
Poloidal Field Design and Plasma Scenarios for the Fusion Ignition Research Experiment (FIRE)

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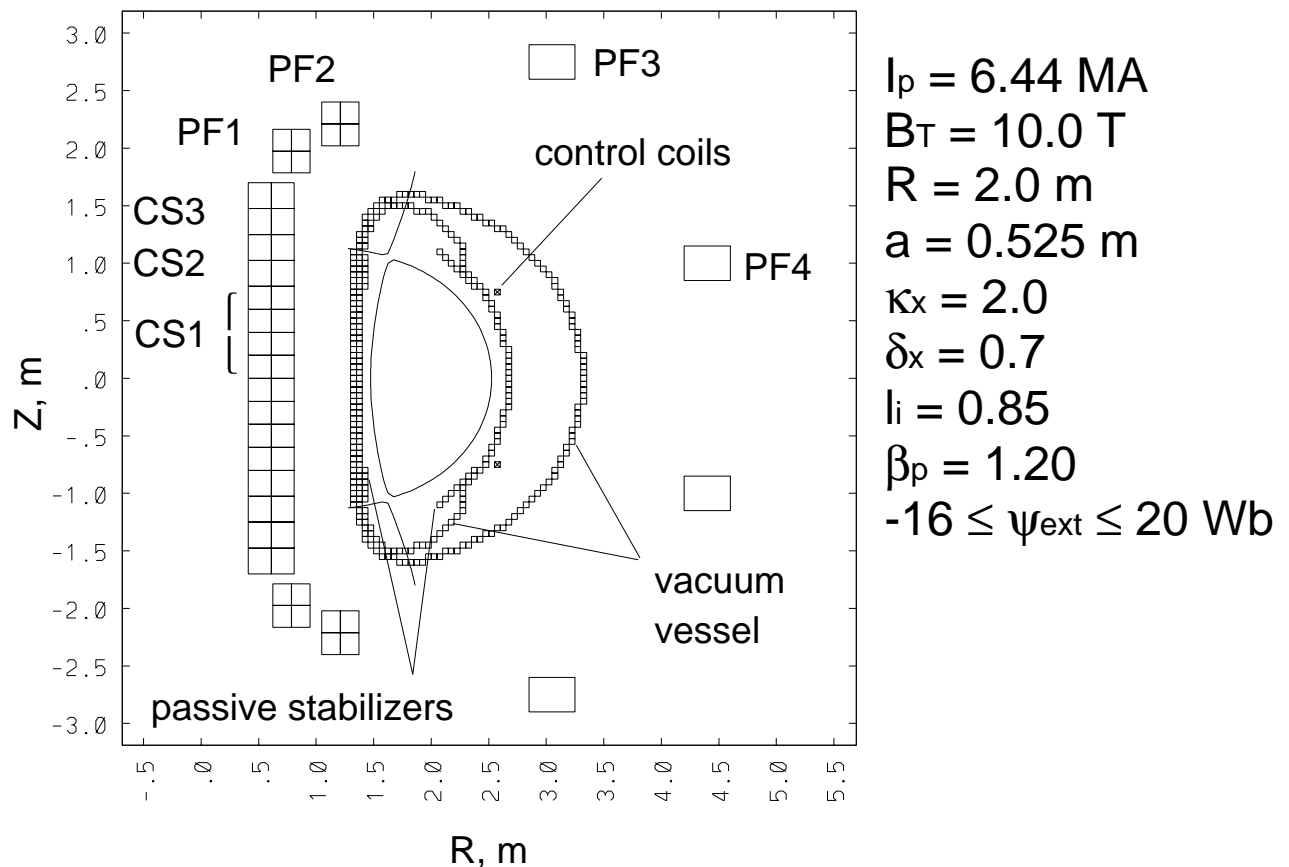
October 27, 1999

