

Fusion Ignition Research Experiment (FIRE)

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Introduction

The major next steps in magnetic fusion energy need to address the following critical fusion plasma issues:

Burning Plasma Physics - The achievement and understanding of self-heated plasmas with high gain that have characteristics similar to those expected in a fusion energy source, and

Advanced Toroidal Physics - The achievement and understanding of sustained self-heated plasmas with characteristics (steady-state or high duty factor pulsed systems) similar to those expected in a competitive fusion system

The tokamak is technically ready to address these issues. The plasma performance and duration to study these issues are shown schematically in Fig.1 in terms of the natural time scale for the important plasma processes.

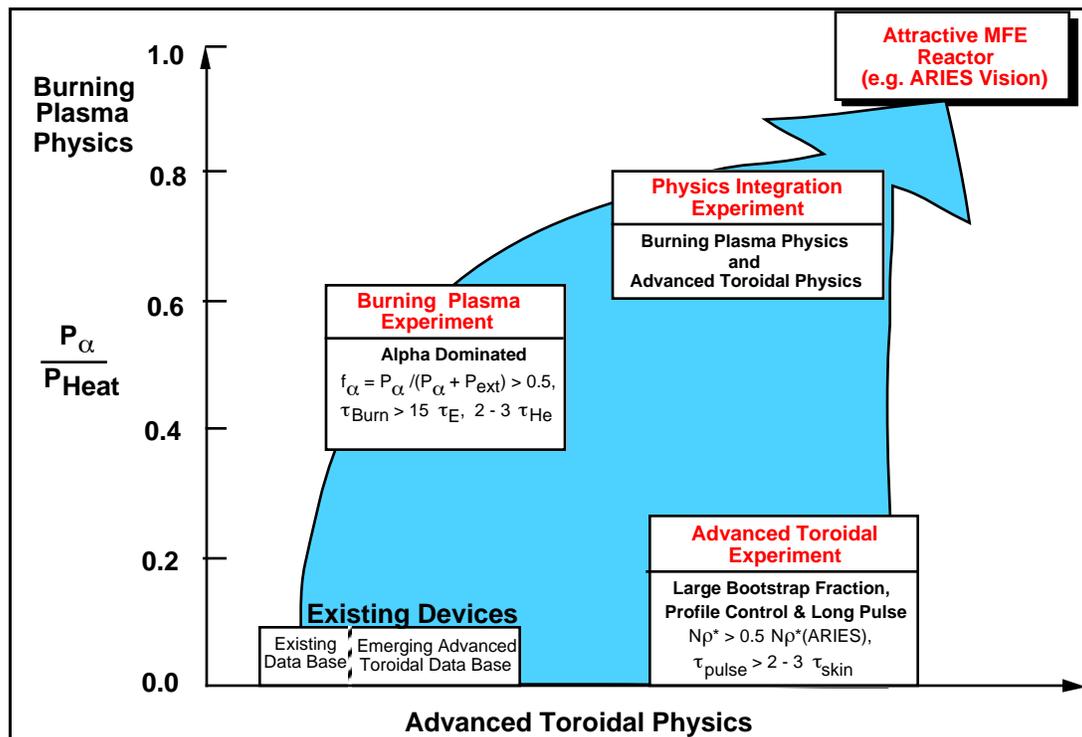


Fig. 1. The stepping stone approach for developing the science foundation for an attractive MFE system.

This report documents the results of a study to evaluate the capability of compact high field tokamaks to address the alpha-dominated burning plasma physics, long-pulse advanced-toroidal physics and fusion technology as part of a Modular Pathway to Magnetic Fusion

Energy (MFE). The conclusion is that a compact high field tokamak utilizing LN cooled copper-alloy coils has the capability to address a major portion of both the Burning Plasma Experiment Step, the Advanced Toroidal Experiment Step and also has significant capability to integrate burning plasma physics with advanced toroidal physics. The device studied resembles CIT. The plasma configuration was drawn from TPX and is a $\approx 1/3$ scale model of ARIES-RS. The size was constrained with the goal to achieve the most important physics goals at a construction cost of $< \$1B$.

The Next Frontier in MFE Research - Exploration, optimization and understanding of alpha-dominated burning plasmas.

