SUSTAINMENT OF PLASMA ROTATION BY ICRF

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OUTLINE

- Background and Motivation
- Representative Experimental Results
- Model Overview
- Angular Momentum Diffusion Equation
- ICRF Model and Torque Density
- ORBIT Code and Collision Upgrade
- Non-Dimensional Rotation Velocity
- Diamagnetic Scaling of Rotation Velocity
- Parameter Studies
- Resonant Surface Scan for Alcator C-Mod
- Conclusions

BACKGROUND AND MOTIVATION

- Alcator C-Mod and JET observe development of co-current plasma rotation in ICRF-heated discharges.
- ICRF heating introduces zero (or negligible) angular momentum to the plasma.
 - Experiments have a symmetric \mathbf{k}_{\parallel} spectrum and contribute no net angular momentum.
 - Even if the k_{\parallel} spectrum lauched is one sided, the angular momentum input is small $(k_{\parallel}=n/R \; ; \; n \; 12 \; for \; C\text{-Mod})$

$$\begin{pmatrix} T \end{pmatrix}_{RF} = RF \text{ Torque } = M \quad v_{\parallel} R = n \quad E /$$

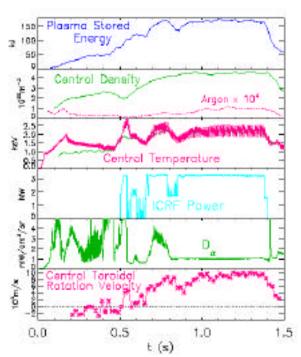
$$\begin{pmatrix} T \end{pmatrix}_{NBI} = typical \text{ NBI torque } = E R \quad v_{beam}^{-1}$$

$$\frac{T_{RF}}{T_{NBI}} = \frac{n \quad v_{beam}}{R} \quad \frac{1}{15} < < 1$$

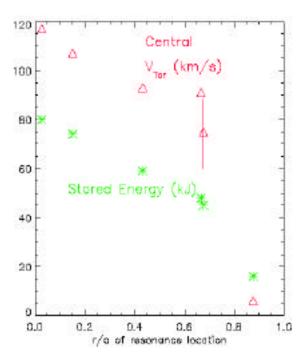
• What is the mechanism for developing toroidal rotation and how does it scale?

REPRESENTATIVE EXPERIMENTS

1. Paper by J. E. Rice, et al. [Nuclear Fusion 39 (1999) 1175] reports rotation observations and scaling.



5.7 T, 1.0 MA D(H) Discharge

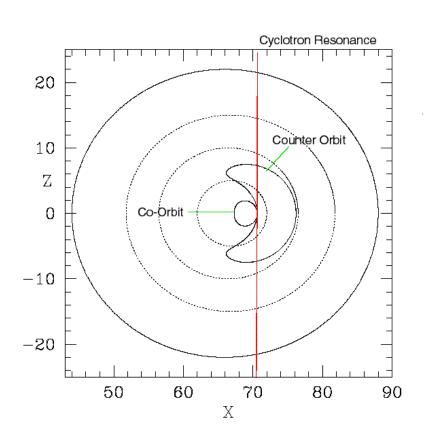


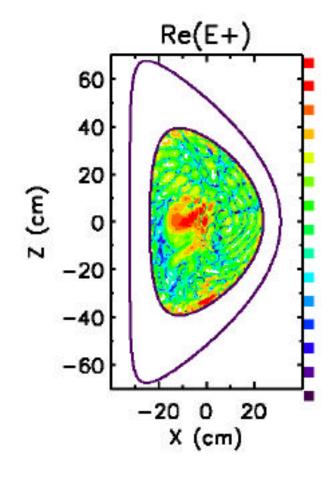
Resonance location scan with B varying and $q_{95} = 4.7$

MODEL OVERVIEW - 1

- 1. Even though ICRF heating introduces no net torque, there remains the possibility of creating positive and negative torque density regions.
- 2. Describe plasma response to torque density by an angular momentum diffusion equation.
 - Separated torque density regions lead to finite central rotation
- 3. Model ICRF heating by the introduction of energetic particles and the removal of an equal number of cold particles.
 - Particles are introduced at a particular flux surface the resonance location— with equal numbers of co- and counter- velocities so there is no angular momentum input.
 - Two ICRF models detailed below.

REPRESENTATIVE INITIAL ORBITS





(Plot by P. Bonoli)

• Fast-wave refraction leads to midplane heating.

