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**Poloidal Field Design and Plasma Scenarios  
for the  
Fusion Ignition Research Experiment (FIRE)**

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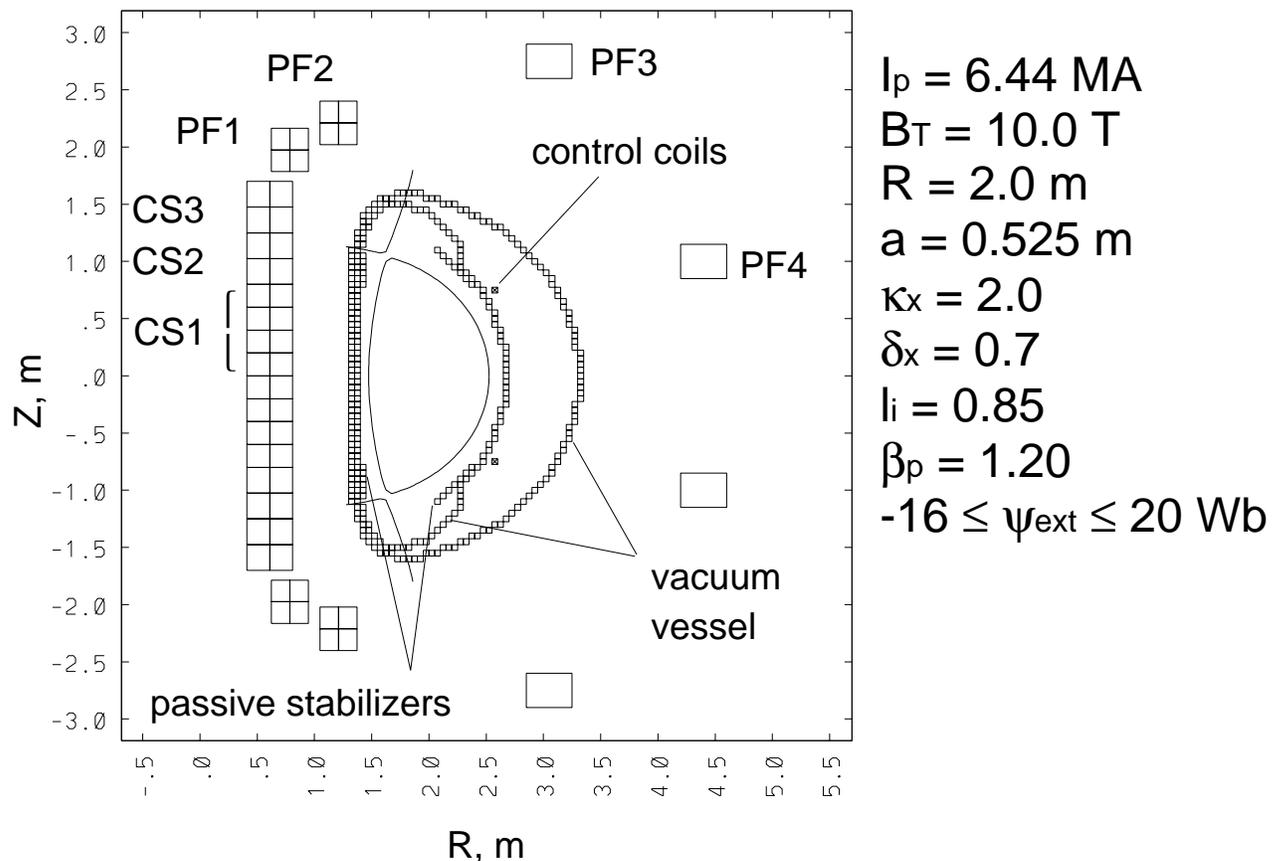
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**October 27, 1999**

