### Development in the DIII-D Tokamak of Hybrid Operations Scenarios for Burning Plasma Experiments

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**General Atomics** 



- Baseline scenarios for burning plasma designs such as ITER and FIRE are based largely on projections from multi-machine databases. It is important to verify the scenarios in present day devices in stationary discharges and probe the limits in these conditions
- ITER specifically has an additional reduced-performance scenario for increasing the neutron fluence ("hybrid" scerario). It is important to assess the physics capabilities of the design for this mission
- Extension of present regimes to the current relaxation time scale may uncover new phenomena; for example, slow relaxation oscillations in Tore Supra

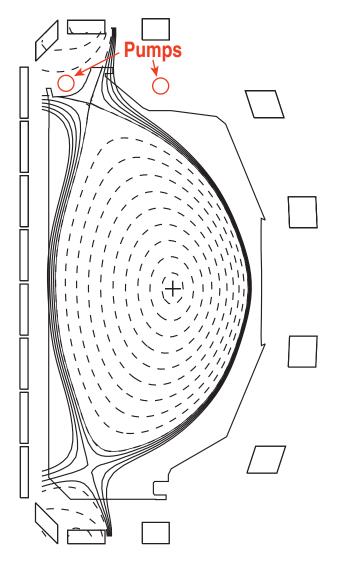


- In the mid-1990's, enhanced discharges with q<sub>min</sub> ~1 but limited by fishbones rather than sawteeth were found. These were not pursued because they could not be projected to fully non-inductive operation [B.W. Rice, et al., Nucl. Fusion <u>39</u>, 1855 (1999)]
- In 2000, a stationary scenario was developed for testing ECCD in enhanced performance plasmas. By controlling β and density, it was found that β<sub>N</sub> = 2.7, q<sub>95</sub> = 4.2 discharges could be run for > 6s without sawteeth [T.C. Luce, et al., Nucl. Fusion 41, 1585 (2001), M.R. Wade, et al., Phys. Plasmas <u>8</u>, 2208 (2001)]
- In 2001, it was found that these discharges could be pushed to  $\beta_N > 3$  if the  $\beta$  is raised after the current profile is relaxed [T.C. Luce, et al., Nucl. Fusion, <u>43</u>, 321 (2003)]
- In 2002, based on results from AUG, JT-60U, and DIII–D, the Steady State Operation topical group and the Transport topical group independently requested that DIII–D and other tokamaks map the performance as a function of q<sub>95</sub> and density, and note the instability which limits the current peaking



### **KEY ELEMENTS**

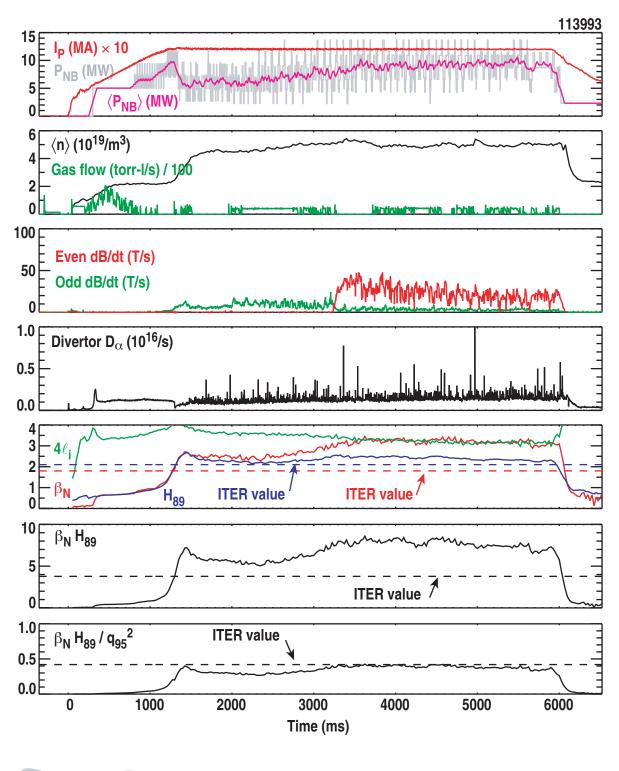
- Density control requires pumping and gas puffing to remove the wall from the particle balance. For DIII–D, this means controlling the shape to keep the pumps engaged and only the upper x point active
- β control requires real-time feedback on the neutral beam injection power.
  Feedback is PD with a target duty cycle. A model-based controller is needed to improve the robustness.
  To eliminate the errors from shot-to-shot jitter in the L-H transition timing, the feedback is triggered when the stored energy reaches a preset level