MODEL OVERVIEW - 2

- 4. Follow particles by ORBIT with ion-ion pitch angle and drag collisions
 - Record particle's flux-surface when energy \rightarrow 0.
 - Particle's displacement from originating flux-surface drives a radial neutralizing current and a $j_r B$ R torque density in the background plasma
 - Continuous creation of energetic particles drives steady j_r current
 - ORBIT also computes the torque density imparted to the background by energetic-ion collisions
 - Total volume-integrated applied torque vanishes to 2·10-4 accuracy.
 - Torque arsing from particle loss imparts counter-current rotation
- 5. Compute non-vanishing central rotation from torque density
- 6. Investigate scaling of central rotation and sensivity to initial conditions
 - Particle energy and pitch, resonance location and q.

ANGULAR MOMENTUM DIFFUSION EQUATION-1

1. General Form of angular rotation rate Ω response to torque density τ

$$-\frac{1}{t}\left(M n R^{2}\right) = \nabla \cdot \left\{n M R^{2} \mid_{M} \nabla\right\} +$$

2. Steady-state axisymmetric version

$$\frac{1}{V} - \left\{ V \left\langle n M R^2 \right\rangle \right\} = - \left\langle \right\rangle$$

$$V = \oint \frac{d\ell 2 R}{d\ell 2 R} = V$$
 and <> denotes magnetic surface average

- 3. $\langle \ \rangle$ is torque density on bulk plasma and has two sources:
 - $j_r B_\theta$ torque arising from radial curents which neutralize energetic particle displacements
 - Collisional Angular momentum transfer from energetic particles.

ANGULAR MOMENTUM DIFFUSION EQUATION-2

4. First integral of angular momentum equation

$$V \left\langle n M R^{2} \right\rangle_{M} \left(\right)^{2} \right\rangle_{M} = -\int_{0}^{\infty} \left\langle \right\rangle V d = T()$$

- T() = torque exerted inside ψ -surface
- No net torque condition: $T(\psi_{max}) = 0$
- 5. Apply no-slip boundary condition at surface
 - Field lines outside separatrix line-tied to vessel; toroidal rotation not permitted
- 6. Torque proportional to rate of creation of energetic particles \dot{N} and angular momentum transferred per particle.

ANGULAR MOMENTUM DIFFUSION EQUATION-3

7. Angular rotation rate (use toroidal flux as independent variable)

$$() = \int_{-\infty}^{\infty} \frac{d}{q V} \frac{T()}{\langle n M R^{2} |_{M} ()^{2} \rangle}$$

8. Conclude:

For regions of separated postive and negative torque density, $T(\Phi)$ is non-zero and toroidal rotation can develop, even though the total torque $T(\Phi_{max})=0$

ION-CYCLOTRON HEATING: MODEL 1

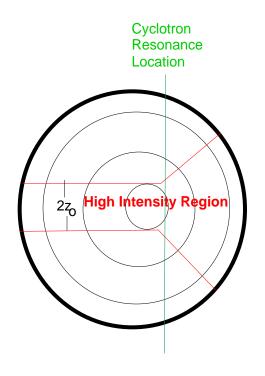
- 1. The ion-cyclotron heating process changes a particle's prependicular energy, while leaving v_{\parallel} and the canonical angular momentum unchanged.
 - No net angular momentum is introduced
- 2. Our ICRF models replace cold particles by energetic particles constrained to have an equal number of co- and counter velocity particles.
 - ICRF Model 1 creates particles at interesection between midplane and cyclotron resonance surface. Pitch is low: $v_{\parallel}/v = (0.25 0.40)$

Mimics ICRF heating for particles with orbits tangent to the resonant surface at the midplane where wave intensity is high.

- 3. Energetic particles then spatially diffuse via banana diffusion and collisionally transfer angular momentum to the bulk plasma.
 - ORBIT code follows these processes via a Monte Carlo approach.

ICRF MODEL 2

• Creates particles at banana tips $(v_{\parallel}=0)$ distributed along cyclotron resonance surface in region of high wave intensity: $-z_{max} \le z \le z_{max}$



• Distribution with z weights midplane creation:

$$\frac{dN}{dz} = \frac{\left(z_{max}^{2} - z^{2}\right)}{z_{max}^{2} \left(2z_{max}^{2} - z^{2}\right)^{1/2}}$$

• Again, ORBIT code follows subsequent spatial diffusion and collisional angular momentum transfer.