The attainment and control of a high Q plasma dominated by alpha heating is the single most important requirement for any approach to fusion power. Fusion gains $Q \sim 20$ are needed for an economical magnetic fusion reactor that is sustained at near steady-state conditions; at this Q value the alpha particles dominate the plasma dynamics, providing 80% of the plasma heating. The goal for the Next Step in Magnetic Fusion is to access sustained alpha dominated plasmas with alpha heating fractions more than an order of magnitude higher than present experiments.

The advanced tokamak, advanced stellarator and the spherical torus plan to have the bootstrap current, generated by gradients in the pressure profile, produce a large fraction of the current needed to define the stabilizing magnetic field. Since the alpha heating profile is directly linked to the pressure profile, this process becomes very non-linear in the alpha-dominated plasmas required for a fusion reactor based on an advanced tokamak. This coupling of advanced tokamak confinement and MHD stability physics with alpha-dominated plasmas is a key generic issue for the development of attractive toroidal magnetic reactors.

Fusion Ignition Research Experiment (FIRE)- A Next Step Option for MFE.

The mission of FIRE is to attain, explore, understand and optimize alpha-dominated plasmas that will provide the knowledge for attractive MFE systems. The guiding design philosophy is that FIRE must have the capability and flexibility of studying and resolving the physics issues relevant to the design of a subsequent advanced integrated fusion facility. A major consideration is to accomplish this physics mission at the lowest possible cost, with a target cost $< \$1B$. This report summarizes the first nine months of a study to evaluate the physics and engineering capabilities of a compact high field tokamak utilizing cryogenically-cooled copper-alloy coils to accomplish this mission.

FIRE Physics Objectives

The physics objectives of FIRE developed to satisfy the mission are to:

1. Determine and understand the conditions required to achieve alpha-dominated plasmas:
 - Energy confinement scaling with alpha-dominated heating
 - β -limits with alpha-dominated heating
 - Density limit scaling with alpha-dominated heating
2. Explore the dynamics of alpha-dominated plasmas using active control techniques.
3. Sustain alpha-dominated plasmas with high-power-density exhaust of plasma particles and energy and alpha ash exhaust in regimes suitable for future toroidal reactors.

4. Explore and understand alpha-dominated plasmas in advanced operating modes and configurations that have the potential to lead to attractive fusion applications.
5. Understand the effects of fast alpha particles on plasma behavior in relevant regimes.

Alpha Heating Fraction, the metric for alpha-dominated burning plasmas

The alpha heating strength can be expressed in terms of $f_\alpha = P_\alpha / (P_\alpha + P_{ext})$ where P_α is the alpha heating and P_{ext} is the externally applied heating (ohmic + neutral beam + rf waves). The fraction of alpha heating, f_α , is plotted in Fig. 2 in terms of the ratio $\pi\tau_E / \pi\tau_E(Q = \infty)$. D-T experiments on TFTR and JET have measured small temperature increases in agreement with the expected alpha particle heating. The sustained D-T discharges on TFTR and JET had $Q \approx 0.2$ for ~ 10 energy confinement times with the alpha particles providing about 4% of the overall plasma heating. The vision of an MFE fusion reactor is ARIES-RS, an advanced tokamak with a $Q = 25$ which has $f_\alpha = 0.83$. The investigation of an alpha-dominated plasma can begin at $f_\alpha = 0.5$, and plasmas with $f_\alpha = 0.66$ to 0.83 would match the dynamics expected in the MFE reactor regime. Note that small reductions in confinement produce only small changes in the alpha heating fraction, while Q is sensitive to small changes in confinement, especially in the high Q regime.