<http://fire.pppl.gov>

***FIRE***   
***Fusion Ignition Research Experiment***

# Plasma Equilibrium Analysis



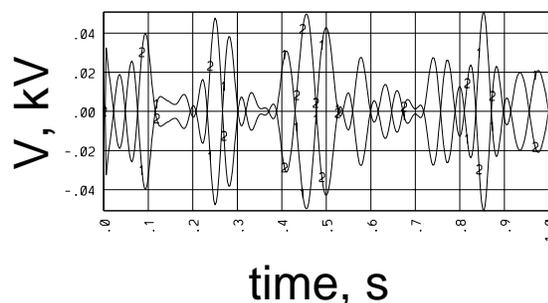
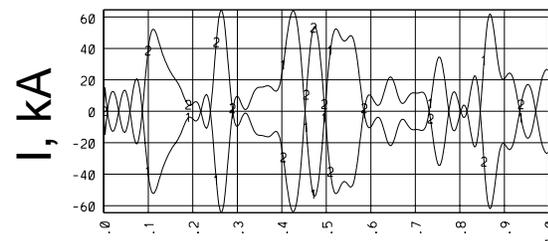
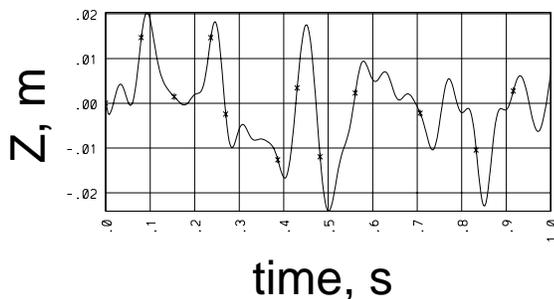
- PF coil locations determined by functionality, interferences, and proximity to plasma
- PF coil currents are determined to provide  $\kappa_x = 2.0$ ,  $\delta_x = 0.7$ , and  $q_{95} \geq 3.0$ , subject to uncertainties in  $l_i$ ,  $\beta_p$ , and  $\psi_{\text{ext}}$
- generate equilibria at fiducial states; SOD, SOF, SOB, EOB, EOC, and EOD, with flux consumption between states determined by TSC
- heating and stresses in the PF coils provide the primary limits on coil currents, and these were combined with power supply analysis and TSC to optimize a scenario

# Vertical Stability and Control

- design passive structures to slow vertical instability and provide a stability factor  $f_s = 1 + \tau_g / \tau_{L/R} \geq 1.2$ , and a growth time sufficiently long for feedback control
- passive stabilizers are made of 1.5 cm thick Cu, toroidally continuous on the inboard, and in saddle configuration on the outboard
- for low pressure plasmas ( $\beta_p = 0.1$ ), over the range  $0.7 \leq l_i \leq 1.1$ , the stability factor and growth time are  $1.3 \leq f_s \leq 1.13$  and  $43 \leq \tau_g(\text{ms}) \leq 19$
- utilize internal control coils for feedback on the plasma vertical position, located just outside the inner VV
- control simulations indicate that for random disturbances with  $\Delta Z_{\text{RMS}} = 1$  cm and step disturbances with  $\Delta Z = 2$  cm, the peak power requirement is 5-10 MVA

$$I_{\text{peak}} = 55\text{-}75 \text{ kA-turns}$$

$$V_{\text{peak}} = 50\text{-}75 \text{ V/turn}$$



# FIRE Reference Discharge Scenario

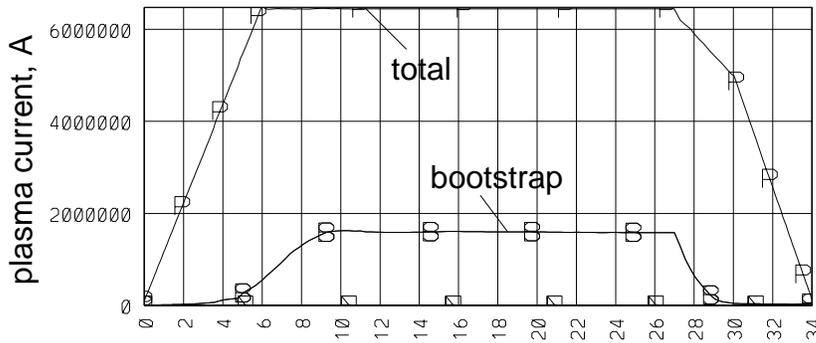
## assumptions/inputs

- $n(\psi,t) = n_o(t)[1 - \psi^{2.0}]^{0.5} + n_b$
- $n_b = 0.3n_o$
- 3% Be impurity
- $\tau_p^* / \tau_E = 5$
- $\tau_E \approx 0.5 \text{ s}$
- $T_{\text{edge}} = 500 \text{ eV}$
- time averaged sawtooth
- Harris collisional bootstrap model