ORBIT CODE

- 1. ORBIT code has been developed to follow energetic particle orbits in toroidal confinement geometries of arbitrary cross section.
- 2. Hamiltonian formalism developed
 - Rigorous Hamiltonian form found:
 - R. B. White and M.S. Chance, Phys. Fluids 27, 2455 (1984)
 - R. B. White, Phys. Fluids B2, 845 (1990)

$$dP /dt = -H /$$
 $d /dt = H / P$
 $dP /dt = -H /$
 $d /dt = H / P$

- 3. Monte- Carlo collisions after A. Boozer et al. Phys. Fluids 24, 851 (1981)
- 4. Collision model: Energetic proton ion-ion collisions with cold deuterons.

$$\frac{d\left\langle \begin{array}{c} ^{2}\right\rangle }{dt} \; = \; _{o}\left(\frac{E_{o}}{E}\right)^{3/2} \quad \frac{1}{E} \; \frac{dE}{dt} \; = - \; _{o}\left(\frac{E_{o}}{E}\right)^{3/2} \; \frac{M_{\,proton}}{M_{\,deuteron}} \qquad \qquad _{o} \; = \frac{2^{\,3/2} \quad n \; e^{\,4} \; \ln n}{\left(M_{\,p}\right)^{1/2} \; E_{o}^{\,3/2}} \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; \ln n} \right) \; = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2}\right)^{1/2} \; E_{o}^{\,3/2} \; e^{\,4} \; e^$$

ORBIT CODE MODIFICATIONS

- Plasma divided into 5.104 bins in toroidal flux (magnetic surface label)
- For each time step, momentum transfer from particles to plasma through pitch angle scattering and drag recorded in each bin.
- Final particle momentum and density recorded in each bin
- Integrals over toroidal flux (bins) needed for angular rotation performed
- Angular momentum check accurate to 1 part in 5000.

NONDIMENSIONAL CENTRAL ROTATION RATE-1

1. Let Φ_0 denote the toroidal flux value where energetic particles of energy E are introduced at a rate \dot{N} .

- 2. Let $v = (2E/M)^{1/2} (aR_a)^{-1}$ denote a nondimensional particle speed.
- 3. ORBIT computes $F(\Phi)$ = fraction of particles ending up inside flux surface Φ and the integral T_1 of the $j_r \times B$ torque.
 - Φ_0 is flux surface of creation for Model 1.

$$T_1(\) = \frac{1}{V} \int_0^{\infty} \frac{d}{q} G(\) \qquad G(\) = \begin{cases} F(\) \\ F(\) - 1 \end{cases}$$

NONDIMENSIONAL CENTRAL ROTATION RATE-2

4. For Model 2, with a distribution of initial flux surfaces, the generalization is:

$$F = \frac{1}{N}_{k=1}^{N} F_{k}$$
 $G = \frac{1}{N}_{k=1}^{N} G_{k}$

where F_k , G_k can be expressed in terms of the Heavyside function Θ

$$F_{k} = \begin{pmatrix} & - & \\ & & \end{pmatrix} \qquad G_{k} = \begin{pmatrix} & - & \\ & & \end{pmatrix} \begin{pmatrix} & \\ & & \end{pmatrix} - \begin{pmatrix} & \\ & & \end{pmatrix} - \begin{pmatrix} & \\ & & \end{pmatrix} \begin{pmatrix} & - & \\ & & \end{pmatrix}$$

- ko denotes the creation flux surface for the kth Monte Carlo particle
- 4. ORBIT also calculates v $T_2(\Phi)$ = mechanical angular momentum deposited inside Φ .

NONDIMENSIONAL CENTRAL ROTATION RATE-3

5. Standard circular tokamak formulas, an assumed constant momentum diffusivity $\chi_M=a^2/6\tau_M$, and $\dot{N}E\tau_E=P\tau_E=W$ are employed to calculate the central rotation frequency

6. On-axis rotation rate is expressed in terms of the nondimensional rotation rate I^*

$$\frac{(0)}{\dot{N}} = v^2 I^* \qquad I^* = \frac{1}{v} \int_0^{max} \frac{d}{d} T \qquad T = T_1 + T_2$$

$$v = \left(2E / M\right)^{1/2} \left(R_{a c,a}\right)^{-1}$$

7. Analytic considerations motivate the introduction of v so that I* is insenstive to physics parameters

ROTATION IN PHYSICAL UNITS

- 1. Select baseline initial particle values used in computing I* to be representative of Alcator C-Mod. Employ ICRF Model 1
 - E=48 keV, pitch = 0.25, rho = 0.165, low-field midplane, and N=2000.
 - Result:

$$I^* = 22.5$$

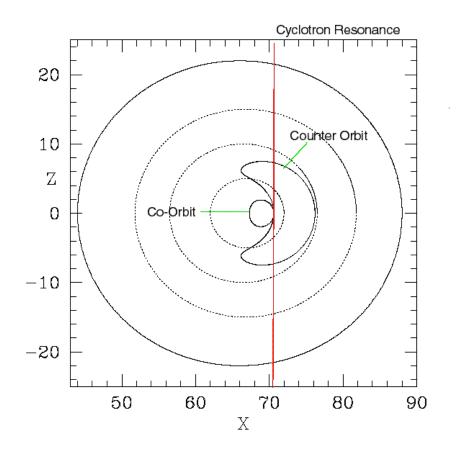
2. In physical variables the rotation rate is