 The essential operational element appears to be reaching high enough β to trigger the m=3/n=2 tearing mode, then waiting for the current profile to relax before raising β further

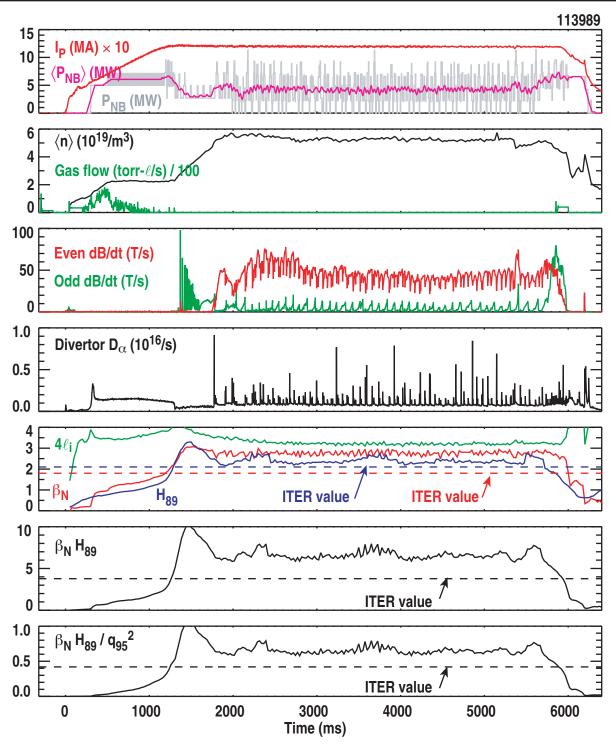


## DISCHARGE WITH q95 = 4.4 RUNS STABLY NEAR THE NO-WALL $\beta$ LIMIT FOR >2s



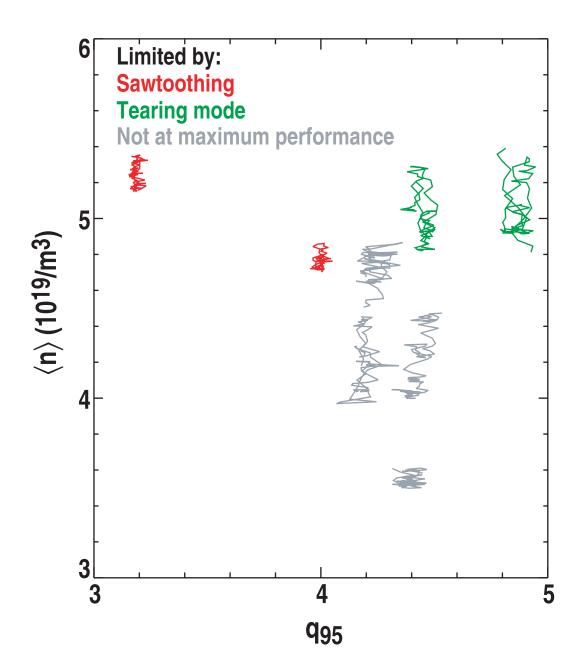