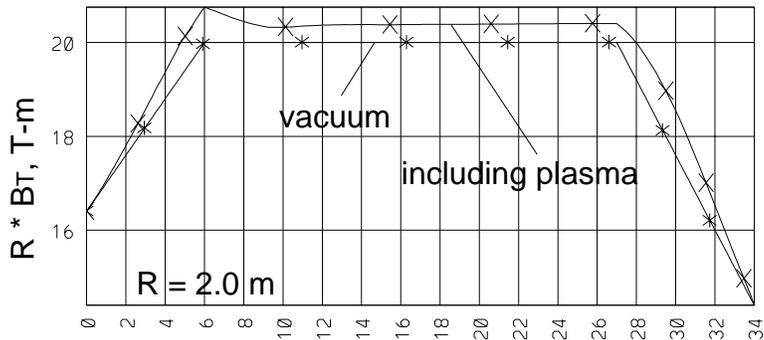
## main plasma parameters

- $I_p = 6.44 \text{ MA}$ ,  $B_T = 10 \text{ T}$
- $I_i = 0.85$ ,  $q_{95} = 3.2$
- $\beta_p = 1.2$ ,  $\beta = 3\%$ ,  $\beta_N = 2.42$
- $W_{\text{th}} = 34.5 \text{ MJ}$ ,  $P_\alpha = 50 \text{ MW}$
- $n_e / n_{Gr} = 0.6$
- $T_e(0)$ ,  $T_i(0) \approx 18\text{-}19 \text{ keV}$
- $f_{bs} = 25\%$
- $V_{\text{loop}} = 0.1 \text{ V}$
- $Q = P_{\text{fus}}/P_{\text{aux}} = 11.4$
- $\Delta\psi(\text{rampup}) = 31.3 \text{ V-s}$   
 $\Delta\psi(\text{SOF} \rightarrow \text{EOB}) = 2.5 \text{ V-s}$
- $n_e(0) = 5.0 \times 10^{20} \text{ /m}^3$   
 $n_e(\text{line}) = 4.55$   
 $\langle n_e \rangle_v = 3.85$
- $\langle n_{\text{He}} \rangle = 0.04 \langle n_e \rangle$

# FIRE Reference Discharge Scenario

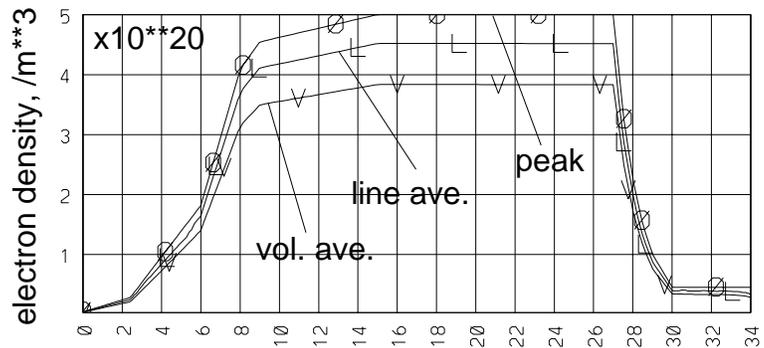


Current Rampup,  $t=0-6$  s  
 $I_p = 0.1 \rightarrow 6.44$  MA  
 $B_T = 8.2 \rightarrow 10.0$  T  
 $n_e = .05 \rightarrow 1.8 \times 10^{20}$   
 plasma diverts at 3.2 s  
 30 MW heating at 4.8 s



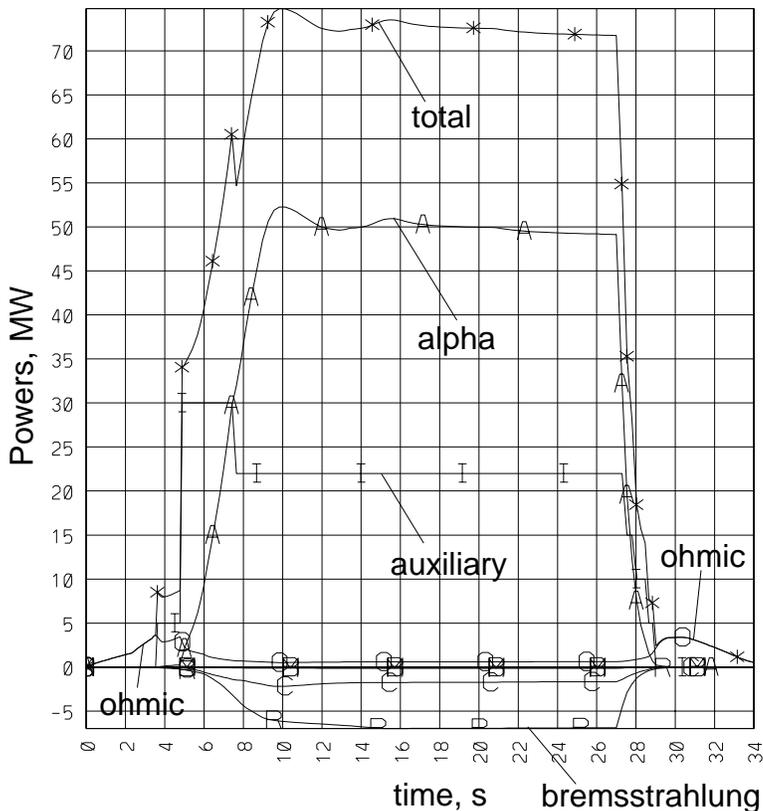
Heating to Burn and Flattop,  $t=6-27$ s

