

## **Control of Transport Barriers**

**Edge transport barriers (20 mins. + discussion)**

**Internal transport barriers (20 mins. + discussion)**

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**Acknowledgements to a large number of people !!!**

## Scope and outline

Need for control of edge and internal transport barriers comes from:

- I. requirements for the next step (e.g. ITER-FEAT).
- II. desire to obtain, optimise and sustain improved confinement.

**A:** Control of edge transport barriers in H-modes, predominantly (I).

**B:** Control of scenarios with internal transport barriers, predominantly (II).

- ⇒ Review and compare the techniques that are used.  
Highlighted by some (unique) examples.  
Show alternatives (e.g. Hybrid scenario).

**Review their relevance, for burning plasmas (R).**

**Indicate points for discussion (D).**

# A: Control of Edge Transport Barriers

### Posters with this Topic:

- D5: H. Meyer, Formation of transport barriers in the MAST spherical tokamak.
- D6: Y. Sakamoto, Impact of toroidal rotation on ELM behaviour in H-mode and ITB plasmas on JT-60U.
- D7: R. Maingi, Effect of Gas Fuelling Location on H-mode Access in NSTX.
- D8: H. Urano, Impact of H-mode pedestal on ELMs with and without pellet injection in ASDEX Upgrade.
- D9: K. Jain, Study on generation of radial electric field with various biased electrode ring configurations in a toroidal plasma.
- D10: M. Yoshinuma, Observations of Edge Radial Electric Field Transition in LHD Plasma.

**Poster presentations indicated during this talk : (P)**

## Driven by requirements for the next step:

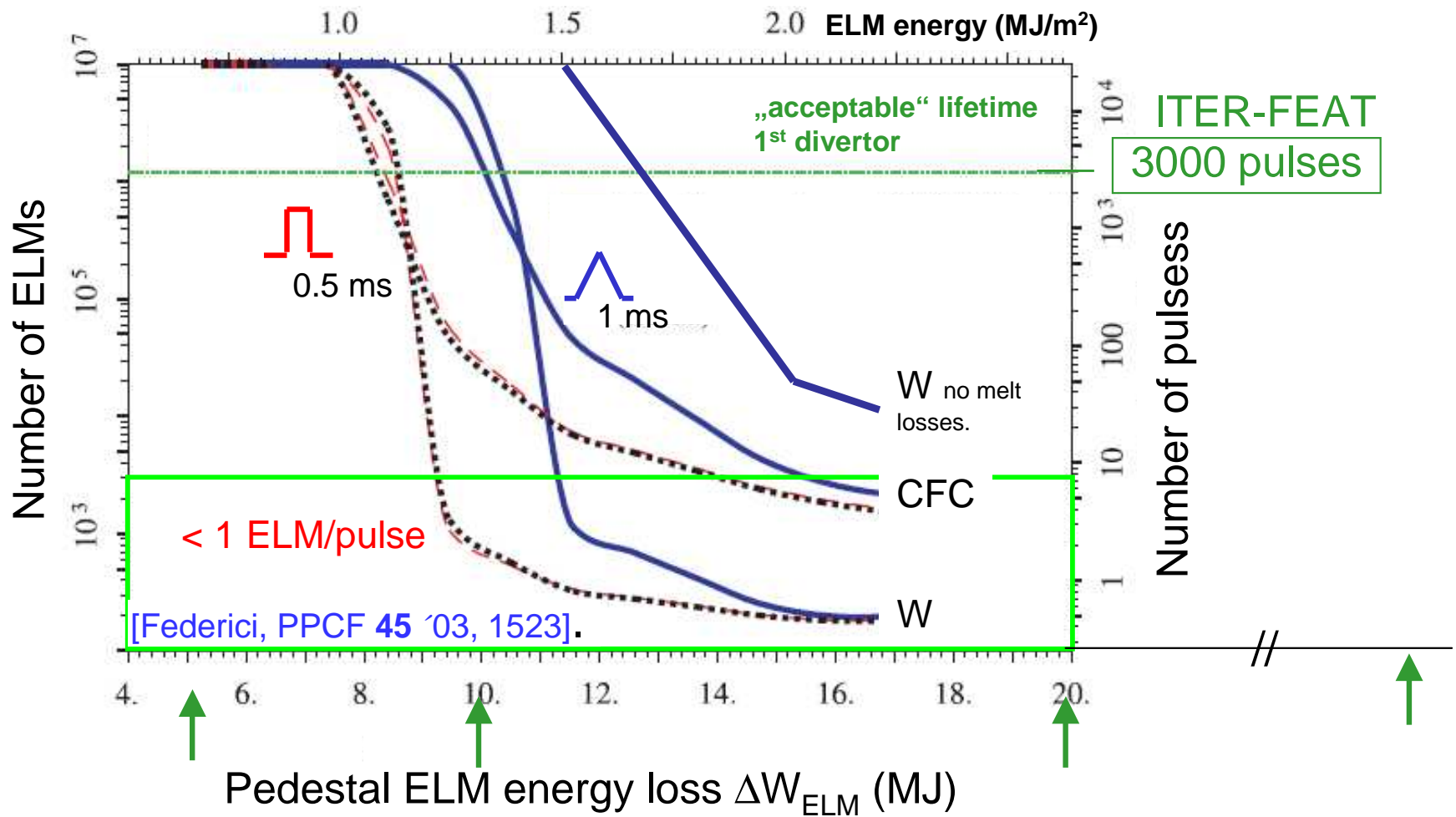
- To access H-mode (in Tokamaks), Power threshold for ITER-FEAT 37–68 MW,  $D_2$  at  $\langle n_e \rangle = 5.0 \times 10^{19} \text{ m}^{-3}$ . Installed power  $\sim 73$  MW.
- The energy losses during type I ELMs are a considerable concern when scaled to a reactor size device (divertor lifetime):

### Predictions for energy loss per ELM for ITER-FEAT (*D*):

- $\sim f_{\text{ELM}}^* \tau_E$  gives:  $\sim 60 \text{ MJ}$  [Herrmann, PPCF 44 '02, 883].
- $\sim \nu_{\text{ped}}^*$ , pedestal collisionality gives:  $\sim 20 \text{ MJ}$  [Loarte, PPCF 44 '02, 1815].
- $\sim \tau_{//}$ , ion transport transit time gives:  $\sim 10 \text{ MJ}$  [Loarte, PPCF 45 '03, 1549].
- $\sim n_e/n_{\text{GW}}$  scaling gives:  $\sim 5 \text{ MJ}$  [Leonard, PPCF 44 '02, 945].

(H. Urano, AUG (*P*)).

# Control of edge transport barriers: Requirements



Loss power due to ELMs:  $f_{ELM} \times \Delta W_{ELM}$ ,

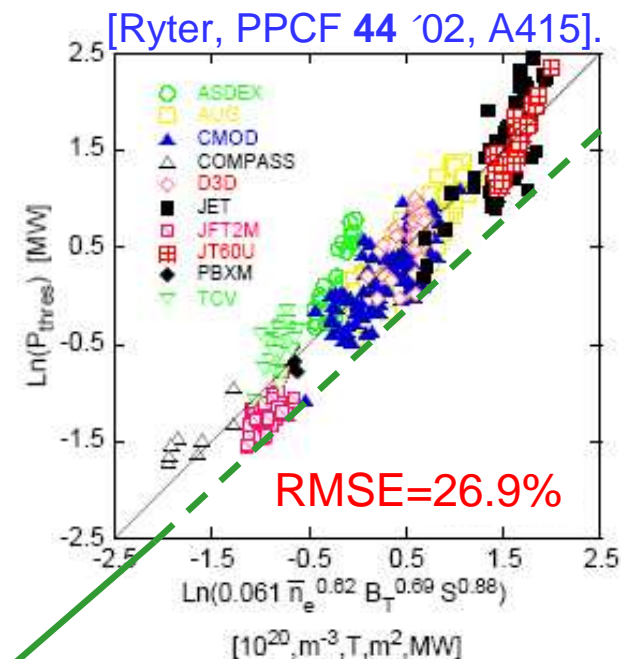
However erosion, strong dependence on  $\Delta W_{ELM}$  (control  $\Delta W_{ELM}$  !)

ELMs have non-uniform  $\Delta W_{ELM}$  distribution: So  $\Delta W_{ELM, average} \sim 3-4$  MJ

# Methods for control of H-mode access

$$P_{\text{thres}} \text{ (MW)} = 0.06 \overset{\text{control}}{\langle n_e \rangle^{0.62}} B_T^{0.69} S^{0.88} \text{ (} 10^{20} \text{m}^{-3}, \text{T, m}^{-2} \text{)}$$

- (i) more complicated dependencies of the variables used (density !).
- (ii) other “hidden” variables, related to Atomic processes, turbulence and MHD.
- (iii) To get Type I ELMs ( $H_{98} \sim 1$ ):  $P_{\text{in}} \sim 2 \times P_{\text{thres}}$ .