### DISCHARGE WITH q<sub>95</sub> = 3.2 RUNS WELL ABOVE ITER BASELINE VALUES FOR > 3s

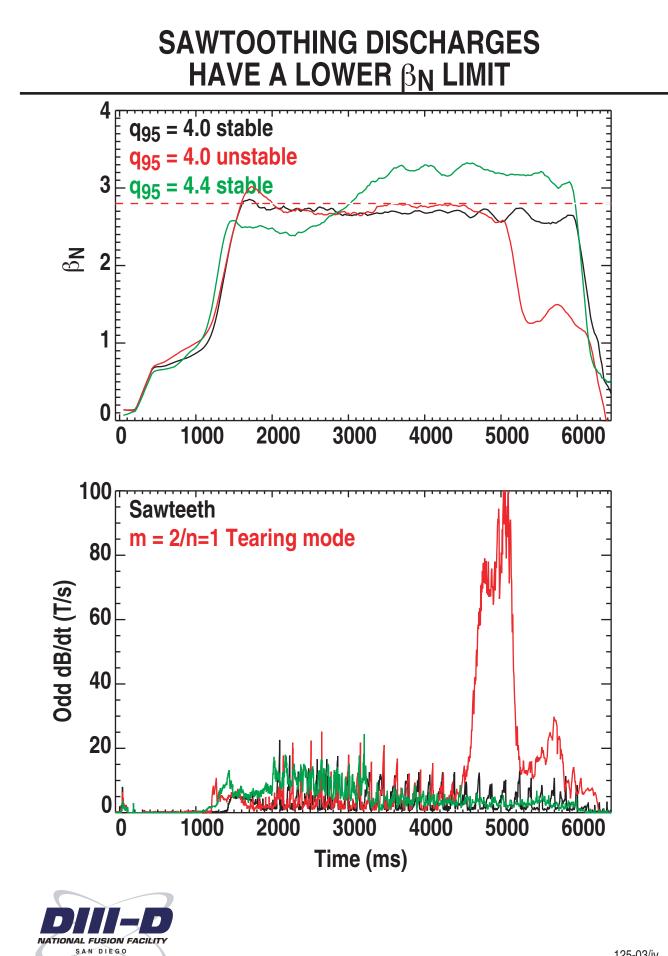




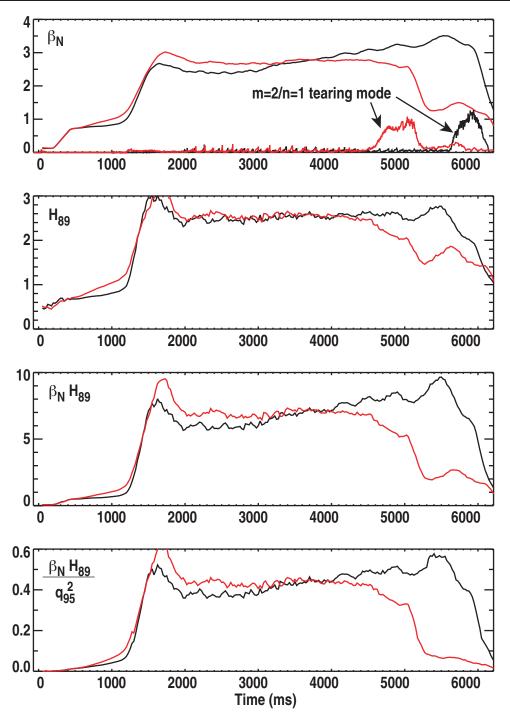
## CURRENT PEAKING IS LIMITED BY SAWTEETH FOR $q_{95} \le 4$ AND TEARING MODES FOR $q_{95} > 4$