$I_p$  and  $B_T$  fixed  
 $n_e = 1.8 \rightarrow 5.0 \times 10^{20}$   
 heating dropped 30  $\rightarrow$  22 MW  
 $P_\alpha \rightarrow 50$  MW,  $Q \geq 10$   
 $\langle n_{He} \rangle \rightarrow 4\% \langle n_e \rangle$ ,  $Z_{eff} \rightarrow 1.4$

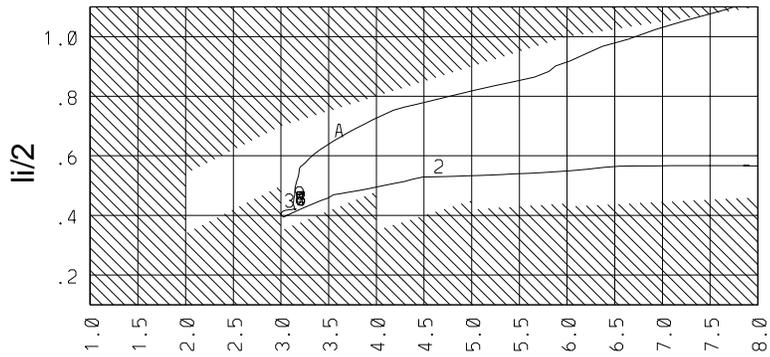


Burn Termination and Rampdown,  
 $t=27-34$ s

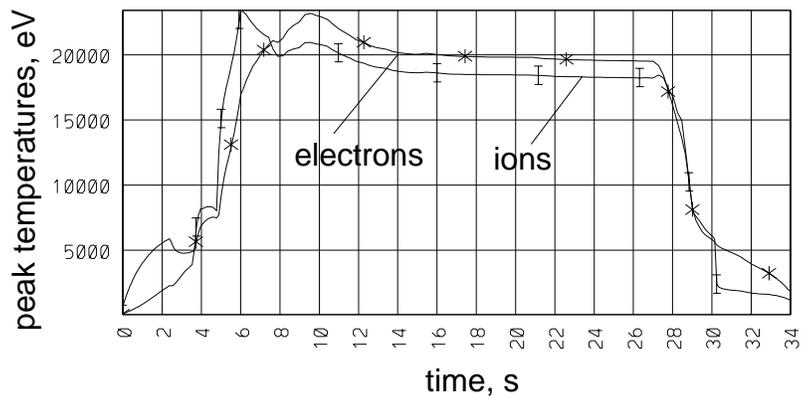
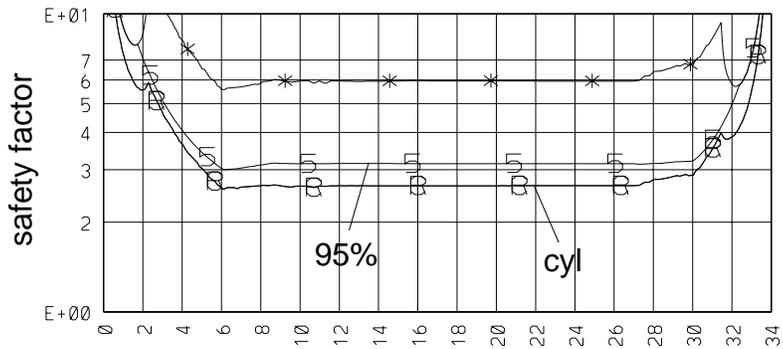
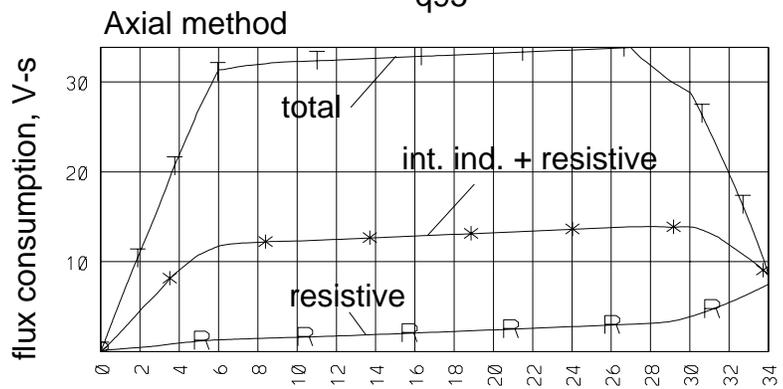
stop plasma fueling  
 $P_\alpha$  drops and H  $\rightarrow$  L mode  
 $P_{aux}$  is dropped 15  $\rightarrow$  10  $\rightarrow$  5 MW  
 $I_p$  reduced to 5.0, and then 0.1 MA