<http://fire.pppl.gov>



FIRE ***Fusion Ignition Research Experiment***

Plasma Equilibrium Analysis



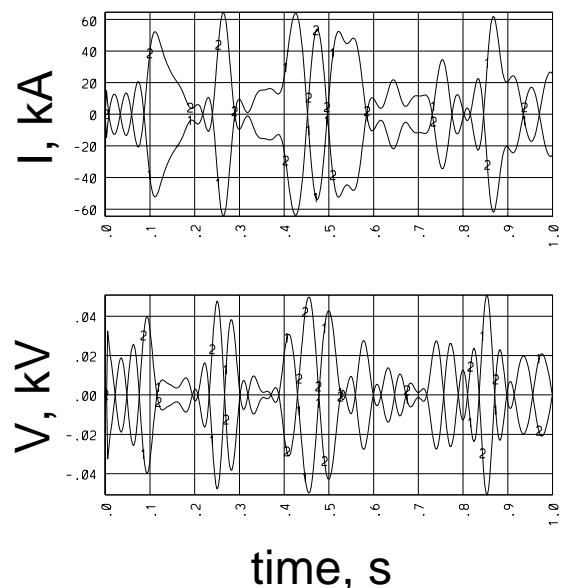
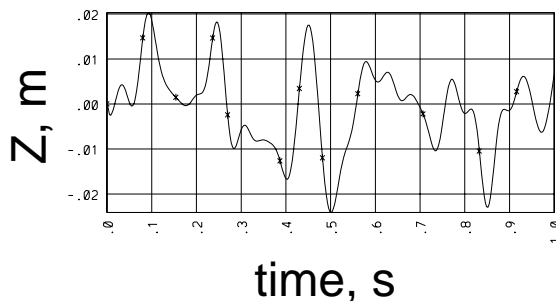
- PF coil locations determined by functionality, interferences, and proximity to plasma
- PF coil currents are determined to provide $\kappa_x = 2.0$, $\delta_x = 0.7$, and $q_{95} \geq 3.0$, subject to uncertainties in l_i , β_p , and ψ_{ext}
- generate equilibria at fiducial states; SOD, SOF, SOB, EOB, EOC, and EOD, with flux consumption between states determined by TSC
- heating and stresses in the PF coils provide the primary limits on coil currents, and these were combined with power supply analysis and TSC to optimize a scenario

Vertical Stability and Control

- design passive structures to slow vertical instability and provide a stability factor $f_s = 1 + \tau_g / \tau_{L/R} \geq 1.2$, and a growth time sufficiently long for feedback control
- passive stabilizers are made of 1.5 cm thick Cu, toroidally continuous on the inboard, and in saddle configuration on the outboard
- for low pressure plasmas ($\beta_p = 0.1$), over the range $0.7 \leq l_i \leq 1.1$, the stability factor and growth time are $1.3 \leq f_s \leq 1.13$ and $43 \leq \tau_g(\text{ms}) \leq 19$
- utilize internal control coils for feedback on the plasma vertical position, located just outside the inner VV
- control simulations indicate that for random disturbances with $\Delta Z_{\text{RMS}} = 1$ cm and step disturbances with $\Delta Z = 2$ cm, the peak power requirement is 5-10 MVA