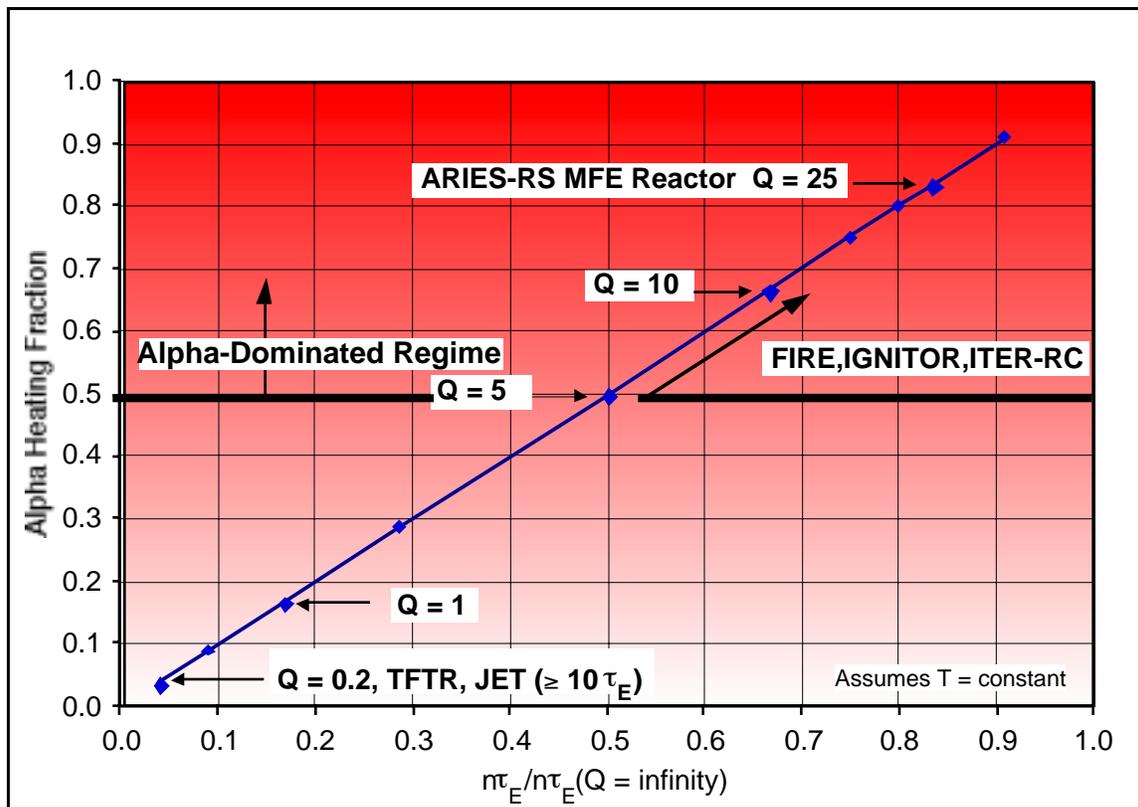


Fig. 2. Fraction of Alpha heating versus $\pi\tau_E / \pi\tau_E(Q = \infty)$ illustrating the alpha-dominated regime.

Choice of FIRE Plasma Performance Requirements.

FIRE is a physics experiment to extend the frontiers of fusion plasma physics into previously unexplored parameter space using advanced capabilities and flexibility for later

upgrades; it is not a demonstration of the scientific and technological feasibility of magnetic fusion. The strategy for the FIRE program is to have a first stage of burning plasma experiments aimed at accessing the alpha-dominated regime with a minimum f_{α} of ≥ 0.5 using projections from the middle of the present tokamak performance database. This would provide a test bed where alpha heating effects are easily observable, and the plasma dynamics could still be controlled externally. This capability is the natural starting point for an experimental campaign to study alpha-dominated plasmas and would be sufficient to accomplish a significant fraction of the stated objectives. The goal for the second stage of burning plasma experiments is to achieve strongly alpha-dominated plasmas with $f_{\alpha} = 0.66$ to 0.83. This level of performance is projected from the best results of the present tokamak performance database, or by a modest 20% improvement in confinement from employing advanced tokamak physics that is expected to be developed by the ongoing base tokamak program over the next 5 years.

The pulse length, or the burn time, is a very important consideration for any burning plasma experiment. The physics time scales of interest (with typical values for FIRE plasmas) are:

- $\tau_{\alpha S}$, the time needed for the alpha particle to transfer its energy to the plasma (~ 0.1 s)
- τ_E , the plasma energy confinement time (~ 0.6 s)
- τ_{He} , the confinement time of alpha ash, slowed down alpha particles ($\sim 5 \tau_E \sim 3$ s)
- τ_{cr} , the time for the plasma current profile to redistribute after a perturbation (~ 13 s)

The characteristic time scales for plasma phenomena in FIRE plasmas are significantly shorter than the corresponding time scales on ITER-RC due to the smaller size, higher density and somewhat lower plasma temperature as shown in Table I.

Table I. Characteristic time scales for plasma phenomena in FIRE and ITER-RC.