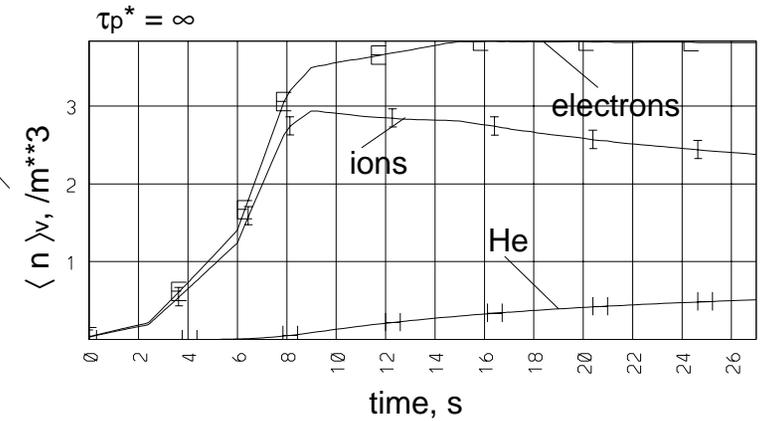
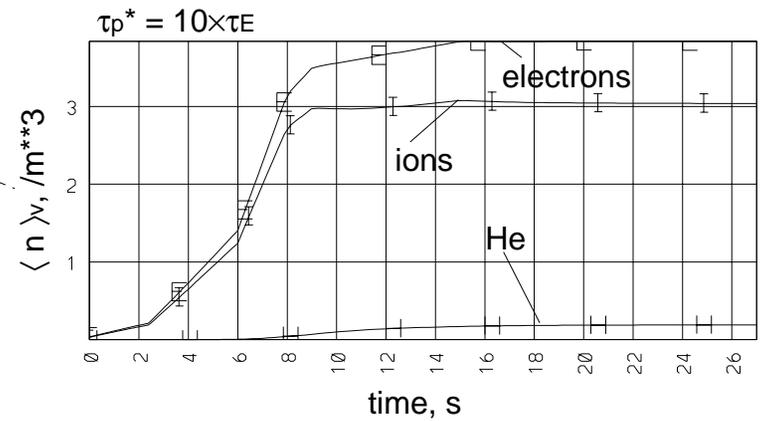
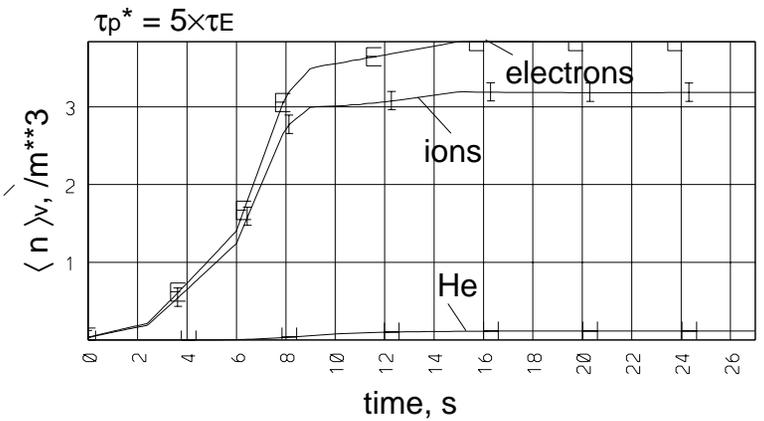
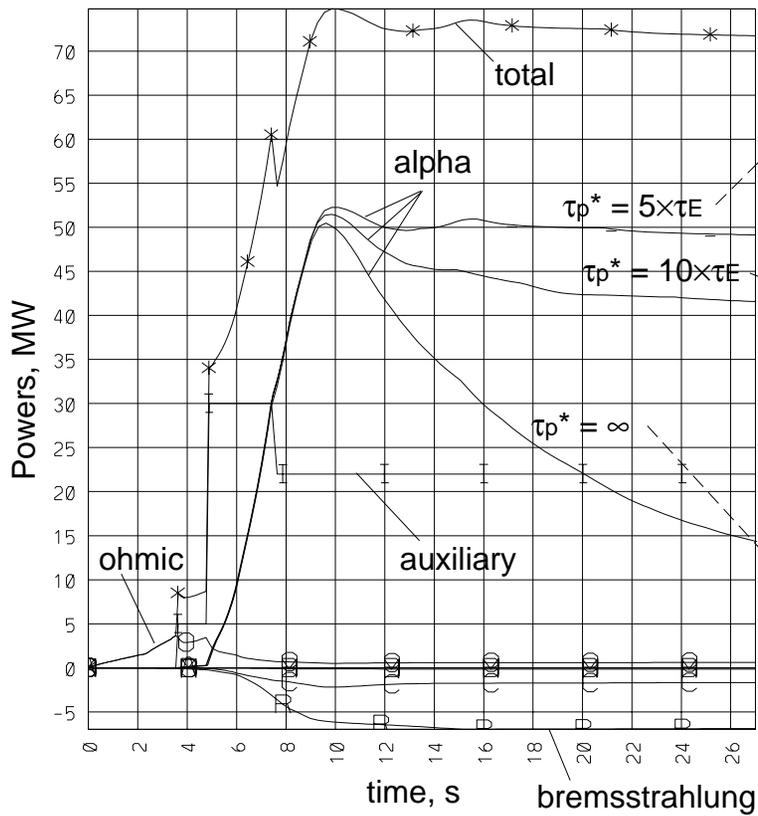
# FIRE Reference Discharge Scenario