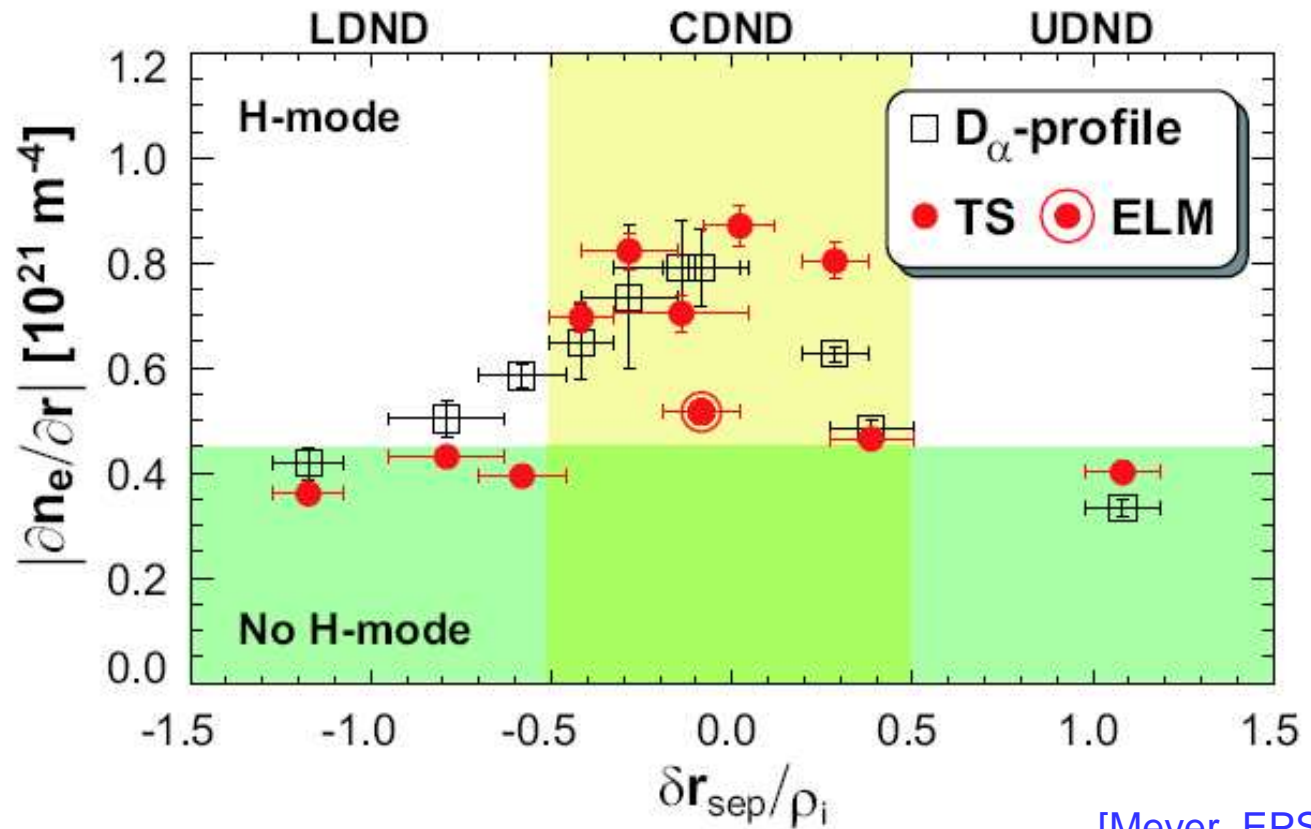
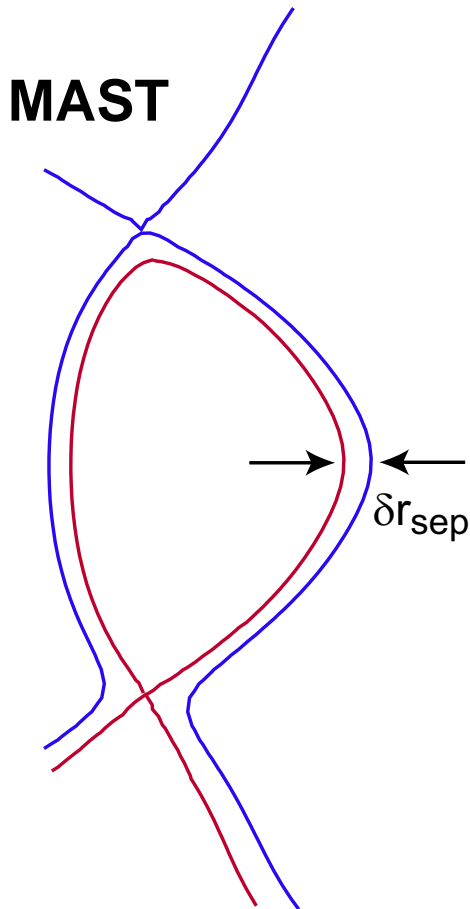
Lower  $P_{\text{thres}}$  using: ?

- (1) the effect of fuelling location (Maingi, NSTX ( $P$ )), pellet injection [Compass-D, Volvic, PPCF 44 '02, A175, DIII-D, Gohil, PPCF 45 '03, 601], (Meyer, MAST ( $P$ )).
- (2) the shape of the divertor or plasma shape [Many !]
- (3) the control of the electric field [T10, Kirnev, PPCF 45 '03, 337], (Jain ( $P$ ), Yoshinuma LHD ( $P$ ), Minami CHS ( $P$ )).

# Methods for control of H-mode access - Example

The shape of the plasma: Results from MAST (Meyer, (P))

Low threshold in double null configurations:



[Meyer, EPS'02]

Applicable to tokamak (reactor) ? (D)  
(DIII-D + recently AUG).



# Methods for control of Type I ELMs

## Impurity seeding:

Benefit in maintaining  $H_{98} \sim 1$  at reactor relevant  $n_e$  (JET, JT-60U).

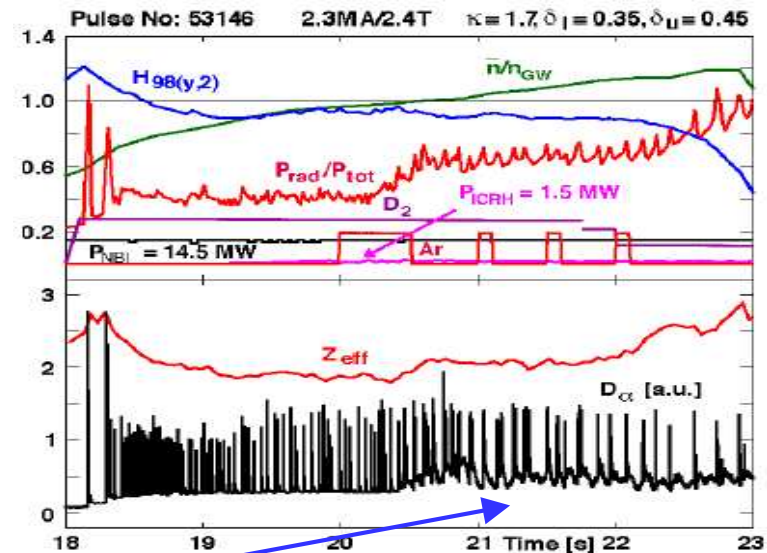
Critical to maintain low temperature in the divertor (reactor without CFC).

Reduction in  $f_{ELM}$ , but may not eliminate large energy fluxes.

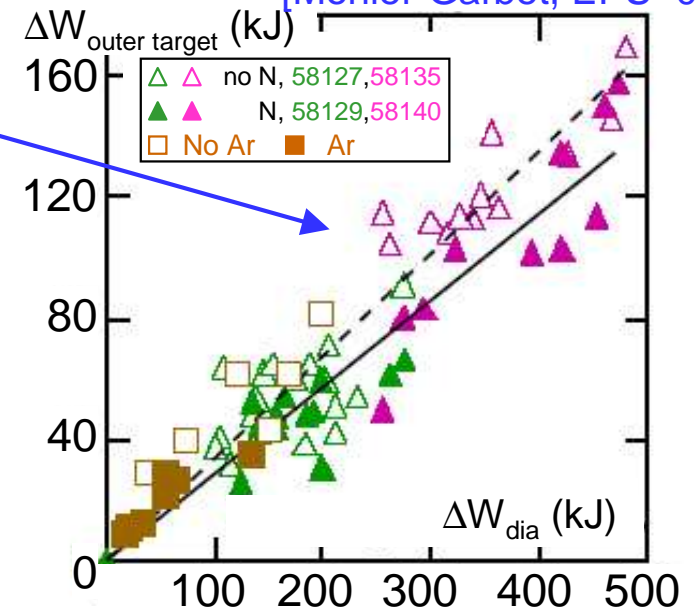
At high seeding levels, long ELM free phases, not stationary in confinement.

Likely to be used in conjunction with other mitigation schemes. **(R)**

[Ongena, IAEA '02]



[Monier-Garbet, EPS '03]