For $Q \approx 10$	τ_E (s)	τ_{He} (s)	τ_{cr} (s)	τ_{burn} (s)
FIRE	0.6	3	~ 13	15
ITER-RC	2.5	7.5	~ 200	450

(Burn times are for inductively driven plasmas)

A FIRE plasma with a burn time of 15 s ($\sim 25 \tau_E$) would allow the pressure profile to come into equilibrium with alpha heating and allow the alpha ash to accumulate for $\sim 5 \tau_{He}$. This pulse length would be sufficient to address Physics Objectives 1, 2, 3, and 5. A significant part of Physics Objective 4 could be accomplished using a current profile that is only partially redistributed with $\tau_{cr} \sim \tau_{burn}$ as in the full field FIRE. In fact, it would be advantageous to establish a variety of plasma current profiles using current ramping as in present advanced tokamak experiments. A pulse length of $\sim 3\tau_{cr}$ would be sufficient to allow the bootstrap driven current in an advanced tokamak mode to come to within 5% of equilibrium. These pulse length requirements match the capabilities of liquid nitrogen (LN) cooled copper coils, which can be designed to allow a burn time of ~ 20 s at full toroidal field. If advanced tokamak physics improves confinement relative to ITER design guidelines by 25% and β by 50%, then the toroidal field and plasma current can be reduced by 25% while maintaining high plasma performance (e.g., $Q \sim 10$). This small reduction in the field of the FIRE copper magnet cooled to LN temperatures would allow the burn time to be increased to ~ 40 s $\sim 3\tau_{cr}$.

FIRE Device Parameters for Initial Evaluation

The FIRE plasma configuration is an extension of the advanced tokamak programs on DIII-D and Alcator C-Mod, and is a $\approx 1/3$ scale model of ARIES-RS, the present vision for an

advanced tokamak fusion reactor. The FIRE plasma has a size and shape very similar to the previously proposed advanced tokamak (TPX), with the added capability of high performance D-T operation. The capability of FIRE to carry out long-pulse non-burning plasmas experiments will be described in a later section. FIRE will have the flexibility to incorporate new innovations as the ongoing advanced tokamak program develops them. The parameters summarized in Fig. 3 were chosen as likely to achieve the FIRE mission at the lowest cost based on results of prior design studies for burning plasmas experiments (CIT, BPX and BPX-AT), as well as recent information from the ITER-EDA and ITER-RC design activities. A more extensive list of parameters and features is given in Appendix 1.

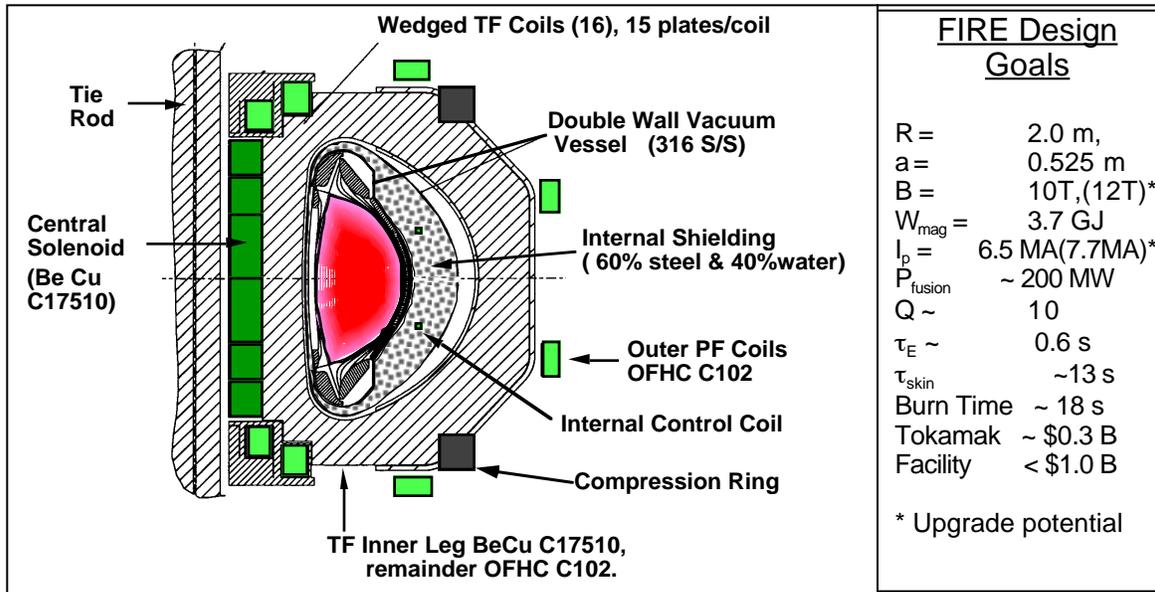


Fig. 3. Cross-section view and design goals of the FIRE.