q95



# $\tau_p^* / \tau_E$ Variation in FIRE

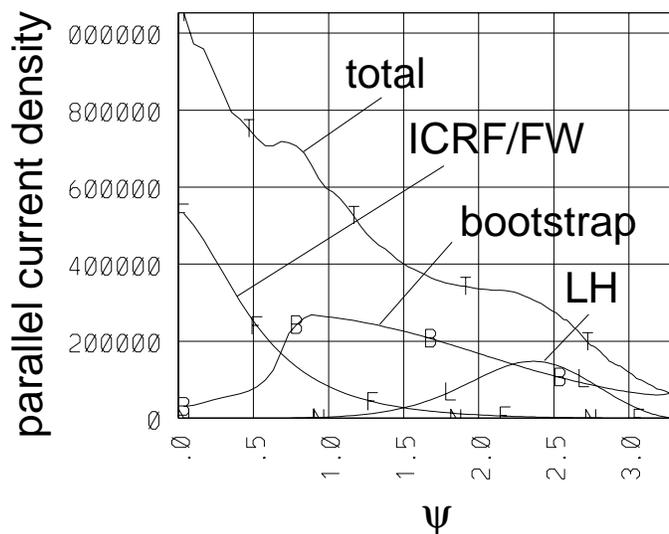


# FIRE Long Pulse DD Capability

- if  $B_T$  is lowered to 4.0 T, and  $I_p$  is lowered to 2.0 MA, the pulse length reaches 250 s
- the TPX physics objectives can be achieved
- taking
  - 14 MW of ICRF/FW
  - 6MW of LHCD
  - $2 \times$  L-mode confinement
  - $n_e(0) = 1.35 \times 10^{20} \text{ /m}^3$
  - $T_e(0) = 15 \text{ keV}$