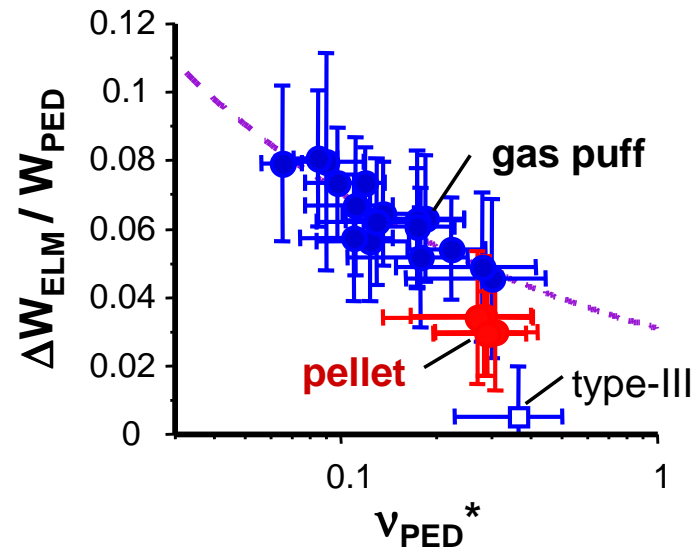
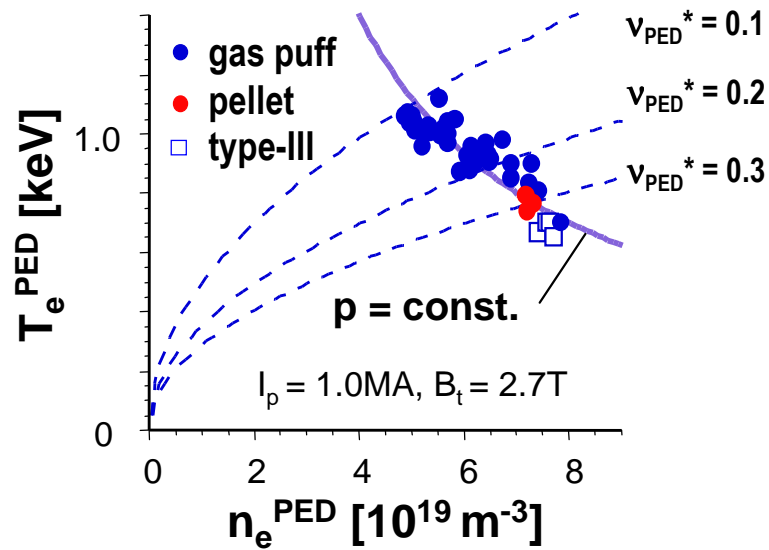
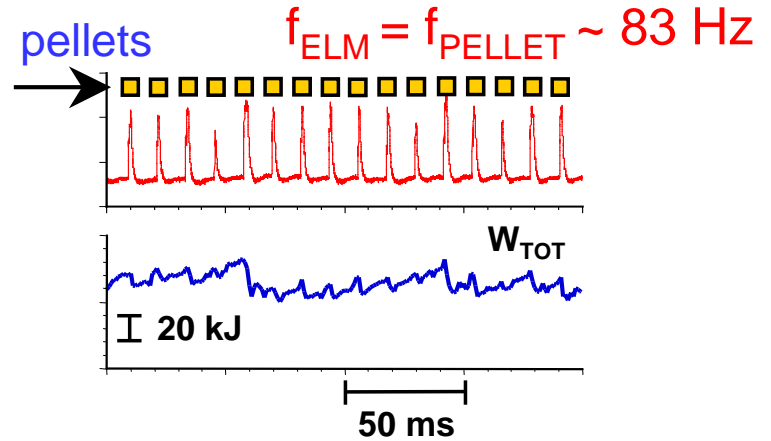
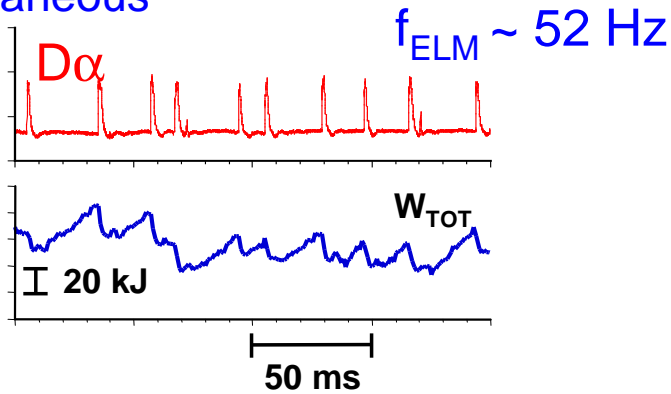




# Methods for control of Type I ELMs

Pellet triggering of ELMs: (H. Urano, AUG (P))

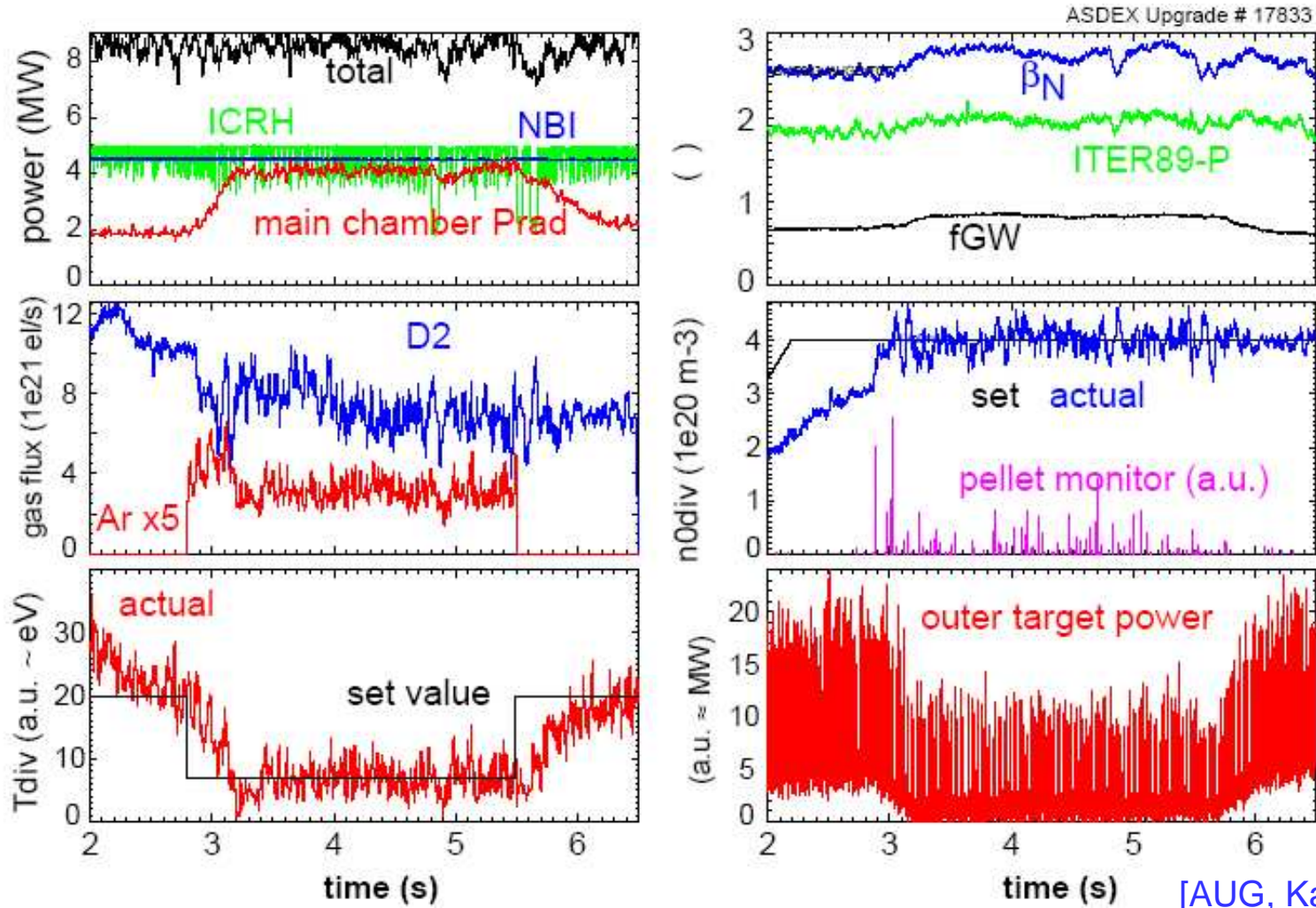
Spontaneous



Pellet injector: Easy extrapolation to ITER. (R)

# Methods for control of Type I ELMs - Example

Combined techniques: Impurity seeding + Pellet triggering of ELMs



[AUG, Kallenbach, '03]

Add pellets to avoid radiation „run-away“ with Ar-seeding

# Methods for control of ELMs

## Edge current variations:

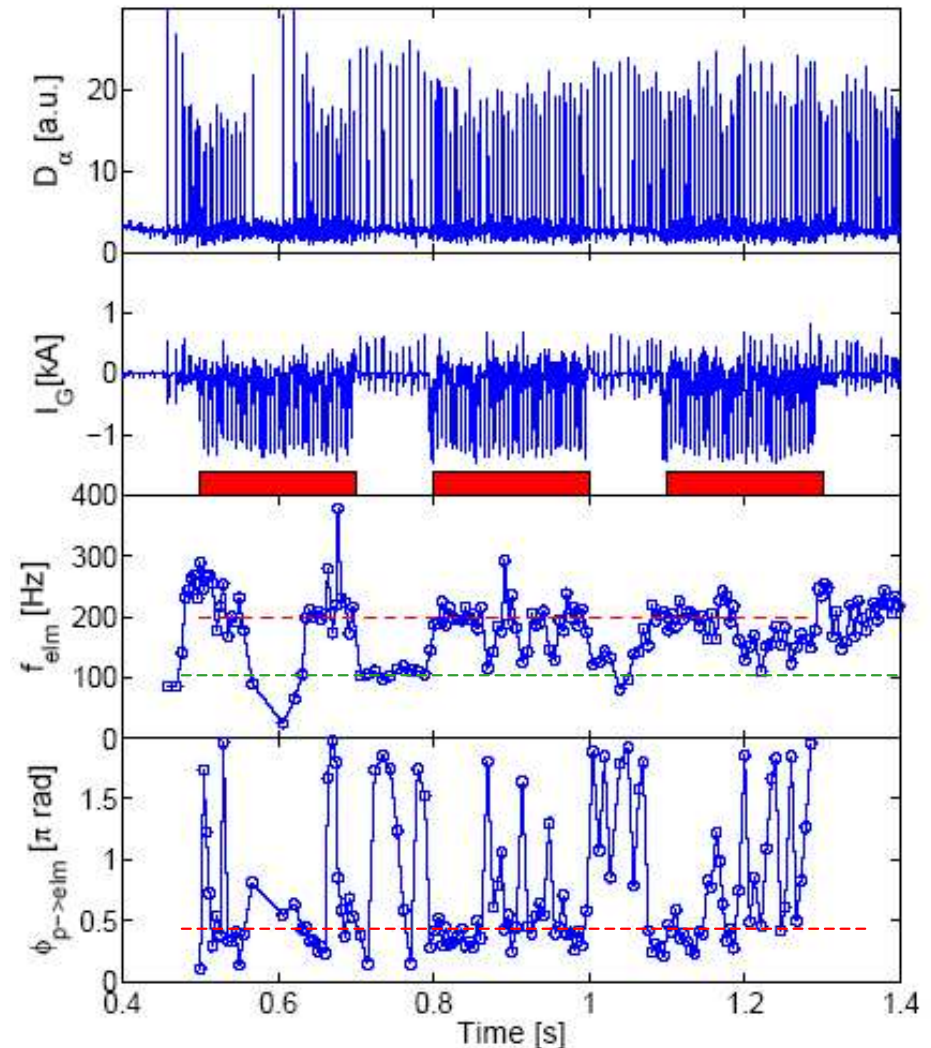
Change the stability of the ELMs.