$$I_{\text{peak}} = 55\text{-}75 \text{ kA-turns}$$

$$V_{\text{peak}} = 50\text{-}75 \text{ V/turn}$$



FIRE Reference Discharge Scenario

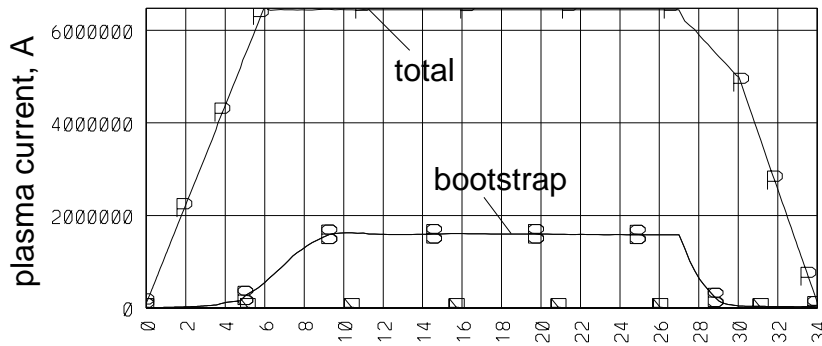
assumptions/inputs

- $n(\psi, t) = n_o(t) [1 - \psi^{2.0}]^{0.5} + n_b$
- $n_b = 0.3n_o$
- 3% Be impurity
- $\tau_p^* / \tau_E = 5$
- $\tau_E \approx 0.5 \text{ s}$
- $T_{\text{edge}} = 500 \text{ eV}$
- time averaged sawtooth
- Harris collisional bootstrap model

main plasma parameters

- $I_p = 6.44 \text{ MA}$, $B_T = 10 \text{ T}$
- $I_i = 0.85$, $q_{95} = 3.2$
- $\beta_p = 1.2$, $\beta = 3\%$, $\beta_N = 2.42$
- $W_{\text{th}} = 34.5 \text{ MJ}$, $P_\alpha = 50 \text{ MW}$
- $n_e / n_{Gr} = 0.6$
- $T_e(0)$, $T_i(0) \approx 18\text{-}19 \text{ keV}$
- $f_{bs} = 25\%$
- $V_{\text{loop}} = 0.1 \text{ V}$
- $Q = P_{\text{fus}}/P_{\text{aux}} = 11.4$
- $\Delta\psi(\text{rampup}) = 31.3 \text{ V-s}$
 $\Delta\psi(\text{SOF} \rightarrow \text{EOB}) = 2.5 \text{ V-s}$
- $n_e(0) = 5.0 \times 10^{20} \text{ /m}^3$
 $n_e(\text{line}) = 4.55$
 $\langle n_e \rangle_v = 3.85$
- $\langle n_{\text{He}} \rangle = 0.04 \langle n_e \rangle$