we get

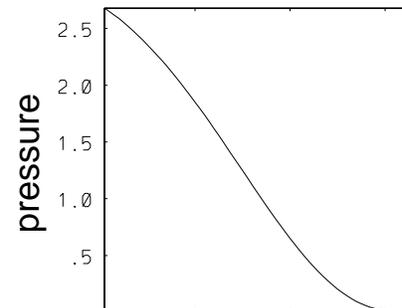
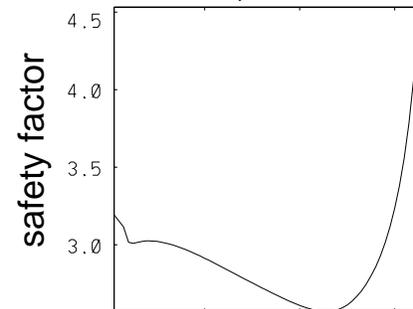
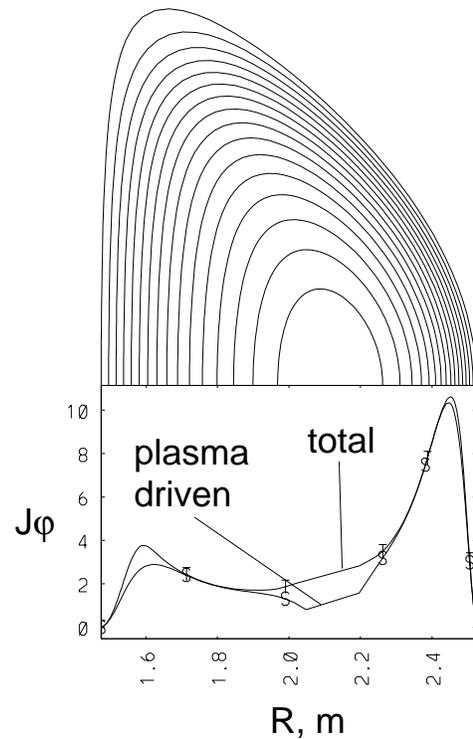
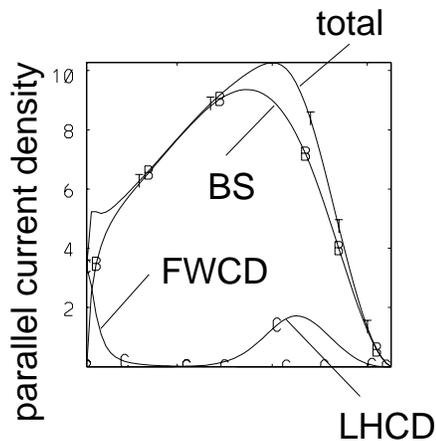
- $I(\text{FW}) = 300 \text{ kA}$  (phased antenna)
- $I(\text{LH}) = 300 \text{ kA}$
- $I(\text{BS}) = 775 \text{ kA}$
- $I(\text{OH}) = 625 \text{ kA}$
- $V_{\text{loop}} = 0.02 \text{ V}$
- $\beta_N = 2.5$
- $\Delta\psi(\text{total}) = 14.6 \text{ V-s}$



# FIRE Burning AT Modes

- reducing  $B_T$  to 6.75 T and  $I_p$  to 4.50 MA, a burning advanced tokamak mode with  $P_{fus} = 160$  MW can be found

$f_{bs} = 91\%$   
 $I(LH) = 275$  kA  
 $I(FW) = 115$  kA  
 $q_{axis} \approx 3.0$   
 $q_{min} = 2.6$   
 $\beta_N = 4.5$   
 $n_e/n_{Gr} = 0.78$   
 $\alpha\text{-loss} = 9.5\%$



- critical issues:
  - ideal MHD, kink mode
  - neoclassical tearing modes
  - alpha particle losses
  - heating/CD power
  - plasma edge compatibility
  - bootstrap current
  - achievable Q

# Summary

- PF coils designed for FIRE provide the reference scenario with sufficient margin to all coil allowables to compensate plasma uncertainties
- In addition, the PF coils can provide
  - a 12 T and 7.7 MA discharge for 11 s
  - a 4 T and 2.0 MA discharge for 250 s
  - burning AT modes at reduced  $I_p$  and  $B_T$
- the passive stabilizer design in combination with internal feedback coils provides sufficient vertical position control with reasonable power
- full discharge scenarios for FIRE
  - demonstrate  $Q=10$  operation
  - sensitivity to plasma parameter assumptions
  - burn response/control
  - plasma current and boundary evolution, flux consumption, and feedback control
  - used in conjunction with coil heating, stress, and power supply analysis to optimize scenarios