Results from COMPASS-D, JET and JT-60U with  $I_p$  ramps report  $f_{ELM} \uparrow$ , at higher edge currents.

BUT, TCV demonstrates control of  $f_{ELM}$ . + model + prediction for use in larger devices.

Oscillations on  $\sim 1$  s. timescale would be enough in ITER-FEAT with external coils (AC losses ?). **(R)**

[Degeling, PPCF 45 '03, 1637] TCV, #24542



But, Type III ELMs

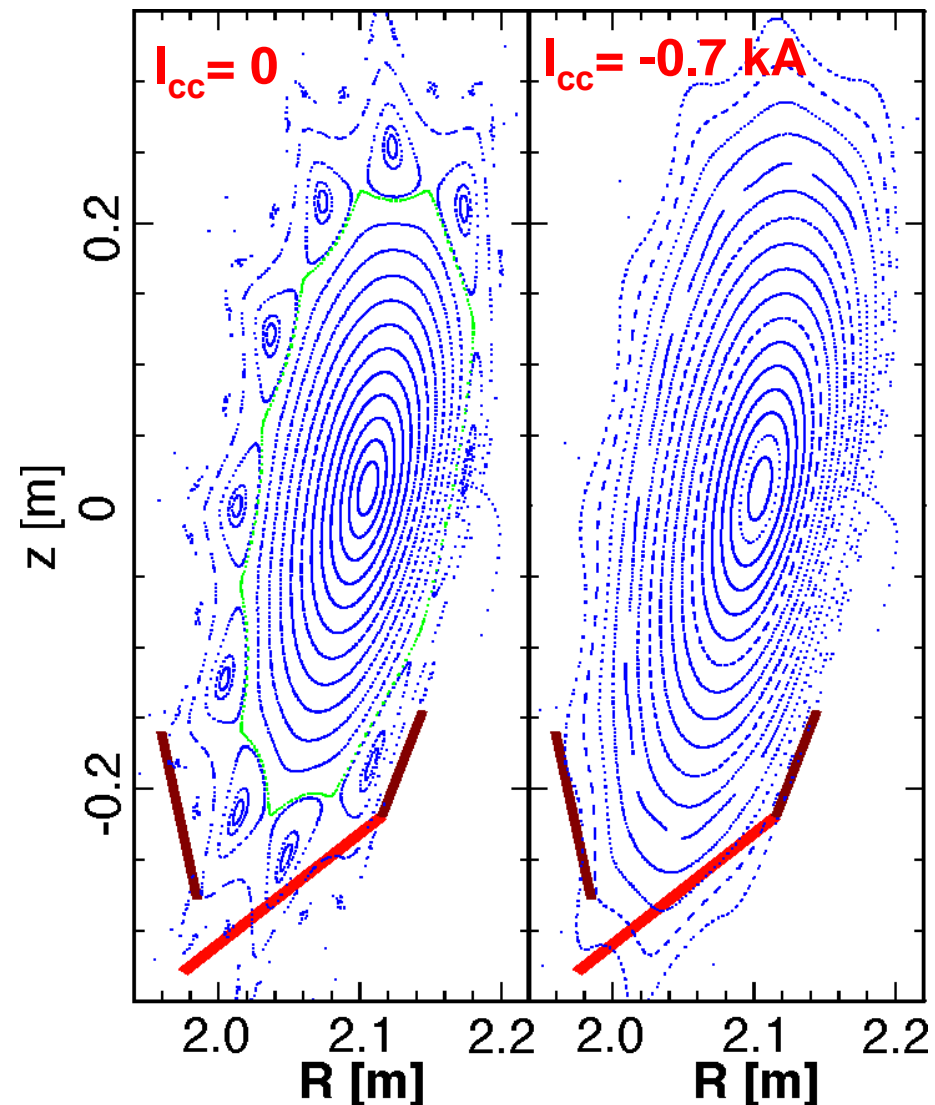
# Methods for control of Type I ELMs

[W7-AS, Weller, EPS'03]

## Ergodisation of the edge:

- Technique for limiter machines (Tore Supra) or helical devices
- W7-AS, high density H-mode without ELMs.
- Combination of poloidal divertor and ergodic edge (JFT-2M, COMPASS-D).
- Very recent results of DIII-D, ELMs suppressed completely [PRL to be submitted]:
- To start: TEXTOR-DED.

## Calculated Vacuum Surfaces



Ergodisation in a reactor ? (**D**)

High  $v^*$

← Today's experiments →

Low  $v^*$

Type II ELMs (AUG):

Control of plasma shape near  
DNX,  $n_e/n_{GW} > 0.85$ ,  $q_{95} > 3.5$ .

EDA Mode (C-Mod):

High recycling with reactor  
relevant heating. No ELMs at all.

Quiescent H-mode (DIII-D):

counter NBI, no ELMs at all.  
Rotation control  
(Sakamoto, JT-60U, (P))

Type III + ITB (JT-60U, JET):

Requires ITB to keep  $H_{98} \sim 1$   
with all their control issues.

at lower  $v^*$  ?

at higher  $n_e/n_{GW}$  ?

Are these our safeguard against a worst case scenario ? (D)



Edge barrier control, reactor relevance (mainly focussed on Type I ELMs):

- Impurity seeding in conjunction with other mitigation schemes.
- Pellet trigger of ELMs has easy extrapolation to ITER.
- PF current oscillations at  $\sim 1$  s.  $\rightarrow$  ITER-FEAT with external coils.
- Edge ergodisation is technical challenge, but RWM stabilisation for advanced scenarios is taken for granted in ITER-FEAT.

Edge barrier control, discussion points

1. Predictions for energy loss per ELM for ITER-FEAT
2. Spherical tokamaks, L  $\rightarrow$  H in DNX, applicable to tokamak (reactor) ?
3. Is ergodisation a possible ELM mitigation method for a reactor ?
4. Scenarios without type I ELMs, our safeguard against a worst case scenario for a burning plasma (no type I ELMs allowed) ?
5. More discussion points.....

# B: Control of Internal Transport Barriers

### Posters with this Topic:

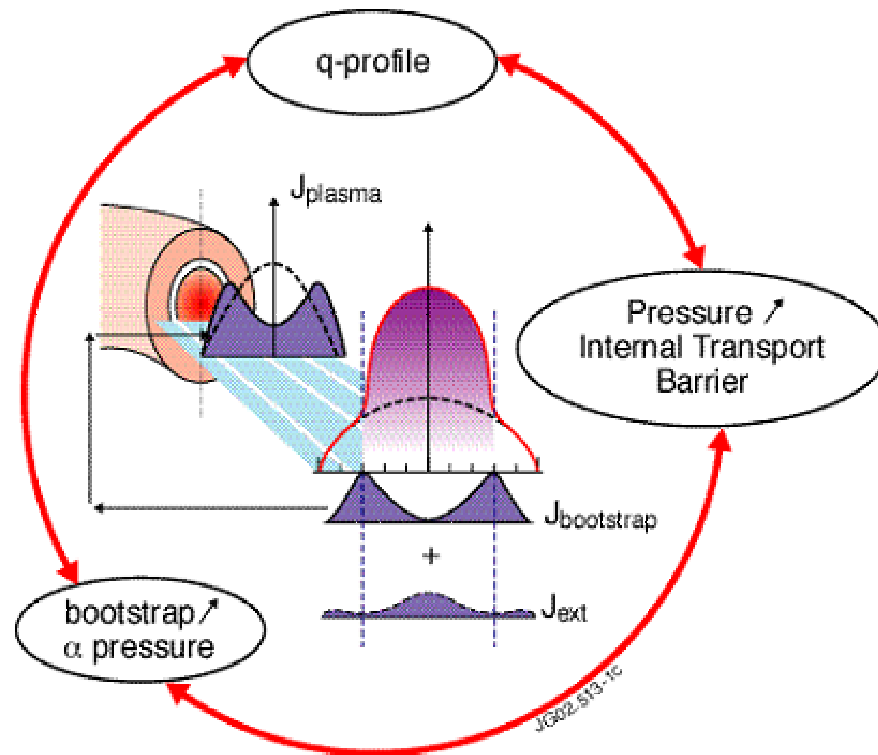
- D1: C. Fiore, Progress in Alcator C-MOD Internal Transport Barrier Studies.
- D2: M. Henderson, Creation and Control of eITBs in Stable Plasma Conditions on TCV.
- D3: T. Minami, Formation of Neoclassical Internal Transport Barriers under Various Operational Regimes on CHS.
- D4: D. Mazon, Real-time control of the current density profile in JET.
- D5: H. Meyer, Formation of transport barriers in the MAST spherical tokamak.

Poster presentations indicated during this talk: *(P)*



# Control of internal transport barriers

Control requirements driven by the desire to obtain, optimise and sustain the improved core confinement to create an advanced scenario.



## Areas for active control:

- Avoid global beta limits,
- MHD....resistive wall modes,
- q-profile,
- ITB strength, radius, duration.