FIRE Reference Discharge Scenario



Current Rampup, $t=0-6$ s

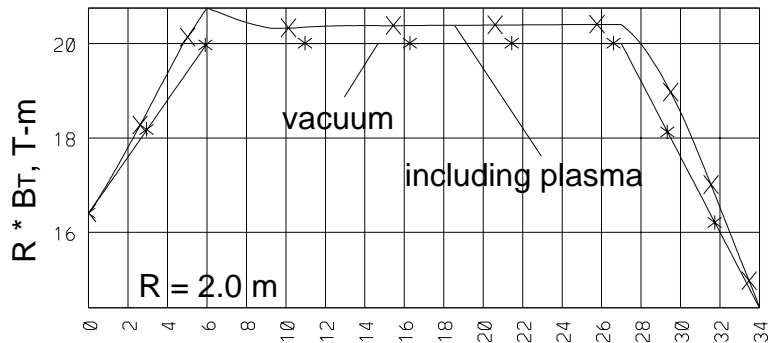
$I_p = 0.1 \rightarrow 6.44$ MA

$B_T = 8.2 \rightarrow 10.0$ T

$n_e = .05 \rightarrow 1.8 \times 10^{20}$

plasma diverts at 3.2 s

30 MW heating at 4.8 s



Heating to Burn and Flattop, $t=6-27$ s

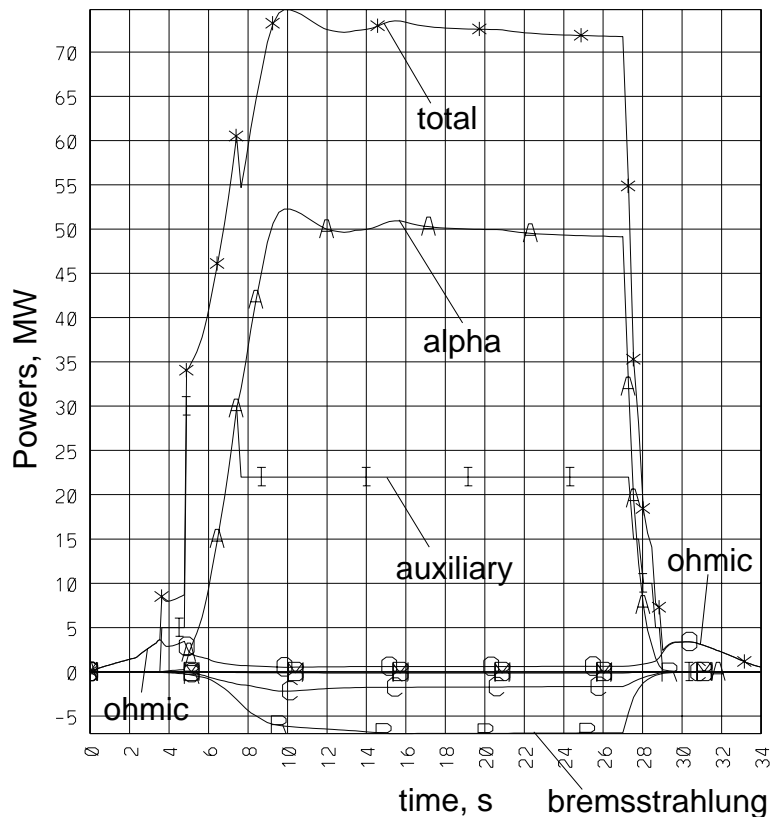
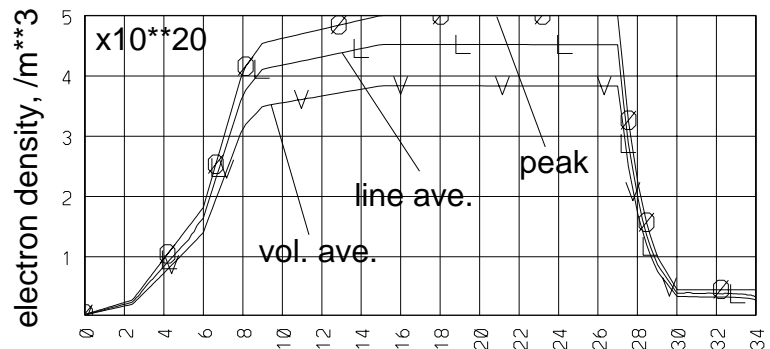
I_p and B_T fixed

$n_e = 1.8 \rightarrow 5.0 \times 10^{20}$

heating dropped $30 \rightarrow 22$ MW

$P_\alpha \rightarrow 50$ MW, $Q \geq 10$

$\langle n_{He} \rangle \rightarrow 4\% \langle n_e \rangle$, $Z_{eff} \rightarrow 1.4$