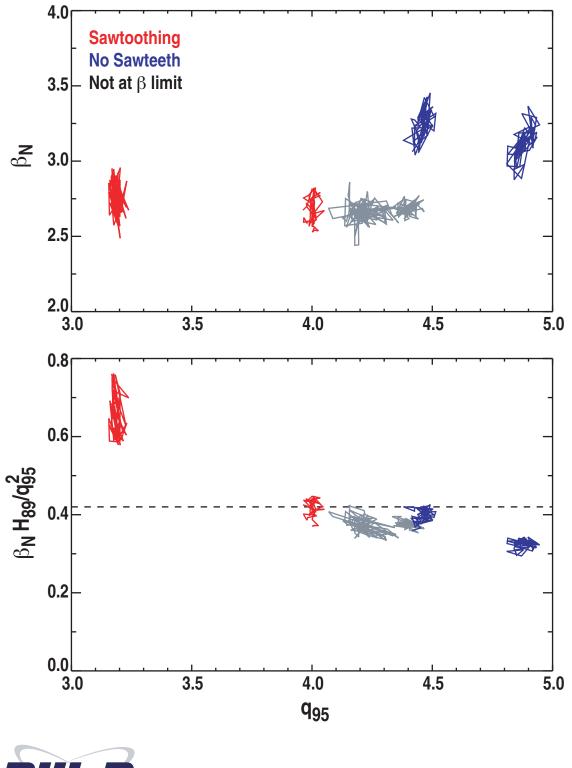


# LONG-PULSE OPERATION IS IMPORTANT BECAUSE HIGHER $\beta_N$ CAN BE OBTAINED UNDER NON-STATIONARY CONDITIONS



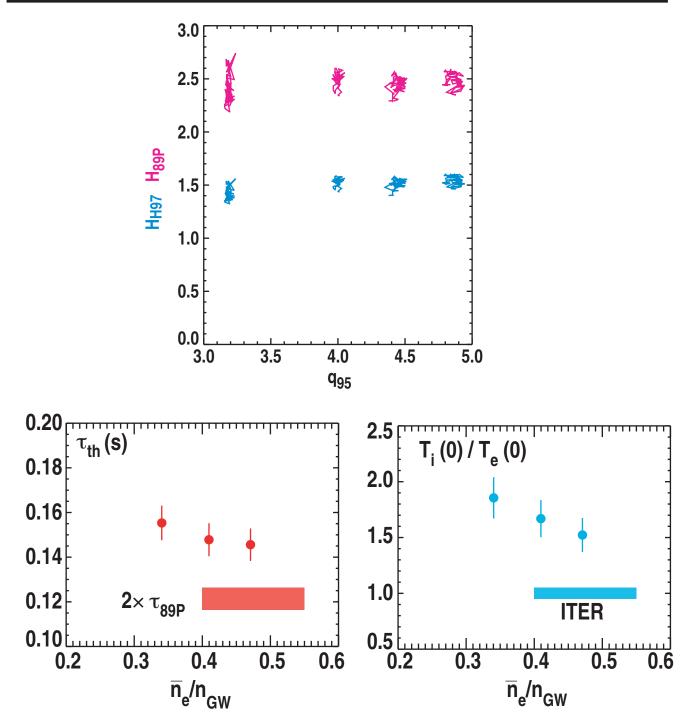


### β<sub>N</sub> LIMIT IS NEARLY INDEPENDENT OF q<sub>95</sub> IN EACH REGIME, BUT FUSION PERFORMANCE MAXIMIZES AT THE LOWEST q<sub>95</sub>





# CONFINEMENT ENHANCEMENT IS ROUGHLY INDEPENDENT OF $q_{95}$ and weakly dependent on $T_{e}/T_{i}$





### **METHODOLOGY FOR PROJECTION TO ITER/FIRE**

- Fixed poloidal cross section
- Fixed q<sub>95</sub>
- Fixed  $\beta_N$
- Fixed confinement multiplier H (but 3 scalings)
- Choose  $n/n_G$  (fixed  $v_*$  would be  $n/n_G > 2$ )
- Use machine's Z<sub>eff</sub> prescription:
  - ITER: 2% Be 1.2% Carbon
  - FIRE: Z<sub>eff</sub> = 1.4 (maybe 3% Be need to check)
- He ash self-consistently used
- Choose 50/50 D-T, mix
- Use thermal heating scheme (no beam-target fusion reactions)
- Use DIII–D n<sub>e</sub>, T<sub>e</sub> profiles
- Fix  $T_e = T_i$