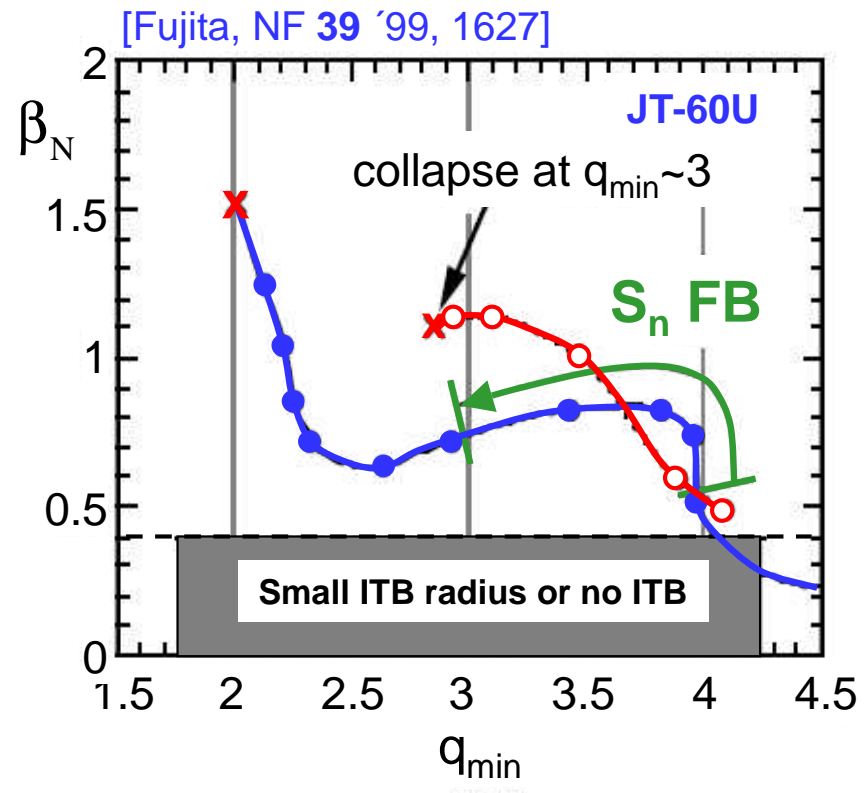
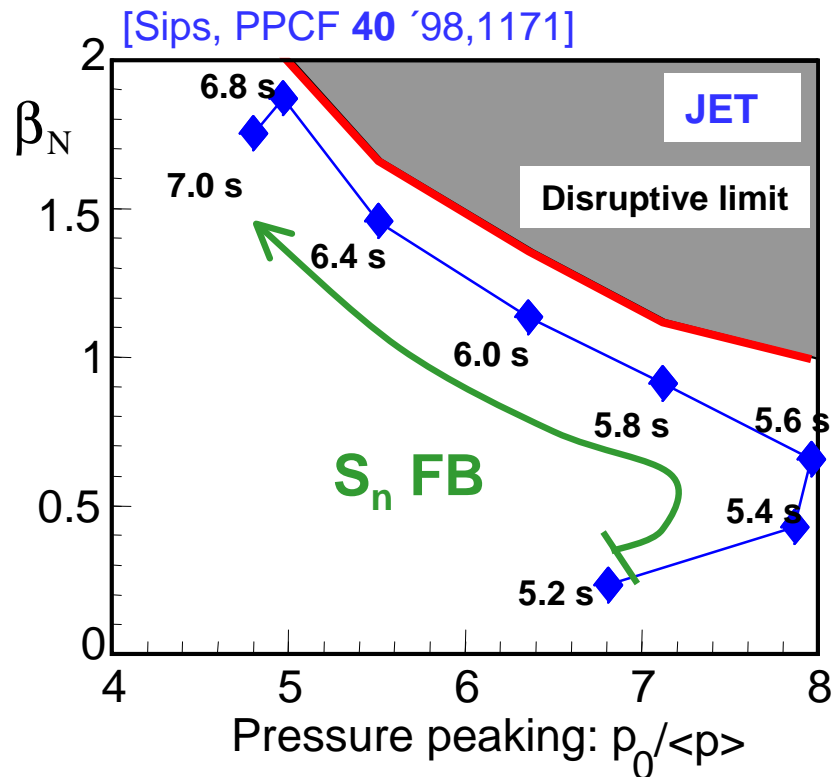
Control of the edge as discussed before ? (**D**)

# Control of ITB's: Beta limits

*Avoiding global beta limits:*

First type of control for ITBs with  $R_{DD}$  using input power to avoid disruptions:

Reduce power during peak pressure profiles or when  $q_{min}$  crosses rationals



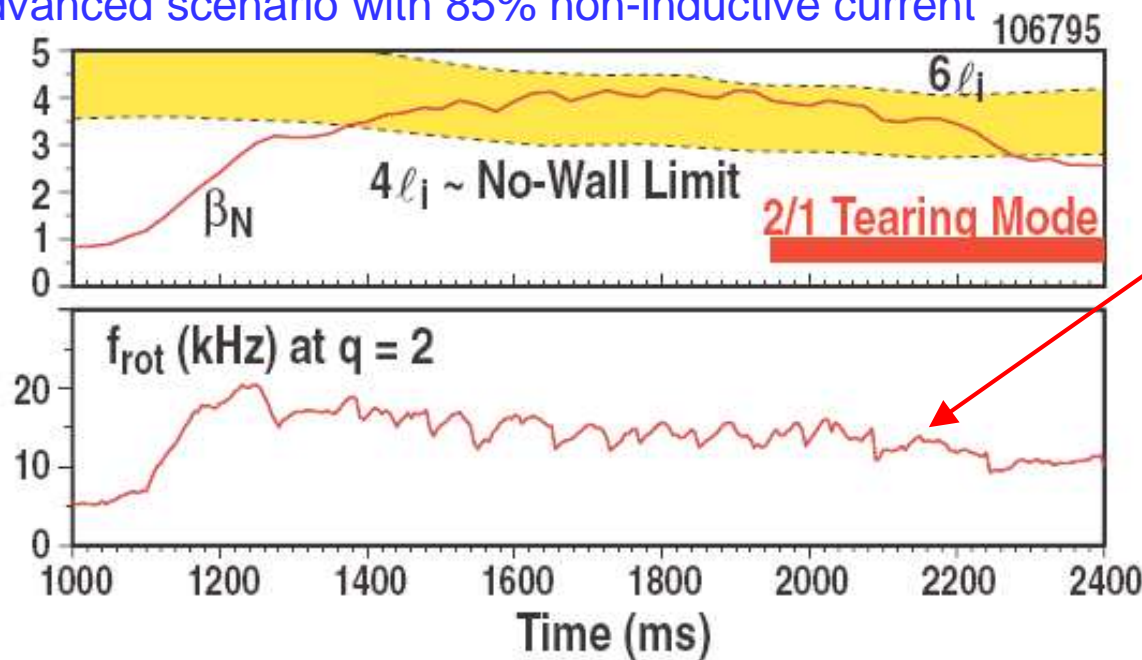
This type of control can not be used when  $\alpha$ -power is main heating source (**R**)

# Control of ITB's: Beta limits

*MHD....resistive wall modes,*

Feedback control of RWMs by rotational drive or flux conserving intelligent coils are crucial to operate at  $\beta_N \sim 3.0-3.5$  [Lao, PPCF 45 '03. 1023].

Advanced scenario with 85% non-inductive current



[Wade, NF 43 '03, 634]

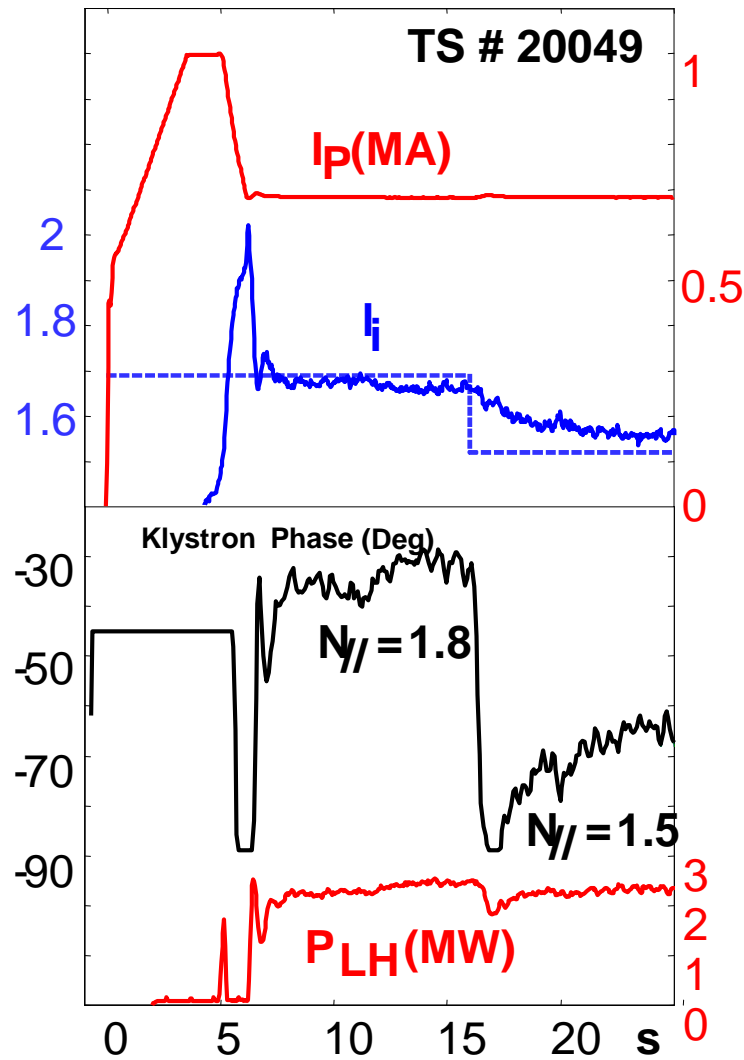
Rotation remains since external coils (C-coils) correct  $n=1$  error fields in feedback (DIII-D).

JT-60U: Plasmas with larger minor radius,  $\beta_N \uparrow$  ( $\sim 10\%$ ) [Kamada, NF 41 '01, 1311].