Burn Termination and Rampdown,
 $t=27-34$ s

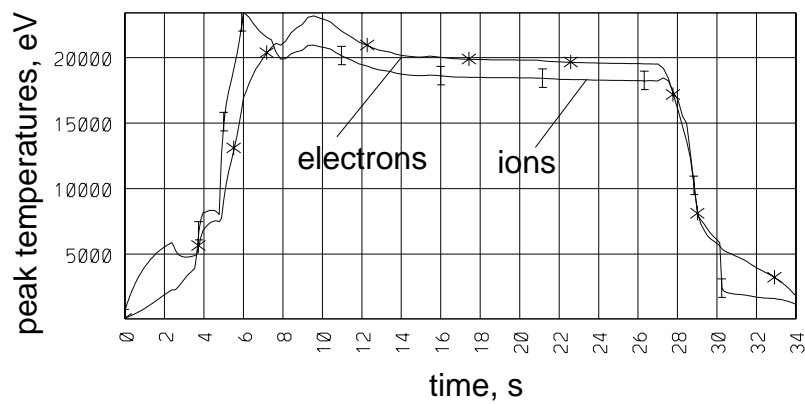
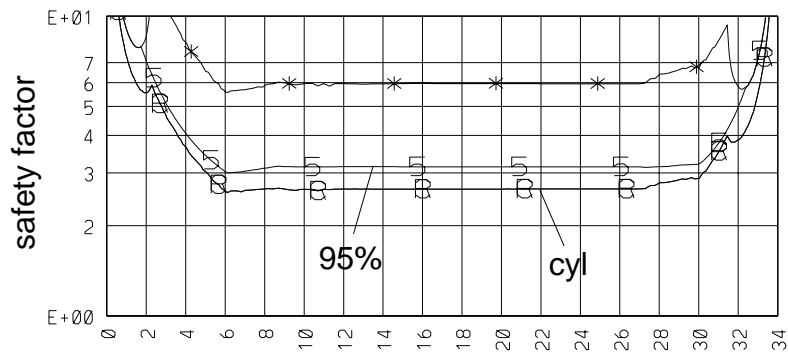
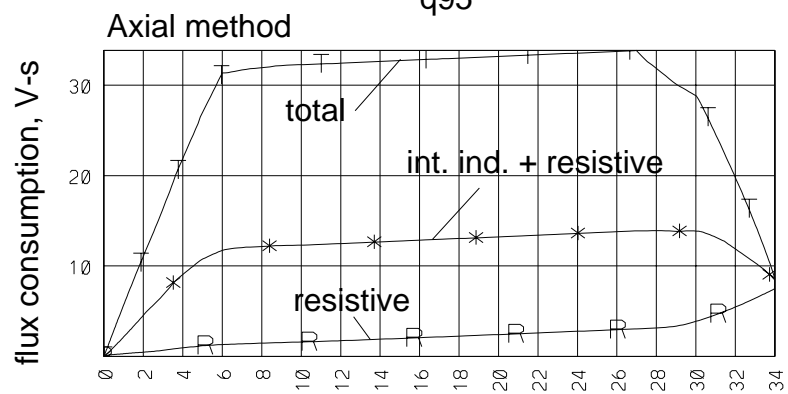
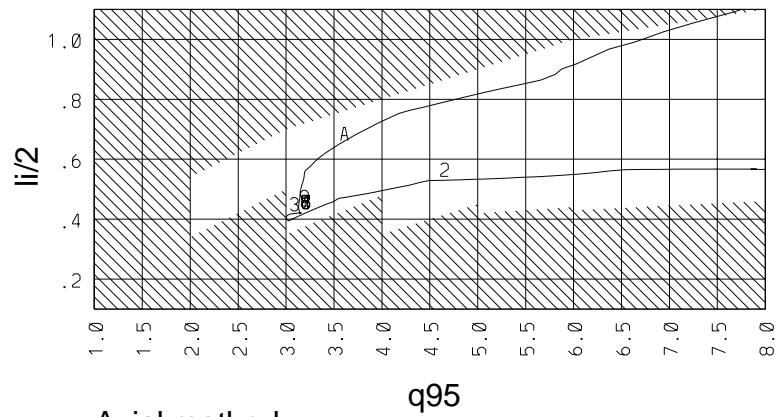
stop plasma fueling