Capability for Alpha-Dominated Burning Plasma Experiments on FIRE

The technical basis for a compact high-field tokamak like FIRE has improved markedly since the CIT ($R = 2.14$ m) and BPX ($R = 2.59$ m) studies of 1989-91. Tokamak experiments (1989 -1999) have led to the development of a new scaling relation (e.g., ITER-98H) which predicts 1.3 times higher confinement than the 1989 CIT design assumption. Alcator C-Mod, which can be considered as a prototype of FIRE, has come into operation and demonstrated:

- Confinement of 1.4 times the 1989 CIT design assumptions, ~ 15% higher than the ITER - 98H scaling.
- High power density ICRF heating of high density shaped plasmas with a divertor.
- Detached divertor operation at high power density.

In addition, D-T experiments on TFTR and JET have shown that tritium can be handled safely in a laboratory fusion experiment. The D-T plasmas behaved roughly as expected with slight improvements in confinement for the very weak alpha heating conditions available. The behavior of the energetic alpha particles was in agreement with theoretical expectations.

The plasma performance of FIRE is estimated using the guidelines similar to those used to project the performance of ITER. The primary considerations are the maximum density

limit, plasma energy confinement, the maximum pressure (β) limit, the power threshold for accessing the high confinement mode (Elmy H-mode) and limitations imposed by impurities due either to alpha ash accumulation or impurities from the first wall and divertor. FIRE assumes an operating density <0.7 of the Greenwald density closer to those in the ITER confinement data base rather than the higher values assumed in the ITER performance projections. FIRE assumes a slightly more peaked density profile (identical to that used in the CIT and BPX projections) than ITER due to the potential for tritium pellet injection into a much smaller high-density modest temperature plasma. The FIRE projections assume the ITER98 Elmy H-mode confinement scaling relation, $\beta_N \leq 2.5$ and the same H-mode power threshold formula as ITER. FIRE takes credit for lower impurity fractions ($\sim 3\%$ Be) characteristic of high-density tokamak plasmas. In particular, FIRE assumes no significant high-Z impurities in the plasma core.

It is important to note that while these guidelines are quite useful for estimating the $n\tau_E T$ performance of **existing** tokamaks to within 30%, the guidelines are mainly empirical with a modest amount of theoretical understanding and can not accurately predict the performance of a Next Step Burning Plasma experiment much less a technology demonstration. An affordable flexible experiment with a performance capability about midway between today's tokamaks and a fusion reactor is needed to benchmark physics understanding and to serve as a Stepping Stone to a reactor.

The strategy of FIRE is to minimize the extrapolation in τ_E , the most uncertain quantity. The fusion gain is maximized by maximizing $n\tau_E$ at a plasma temperature of ~ 10 keV. Analysis of the power balance in the plasma, first done by J.D. Lawson, shows that $n\tau_E$ values of $\sim 4 \times 10^{20} \text{ m}^{-3} \text{ s}$ are required to achieve Q values ~ 10 for a D-T plasma with modest impurity contamination and typical profiles. The compact high field tokamaks (IGNITOR and FIRE) reduce the requirement on τ_E by operating at densities almost an order of magnitude higher than larger lower field devices such as ITER. Operating in the high-density regime $n_e(0) = 6.75 \times 10^{20} \text{ m}^{-3}$ is a straightforward matter since Alcator C-Mod has already operated up to $\sim 10^{21} \text{ m}^{-3}$. For Q = 10, FIRE requires an energy confinement time, τ_E , of only ~ 0.6 s, which has been achieved in existing tokamaks such as JET, rather than the ~ 2.5 s required in the reduced size ITER or the 6 s required for ignition in ITER. The dimensionless confinement time, $B\tau_E$, is useful to quantify the extrapolation required in plasma energy confinement from present experiments to potential Next Step Options (Table II) for burning plasmas.

Table II. Extrapolation of dimensionless energy confinement time for potential Next Step Options.