Conduction wall + control coils for a reactor, difficult but possible ? (D)

# Control of ITB's: q-profile control

Control of  $q(r)$ , with ECCD, (LHCD),NBCD + PF coils:



[Mazon, EPS '03]

Pre-programmed  $\Rightarrow$  Closed loop systems

**Without ITB:** Obtain desired  $q(r)$  at low  $\beta$ .

Vertical flux  $\Leftrightarrow$  ohmic generator

Plasma current  $\Leftrightarrow$  LHCD power

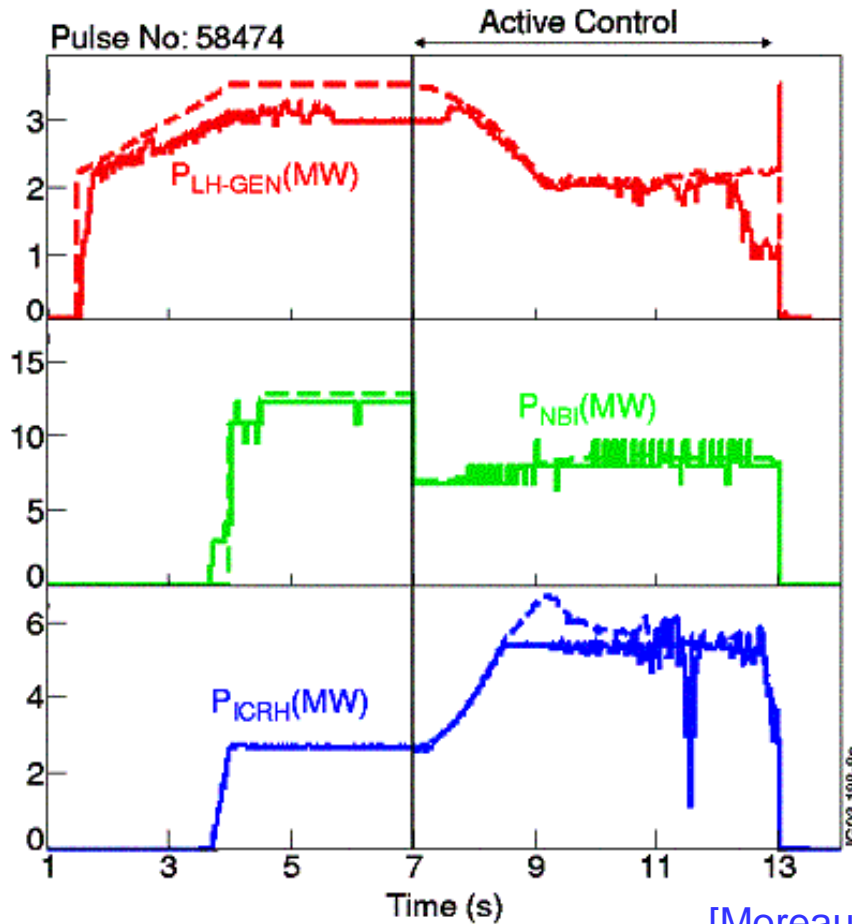
Internal inductance  $\Leftrightarrow$  LH parallel index

Tore Supra: Unique measurements with hard X-rays of LHCD deposition profile.

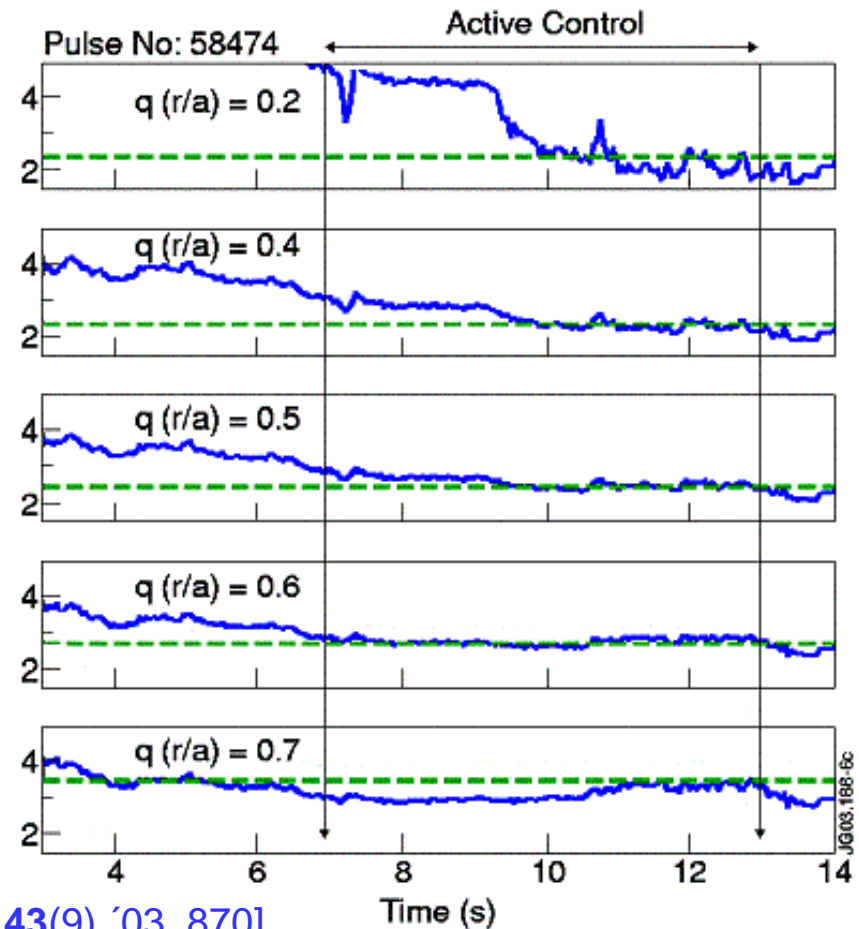
Can be combined with control on  $T_{surf}$ . (**R**)

# q-profile control - Example

JET: target  $q(r)$  or  $q(r)$  during weak ITB phase (low  $\beta$ ), multiple actuators.



[Moreau, NF 43(9) '03, 870]



Control matrices from modelling or from step response in experiments ? (**D**)

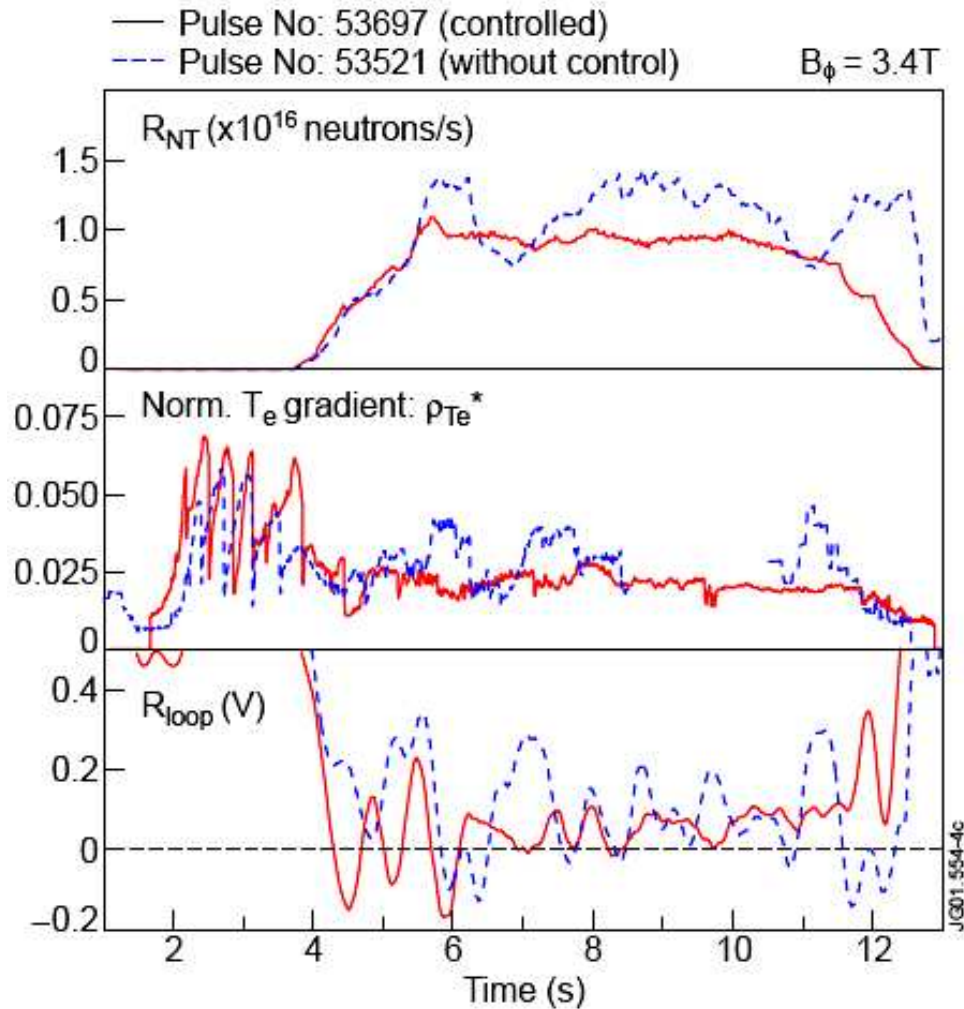
Need to control  $q(r)$  and  $p(r)$  to be reactor relevant ! (**R**)

1. Control of the rotation shear with NBI in TFTR (old result). Similar results for JT-60U using NBI (Sakamoto, *(P)*).
2. Strong dependence of type of barrier obtained with q-profile (reversed, flat or weak shear in JT-60U) or rational q-surfaces (JET).
3. Barrier for  $n_e$  depends on  $B_T$  with off-axis ICRH in C-Mod (rotation increase is observed) (Fiore, *(P)*)
4. Quiescent H-mode + ITB (QDB): avoid erosion of ITB due to ELMs, counter NBI. DIII-D:  $\beta_N H_{89} \sim 7$  for  $> 3.8$  s , need ECCD to control  $q(r)$ .