### **PROJECTION OF 113993 TO ITER**

q <sub>95</sub> = 4.4	β <mark>N = 3.2</mark>	n/n <sub>G</sub> = 1	min ∿ <sub>*,i</sub> = 0.02	26		
B = 5.3 T	I = 10.3 MA	$\alpha_{n}$ = 1.38	$\alpha_{T}$ = 1.93			
Flattop time	= 4500s = 1.25h					
	н	P <sub>fus</sub> (MW)	P <sub>aux</sub> (MW)	Q <sub>fus</sub>		
ITER89P	2.2	670	165	4.1		
IPB98y2	1.58	650	64	10.2		
Pure gB	1.45 (1.61)	630	0	$\infty$		

ITER89P: P.N. Yushmanov et al., Nucl. Fusion 30, 1999 (1990) IPB98y2: ITER Physics Basis Editors, et al., Nucl. Fusion 39, 2137 (1999)

Pure gB: C.C. Petty, et al., Fusion Sci. Tech. 43, 1 (2003)

Numbers in parenthesis are the values for the DIII–D case. The confinement multiplier must be reduced in the ignition cases to obtain energy balance



### **PROJECTION OF 113989 TO ITER**

q <sub>95</sub> = 3.2	β <mark>N = 2.8</mark>	n/n <sub>G</sub> = 1	$\min v_{*,i}$ =	= 0.047
B = 5.3 T	I = 13.9 N	IA $\alpha_n = 1.25$	α <b>τ</b> = 1.92	2
Flattop ti	me = 1900s	> 30 min		
	н	P <sub>fus</sub> (MW)	P <sub>aux</sub> (MW)	Q <sub>fus</sub>
ITER89P	2.4	950	31	31
IPB98y2	1.34 (1.47)	940	0	$\infty$
Pure gB	0.99 (1.63)	940	0	$\infty$



q <sub>95</sub> = 3.2	β <b><sub>N</sub> = 2.8</b>	n/n <sub>G</sub> = 0.7	min $v_{\star,i}$ =	0.062				
B = 10 T	I = 6.3 MA	$\alpha_{\sf n}$ = 1.25	α <b><sub>T</sub> = 1.92</b>					
20s flattop needs 30 Volt-seconds								
	н	P <sub>fus</sub> (MW)	P <sub>aux</sub> (MW)	Q <sub>fus</sub>				
ITER89P	2.4	280	48	5.8				
IPB98y2	1.47	280	35	8.0				
Pure gB	1.55 (1.63)	270	0	820				

A potential advantage of the high field approach is high  $Q_{fus}$  with  $n/n_G < 1$ 



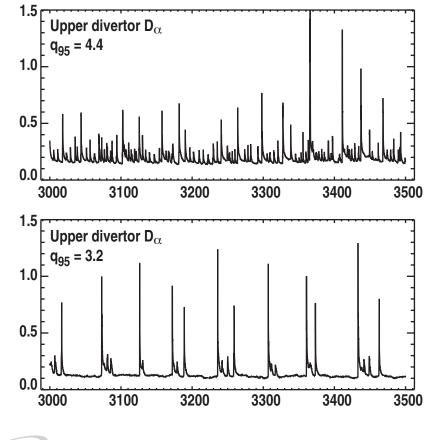
### **REMAINING PHYSICS ISSUES FOR PROJECTION**

#### Confinement dependence on T<sub>e</sub>/T<sub>i</sub>

- Need density scans at fixed q<sub>95</sub> however, H seems independent of this parameter in present range of density, so dependence may be weak
- Physics of current profile evolution at high q<sub>95</sub>
  - Need good stationary data at low density to get ECE data. The main questions are whether there is dynamo-like action in the tearing mode and does it require a fluctuating amplitude?

#### Divertor issues

 Lower current means lower absolute density which may place greater strain on the divertor. Perhaps the ELM behavior is better at higher q<sub>95</sub>





- Stationary high-performance discharges in DIII–D provide confidence that ITER and FIRE can meet and exceed their baseline performance
- Based on the DIII–D dischanges at higher q<sub>95</sub>, ITER could match baseline performance with an inductive capability of > 4000s operation for its nuclear testing mission
- The variance in the confinement projections points to the need for data from JET and JT-60U to reduce the uncertainties
- Physics studies involving multiple machines are necessary to validate any conclusions on the remaining physics issues