(0) =
$$\left\{ \frac{6 \text{ W}}{\text{e B}_{\text{a}} R_{\text{a}}^{3} \text{a}^{2} \bar{\text{n}} (2)^{2}} \left(\frac{\text{M}}{\text{E}} \right) \right\} I^{*}$$

For the shot on sheet 4, this gives $v_{tor} = \Omega(0) R_a = 7 \cdot 10^4 \text{ m/s}$, in good accord with the reported value. Results insensitive to E, pitch, and N.

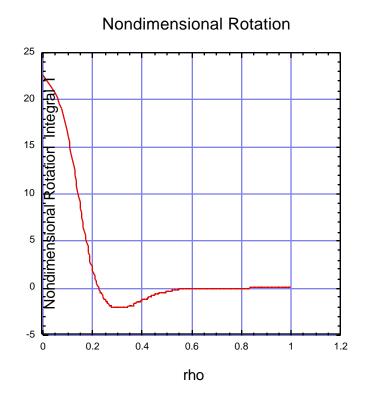
INITIAL ORBITS

1. Initial orbits are characteristic of orbits near the magnetic axis

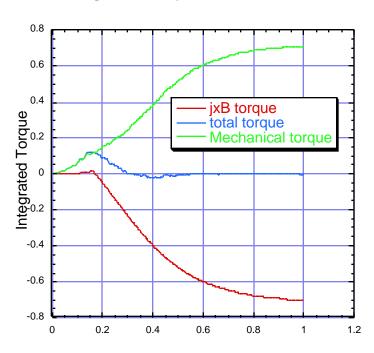


ROTATION AND TORQUE PROFILES - RUN 1

• Rotation Profile is peaked.



Integrated Torque Profiles - Run 1

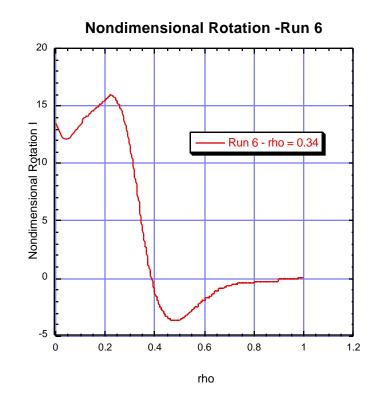


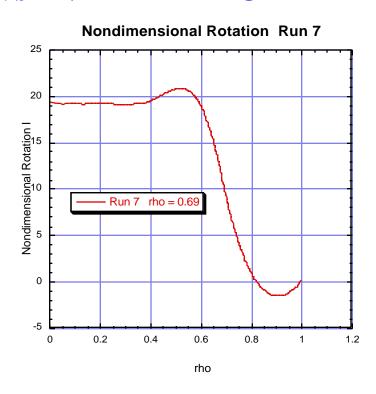
SENSIVITY STUDIES

• How much does the central rotation change as E, rho, pitch, q-profile, and initial surface (ICRF resonance surface) vary? Results expressed as I^* .

Run	Objective (N=500)	I *	rho	E (keV)	pitch	q _{max}	resonance
1	Baseline (N=2000)	22.5	0.165	48	0.25	4.0	LFS
1.1	Baseline (N=200)	24.9	0.165	48	0.25	4.0	LFS
2	Pitch variation	28.3	0.165	48	0.35	4.0	LFS
3	Energy dependence	24.6	0.165	24	0.34	4.0	LFS
4	HFS vs LFS (run 1)	-18.6	0.165	48	0.25	4.0	HFS
5	q _{max}	17.5	0.165	48	0.25	8.0	LFS
6	initial rho	13.5	0.34	48	0.5	4.0	LFS
7	initial rho	19.3	0.69	48	0.64	4.0	LFS
8	Banana vs	11.4	0.34	48	0.32	4.0	LFS
	Circulating (run 6)						
9	HFS vs LFS (run 7)	-22	0.69	48	0.64	4.0	HFS
10	On axis	7.3	0.0	48	0.35	4.0	On-axis
11	On axis - pitch	-1.9	0.0	48	0.25	4.0	On-axis