Rotation profile control in a reactor ? (*D*)

# ITB radius, strength and duration - Example

[Mazon, PPCF 44 '02,1087]



## Closed loop control: JET

ICRH  $\Leftrightarrow \rho_T^*$

NBI  $\Leftrightarrow$  neutron rate

LH holds the q-profile

Ion and electron ITB's,

- More stable at lower beta.
- No impurity accumulation.
- Edge: Type III ELMs.

What about higher beta ? (**D**)

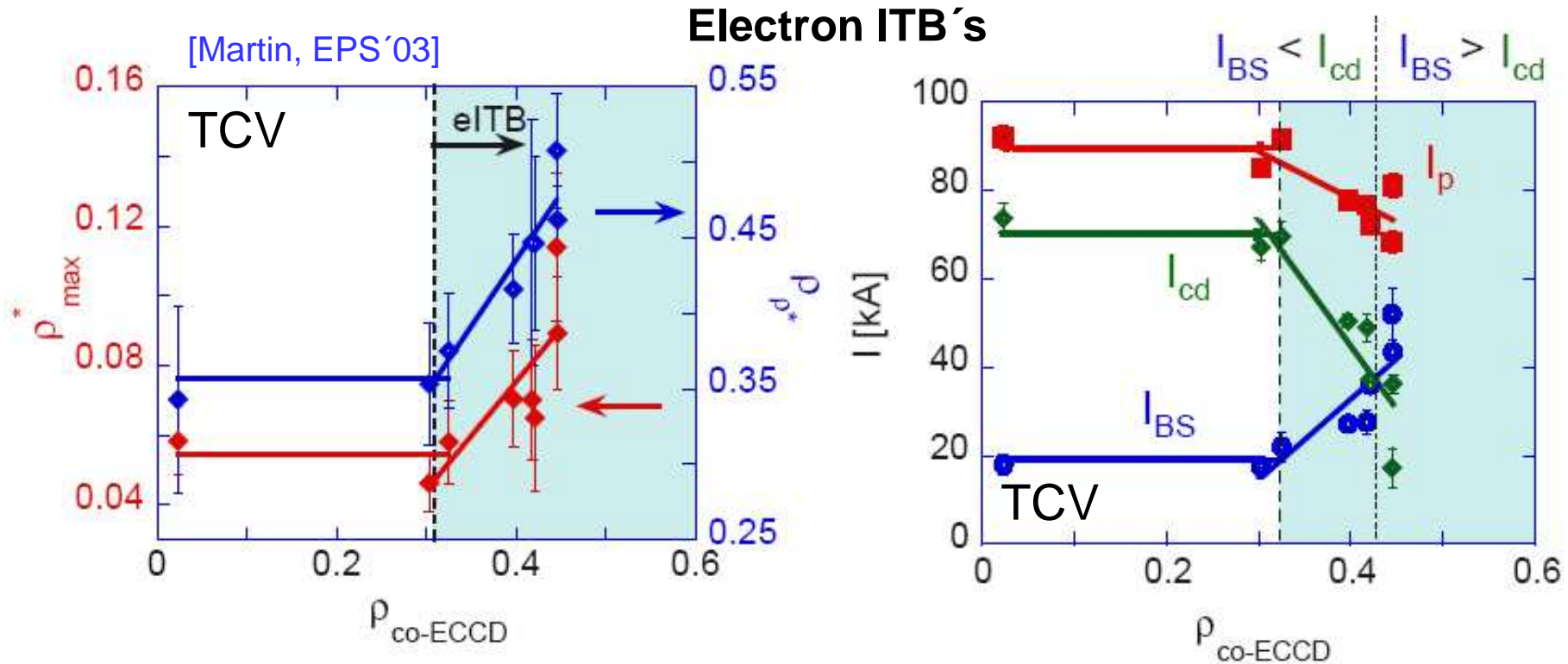
What about the ELM type ? (**D**)

Plan: Also control  $q(r)$  (**Mazon, (P)**)



# ITB radius, strength and duration - Example

Experiments at higher beta: more bootstrap current fraction.



Full non-inductive: Flexible ECCD systems of TCV maximise ITB with off-axis **co-ECCD** (loses efficiency). **Counter ECCD** could be used but then, inductive scenario (**Henderson, TCV (P)**).

How much power for ECCD and NBCD in ITER would you need ? (**D**)

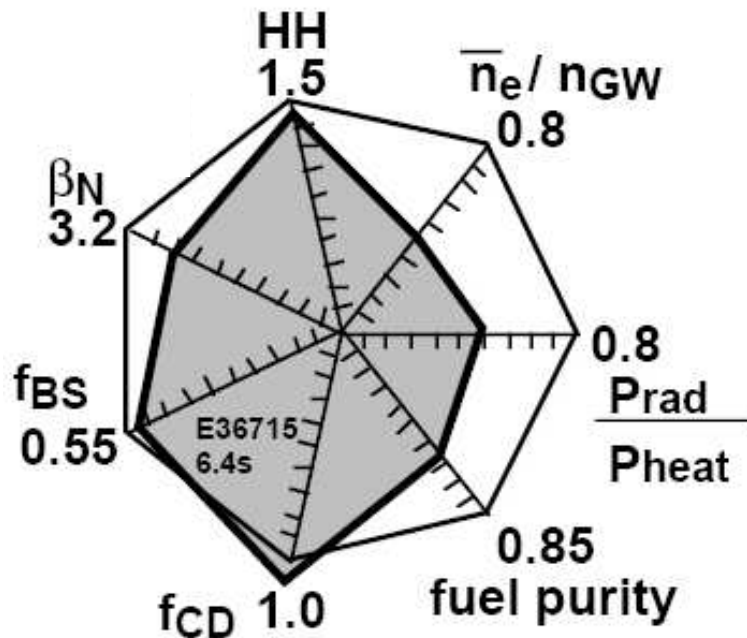
# Lets review the situation.....

**Control of MHD:**  $p_0/\langle p \rangle$  and RWM stabilisation, avoid disruptions.

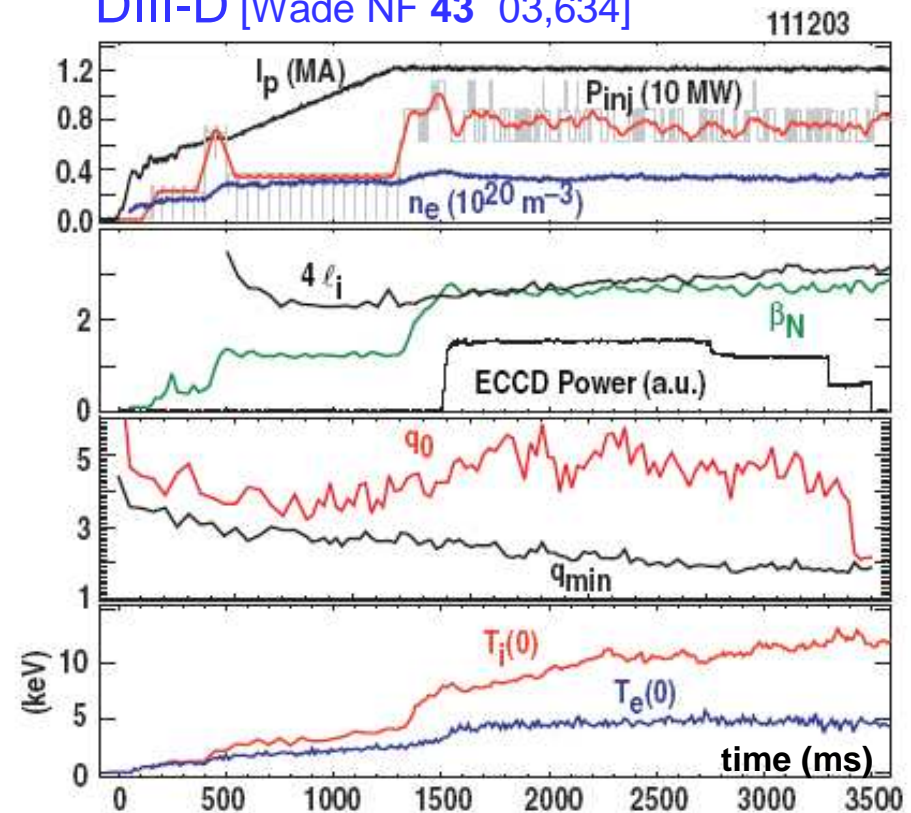
**Control of  $q(r)$ :** Target  $q(r)$ , or keep  $q(r)$  at low beta (so far).

**Control of ITB:** Dramatic improvement of  $H_{89}\beta_N$  with control ?

JT-60U [Kamada NF 41 '01,1311]



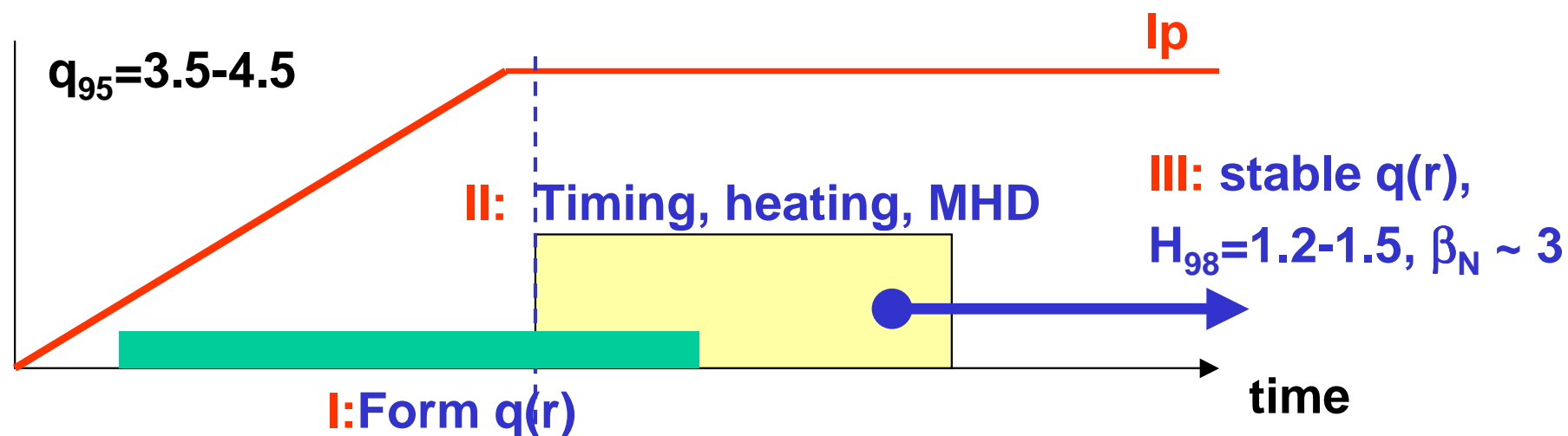
DIII-D [Wade NF 43 '03,634]



Why not minimise control requirements using self-consistent scenario (D) ? 