	JET	FIRE (Q = 10)	ITER-RC (Q = 10)	ITER-EDA (Q = ∞)
$B\tau_E$ (T-s)	3	6	14	34

The extrapolation to Q ~ 10 conditions in FIRE is a factor of two beyond JET, while ITER-RC requires a factor of four extrapolation, and ITER-EDA required an extrapolation of ~ 11 to achieve the objective of ignition.

The plasma parameters for a nominal FIRE operating point were calculated using a zero dimensional model and the physics guidelines. The alpha heating fractions for FIRE and ITER-RC are illustrated in Fig. 4 under the assumptions of modestly peaked density profiles (triangles) and flat density profiles (crosses). The initial design point selected for FIRE satisfies all of the standard tokamak design guidelines needed to access the alpha dominated range with $P_\alpha / P_{\text{heat}} \geq 0.5$ (Q ≥ 5). This represents more than an order of magnitude advance beyond the capability of TFTR/JET to study alpha driven physics, and

would provide a checkpoint more than half way to the alpha heating fraction $P_{\alpha}/P_{\text{heat}} \geq 0.8$ required in a fusion reactor.

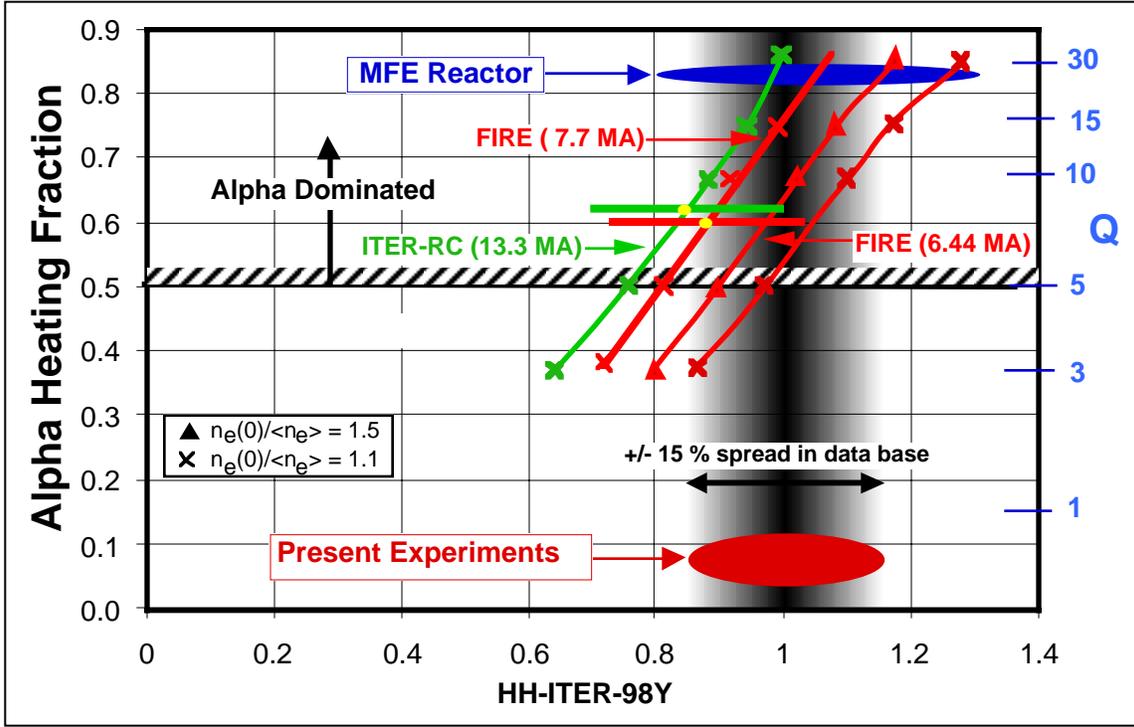


Fig. 4. Performance of FIRE and ITER-RC versus H-mode multiplier. HH = 1.0 is the center of present tokamak H-mode data base (ITER DB3). The triangles are for slightly peaked density profiles, $\alpha_n = 0.5$. The MFE reactor points are for ARIES-RS at densities ranging from 1.0 to 1.8 times the Greenwald density.