P_α drops and $H \rightarrow L$ mode

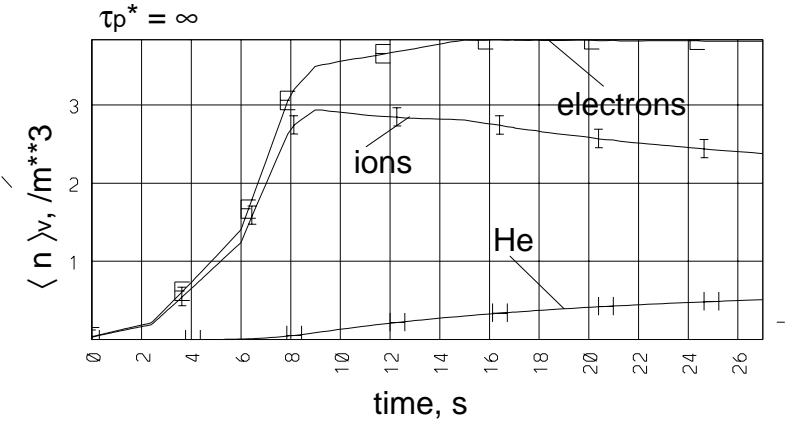
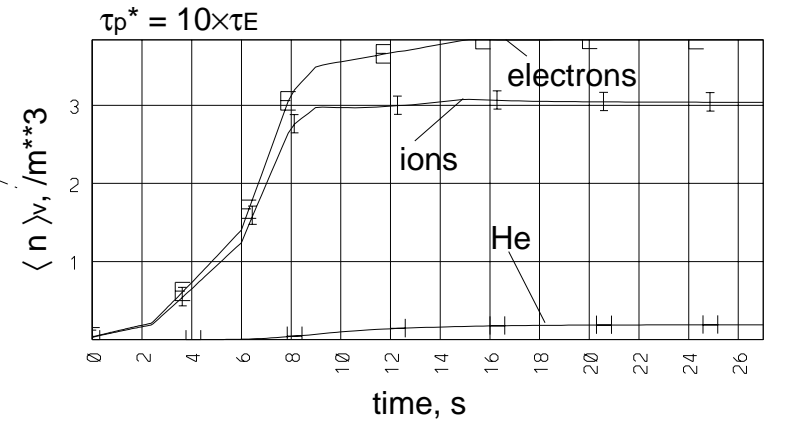
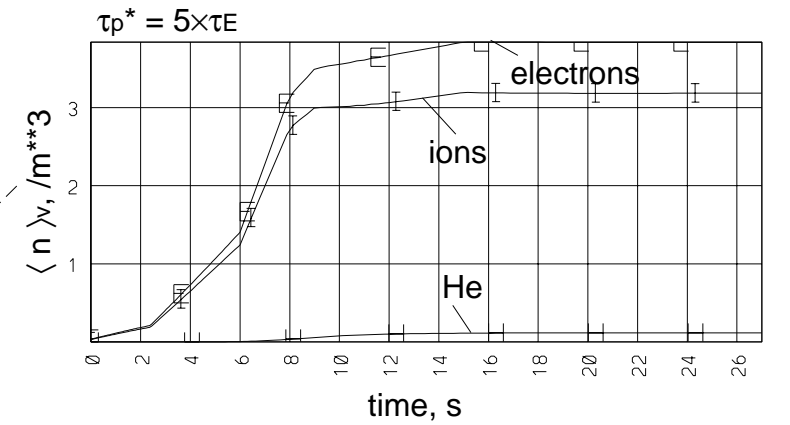
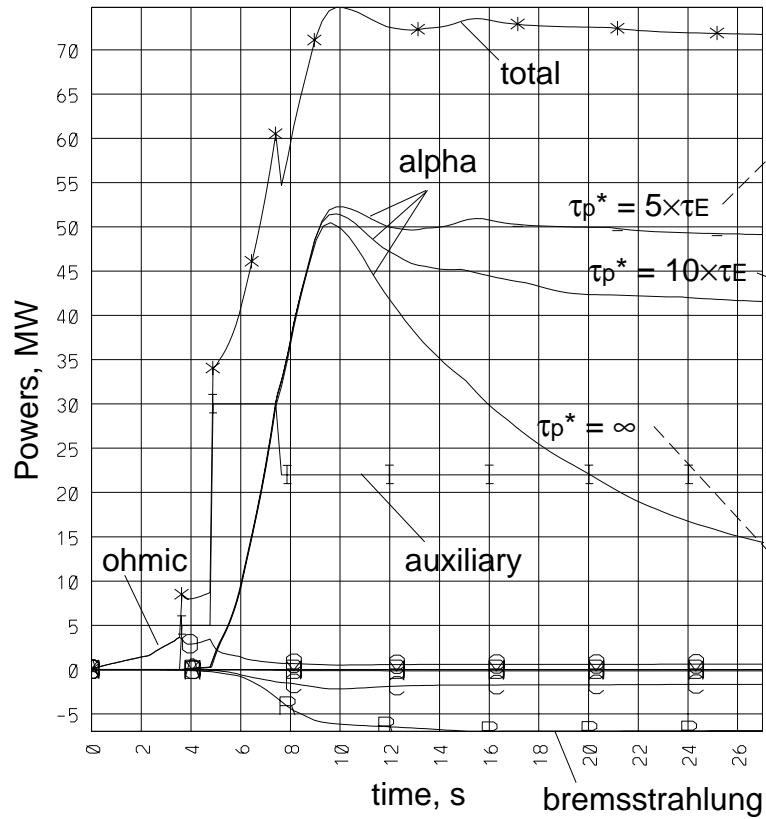
P_{aux} is dropped $15 \rightarrow 10 \rightarrow 5$ MW