## Hybrid scenario:

AIM: Improve core confinement and  $\beta$ , **without need for stringent control**



**I:** Obtain low central shear,  $q_0 \sim 1$ , no sawteeth (no ITB !)

**II:** Apply main heating to obtain  $\beta_N \sim 2-2.5$  + mild MHD.

**III:** Extend heating, raise to  $\beta_N \sim 4I_i$  with stationary  $q(r)$ . Edge: Type I Elms.

Developed at ASDEX Upgrade and DIII-D:  $\underline{H_{89}\beta_N \sim 7}$ ,  $I_{CD}/I_p \sim 50\%$

[ASDEX Upgrade, Sips PPCF 44 '02 A151

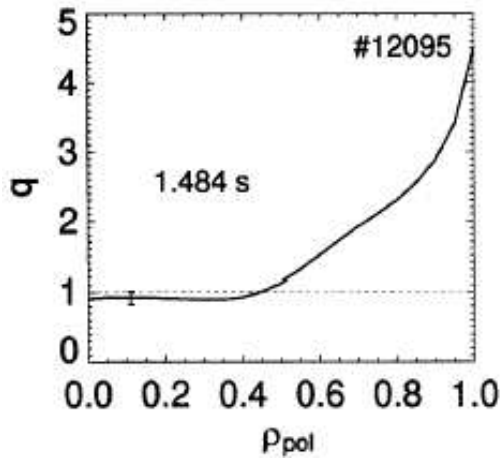
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DIII-D, Luce NF 43 '03,321]

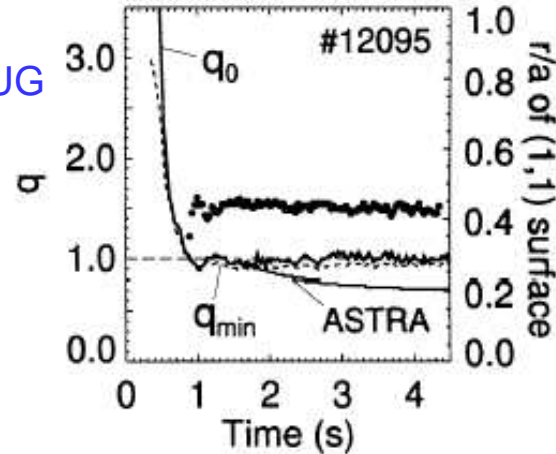
# Hybrid scenario: Advanced with minimum control ?

q-profile is stationary without control, MHD events play key role:

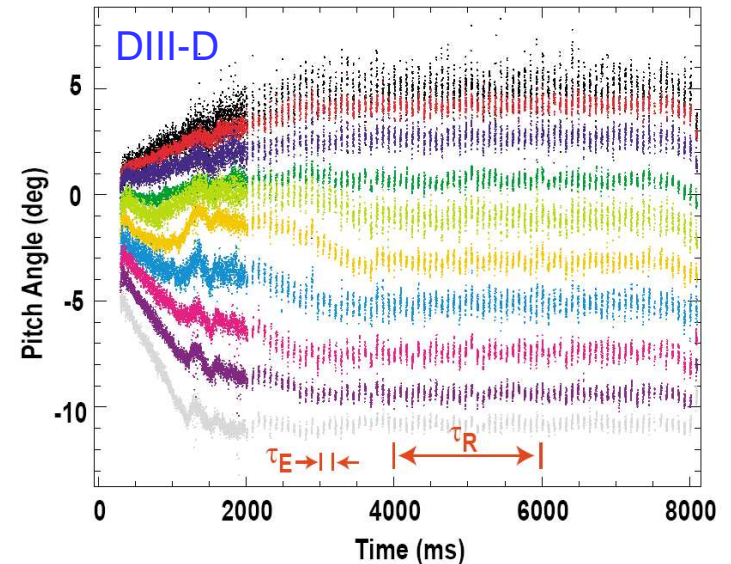
Fishbones, [Wolf PPCF 41 '99, B93]



AUG



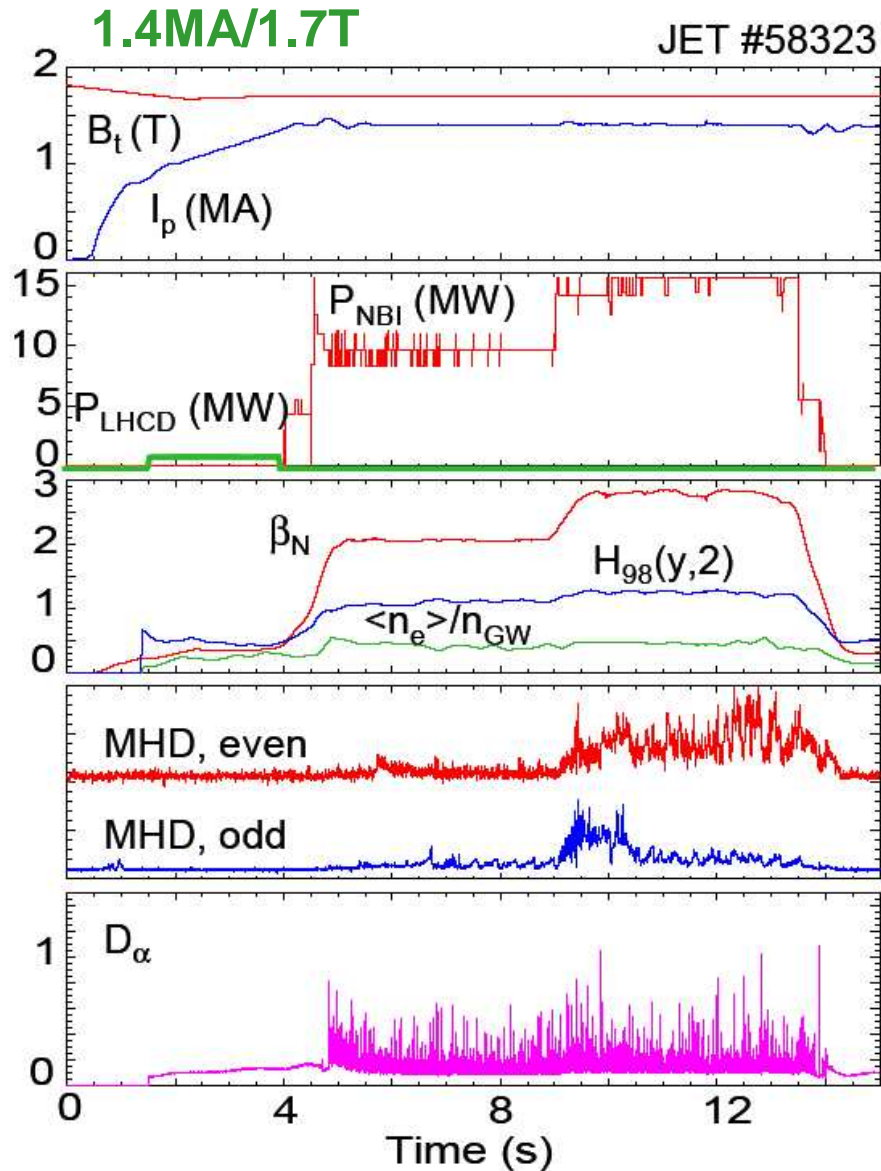
3/2 NTM, [Luce IAEA '02]



High beta ( $\beta_N \sim 4l_i$ ) without ITB: Transport analyses in AUG and DIII-D, show that, although profiles are peaked, core transport is driven by ITG and ETG/TEM turbulence (profiles are stiff).

How does this regime extrapolate to a reactor ? (**D**)





## Experiments at JET [Sips EPS '03].

- establish hybrid scenario, with non-dimensional parameters similar to AUG (DIII-D)
- make them stationary.
- document differences (if any) when going to lower  $\rho^*$ .

## Map existence domain [Luce EPS'03]

- Experiments at AUG & DIII-D.
- For which  $q_{95}$  and density ( $0.3 < n_e / n_{GW} < 1$ ) ?

With  $I_{CD}/I_p \sim 50\%$  not steady state ! (**R**)

Internal barrier control and sustain (edge control?):

- Simple control on reaction rate can not be used to avoid disruptions in ITB plasmas when  $\alpha$ -power is main heating source in core.
- Need to control  $q(r)$  and  $p(r)$  to be reactor relevant at high beta !
- Control of profiles with control on  $T_{\text{surface}}$  of first wall.
- Hybrid scenario: minimum control, why  $q_0 \sim 1$  without sawteeth ?

Internal barrier control, sustain:

1. Control of the edge (e.g ELMs) for ITB plasmas ?
2. Control matrices: modelling or step responses in experiments ?
3. Rotation profile control in a reactor OR impurity accumulation?
4. Should go to higher beta soon (better ITB  $\rightarrow$  impurity accumulation ?)
5. How much power for ECCD and NBCD in ITER would you need ?
6. More discussion points.....