The performance projections (Fig. 5) indicate that FIRE is also capable of exploring strongly alpha-dominated regimes with $P_{\alpha}/P_{\text{heat}} \geq 0.66$ ($Q = 10$ to 30) if the relatively higher performance ($H98 = 1.2$) of the smaller compact high field tokamak, Alcator C-Mod, or the top end of the JET confinement results are obtained at burning plasma conditions in FIRE. During the next ten years the ongoing world wide advanced tokamak program is expected to provide additional improvements of at least $\sim 25\%$ in confinement and 50% in β . This capability would allow FIRE to explore “ignited” plasma conditions with $P_{\alpha}/P_{\text{heat}} \geq 0.8$ (Q up to 30) at reduced fields and longer pulses with burn duration comparable to several plasma current redistribution times.

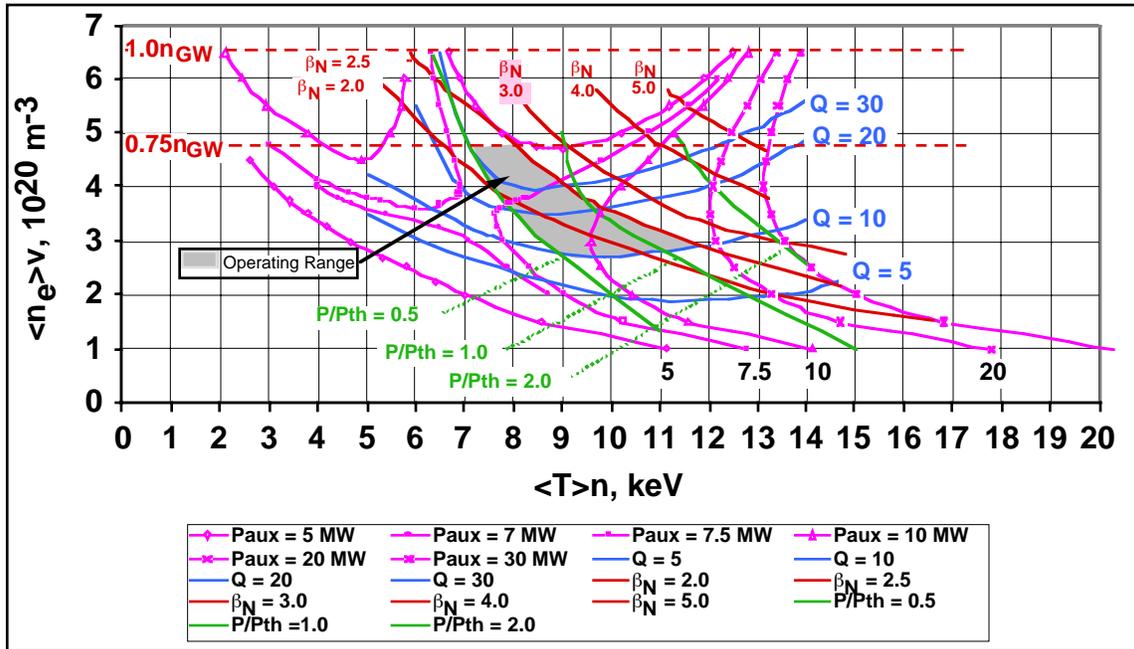


Fig. 5. High Gain ($Q > 10$) FIRE operating range with an ITER-98 H-mode factor = 1.2, $\beta_N \leq 2.5$, $P_{\text{heat}} \geq 1.0 P_{\text{th}}$ to access H-mode and $P_{\text{heat}} \geq 0.5 P_{\text{th}}$ to remain in the H-mode while satisfying a density limit of $n/n_{\text{GW}} \leq 0.75$.

Success with FIRE would establish the basis for an advanced toroidal MFE reactor, namely a smaller and cheaper system obtained by introducing modest advanced features to make the tokamak even more attractive as a fusion reactor concept.

Capability for Long Pulse Advanced Tokamak Experiments in FIRE

The development, exploration and detailed understanding of high-confinement, high-fusion power-density and steady-state (high-duty-cycle) plasmas are needed to provide the basis for economically attractive applications of fusion power. FIRE has significant capability to address the “steady-state” advanced toroidal configuration initiative of the Modular Strategy using non-burning deuterium plasmas.