I_p reduced to 5.0, and then 0.1 MA

FIRE Reference Discharge Scenario



τ_p^* / τ_E Variation in FIRE

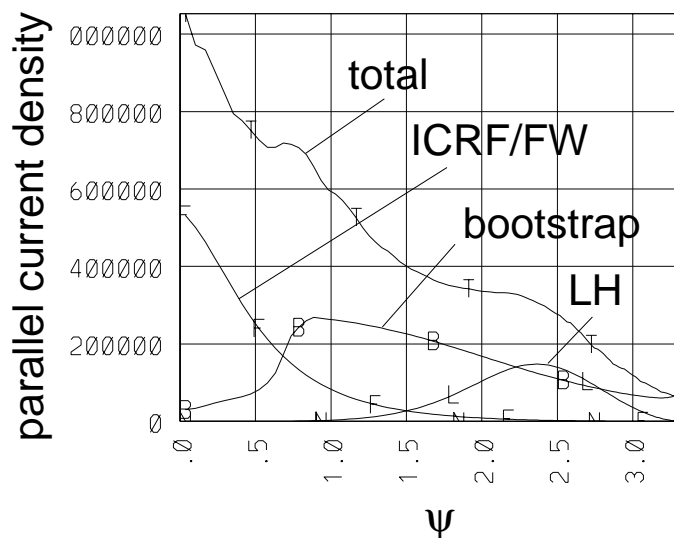


FIRE Long Pulse DD Capability

- if B_T is lowered to 4.0 T, and I_p is lowered to 2.0 MA, the pulse length reaches 250 s
- the TPX physics objectives can be achieved
- taking
 - 14 MW of ICRF/FW
 - 6MW of LHCD
 - $2 \times$ L-mode confinement
 - $n_e(0) = 1.35 \times 10^{20} \text{ /m}^3$
 - $T_e(0) = 15 \text{ keV}$

