; larger low-B options can also accommodate NI-NBI and ECRF and typically also allow a 'cafeteria' mix of the four possible H/CD candidates. Long-pulse/ss 'sources' are needed



Conclusions and Opinions

- Fusion science needs fusion technology (and vice-versa)
- Fusion technology is [close to being] ready for a BPSX
- But the challenges are great, and we must not lose sight of the fact that the scientific success of a BPSX will hinge critically on the achievement of adequate performance of *all* of its enabling technologies
- Conversely, given success with these enabling technologies, and then success with the ensuing plasma science, fusion will, for the first time, have a means to achieve routine production of copious amounts of fusion power, and to begin exploring the *real* challenges of fusion energy

"It is far better to light just one small BPSX than to curse the darkness."