ROTATION CURVES vs INITIAL RHO



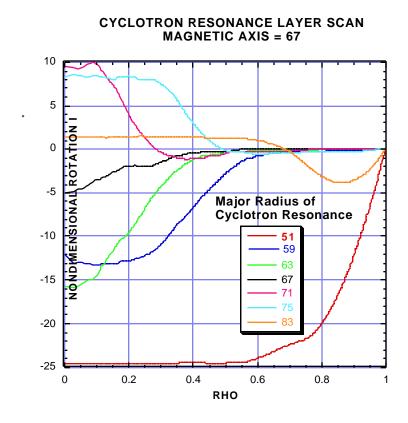


- As resonance layer is moved outward, rotation profile broadens.
- Possibilty of positional control of velocity shear layer via ICRF frequency
 - If shear layer width scales with ρ_{θ} , layer will affect microinstabilities

 - For C-Mod: $2.5 ext{ } 10^6 ext{ rad/s} ext{ } \left(2 ext{T/M}\right)^{1/2} ext{a}^{-1}$

ICRF RESONANT LAYER SCAN FOR C-MOD

• Use ICRF Model 2; calculate nondimensional rotation profile I*

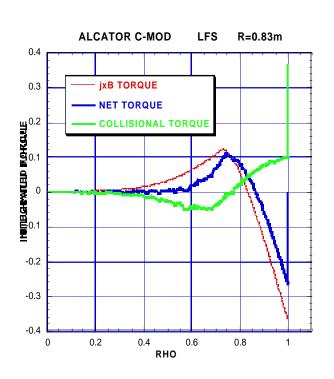


• When the resonant surface is on the high-field side, Counter-rotation is predicted

ORBIT LOSS TORQUE

When cyclotron resonance layer is close to the surface, direct orbit loss gives counter rotation

Example: Alcator C-Mod with resonance at 0.83 m and 80 percent loss





SPATIALLY DEPENDENT DIFFUSIVITIES

- 1. Assume diffusivity scales with q: $= {}_{o}q^{n}$
- 2. Change relationship between a, χ_0 , and τ_E
 - For uniform diffusivity $_{0} = a^{2} / 6_{E}$ (Taken from J₀ Bessel Function)
 - For diffusivity profile $_{o} = a^{2} / C_{n}(q)_{E}$
 - For n=2,

$$C_n(q) = q^2 + 2q + 3$$

$$v_{tor}(0) = \left\{ \frac{\left(q^2 + 2q + 3\right)W}{e B_a R_a^2 a^2 n (2)^2} \left(\frac{M}{E}\right) \right\} I^*$$

- Provides for increase of rotational velocity with decreasing current.
- For resonance close to axis, I* depends only weakly on q.

SUMMARY - 1

- 1. Separated regions of positive and negative torque density can generate central rotation
 - General property of a diffusion equation
- 2. ICRF generates two types of torque density on bulk plasma which are comparable in magnitude and integrate to zero net torque
 - $j_r \times B$ and mechanical angular momentum transfer by collisions
- 3. ORBIT code follows individual particles and computes the torque densities
 - ICRF model (initial condition for ORBIT) replaces a cold particle by an energetic particle.
 - Equal numbers of co- and counter energetic particles assure not net momentum injection. Angular momentum check to 2·10-4 level.

SUMMARY - 2

4. Central rotation arises

• Co-current sense, magnitude, and scaling in accord with Alcator C-Mod

$$- v_{exp}(0) = 10.0 \cdot 104 \text{ m/s}$$
 $v_{model}(0) = 7 \cdot 104 \text{ m/s}$

- Insensitve to particle energy, pitch, q_{max} , N, and initial ρ .
- High-field-side initial ρ gives counter-current rotation.

5. Summary formula

$$v_{tor}(0) = \left\{ \frac{6 \text{ W}}{e B_a R_a^2 a^2 n (2)^2} \left(\frac{M}{E} \right) \right\} I^*$$

$$I^* = 10-20$$

CONCLUSIONS

- A mechanism to create central rotation in tokamaks with ICRF heating has been indentified.
- Toroidal velocity scales diamagnetically
 - Magnitude and sense in accord with C-Mod data.
- Precise treatment of angular momentum needed and provided by ORBIT code





CONCLUSIONS

- A mechanism to create central rotation in tokamaks with ICRF heating has been identified.
- Toroidal velocity scales diamagnetically
 - Magnitude and sense in accord with C-Mod data.
- Precise treatment of angular momentum needed and provided by ORBIT code
- Provides means to control rotational profile.