we get

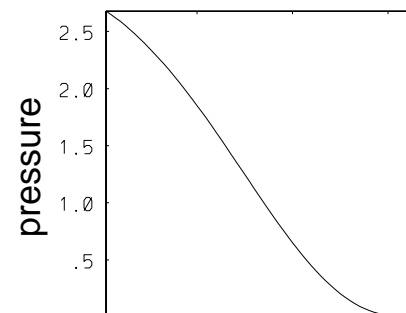
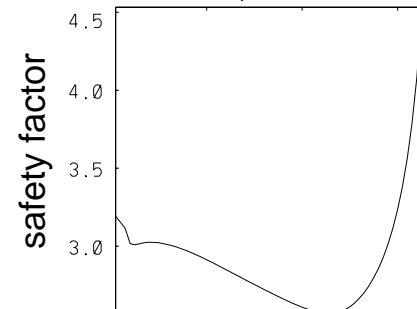
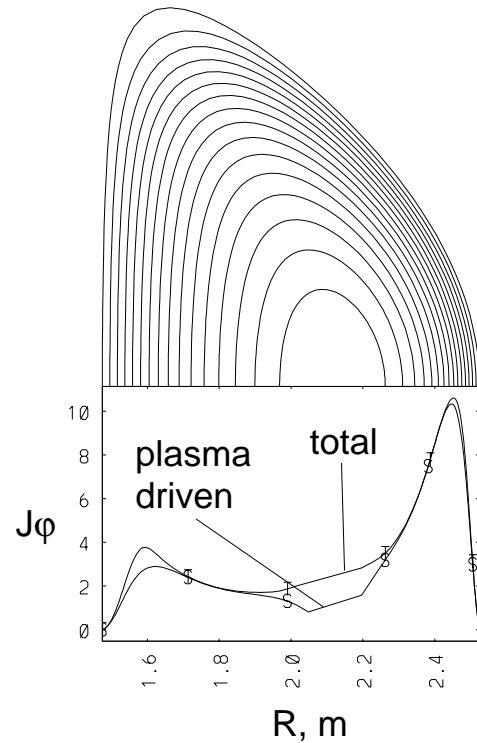
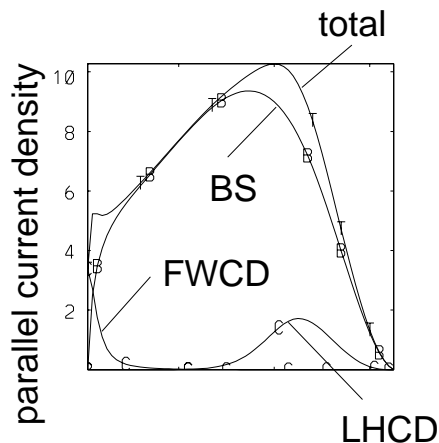
- $I(\text{FW}) = 300 \text{ kA}$ (phased antenna)
- $I(\text{LH}) = 300 \text{ kA}$
- $I(\text{BS}) = 775 \text{ kA}$
- $I(\text{OH}) = 625 \text{ kA}$
- $V_{\text{loop}} = 0.02 \text{ V}$
- $\beta_N = 2.5$
- $\Delta\psi(\text{total}) = 14.6 \text{ V-s}$



FIRE Burning AT Modes

- reducing B_T to 6.75 T and I_p to 4.50 MA, a burning advanced tokamak mode with $P_{fus} = 160$ MW can be found

$f_{bs} = 91\%$
 $I(LH) = 275$ kA
 $I(FW) = 115$ kA
 $q_{axis} \approx 3.0$
 $q_{min} = 2.6$
 $\beta_N = 4.5$
 $n_e/n_{Gr} = 0.78$
 $\alpha\text{-loss} = 9.5\%$



- critical issues:
 - ideal MHD, kink mode
 - neoclassical tearing modes
 - alpha particle losses
 - heating/CD power
 - plasma edge compatibility
 - bootstrap current
 - achievable Q

Summary

- PF coils designed for FIRE provide the reference scenario with sufficient margin to all coil allowables to compensate plasma uncertainties
- In addition, the PF coils can provide
 - a 12 T and 7.7 MA discharge for 11 s
 - a 4 T and 2.0 MA discharge for 250 s
 - burning AT modes at reduced I_p and B_T
- the passive stabilizer design in combination with internal feedback coils provides sufficient vertical position control with reasonable power
- full discharge scenarios for FIRE
 - demonstrate $Q=10$ operation
 - sensitivity to plasma parameter assumptions
 - burn response/control
 - plasma current and boundary evolution, flux consumption, and feedback control
 - used in conjunction with coil heating, stress, and power supply analysis to optimize scenarios