The issues to be addressed include:

1. Optimization of confinement and β using current and pressure profile control
2. Integration of high performance plasma with long pulse particle and power exhaust
3. Development of controls and techniques to avoid or mitigate the effects of disruptions

The objective of FIRE would be to extend these studies beyond the plasma performance and duration accessible in present tokamaks to values closer to those for a fusion plasma. The physics of a fusion plasma is characterized by the dimensionless parameters, ρ^* (normalized gyro-radius), ν^* (normalized collision frequency) and β . Existing tokamaks are able to replicate the ν^* and β for a fusion reactor plasma but not simultaneously ρ^* , which requires a plasma with a larger Ba . The important time scale for exploring advanced toroidal physics is τ_{cr} , the time for the plasma current profile to redistribute after a disturbance. The current redistribution time is often called the plasma current skin time. A plasma duration of $\sim 3 \tau_{\text{cr}}$ would be sufficient to allow the current profile to relax to within

5% of the steady-state current profile, and would be sufficiently long to address long pulse advanced tokamak physics.

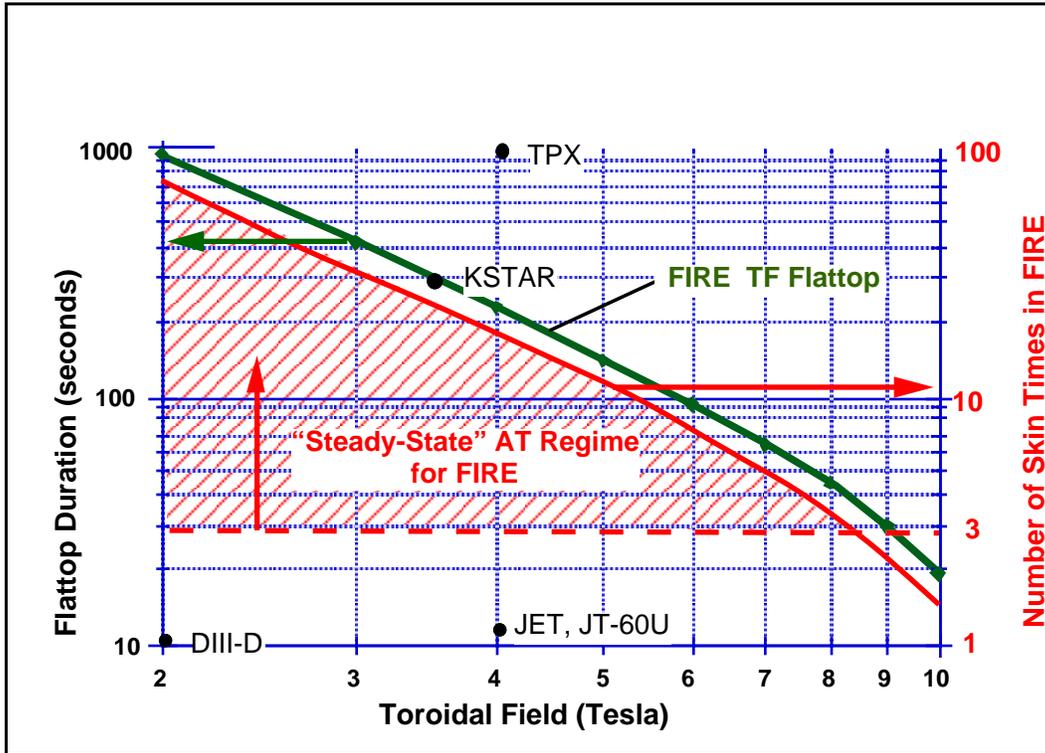


Fig. 6. Capability of the FIRE toroidal field system for long-pulse experiments.

The flattop of the magnetic field in FIRE increases rapidly as the magnetic field is reduced as shown in Fig. 6. In FIRE, the skin time is typically ~ 13 s at $Q \sim 10$ parameters due to the small minor radius, so pulses ~ 40 s would allow the plasma current profile to approach within 5% of its equilibrium value. FIRE operated at 8T would be able to extend the range of long-pulse advanced tokamak physics studies a factor of two in ρ^* beyond the capability of any existing shaped divertor tokamak or any under construction for “long-pulse” durations $\geq 3 \tau_{cr}$. The addition of lower hybrid in a later upgrade phase would be suitable for current drive to sustain the long pulse plasmas in FIRE. This capability would be within a factor of two of ρ^* in ARIES-RS.

Table III. Comparison of Long Pulse Advanced Tokamak Experiments. ($\beta/v^* = \text{constant}$)

	DIII-D	JET	KSTAR	TPX	FIRE	ITER-RC	ARIES-RS
B(T)	2.2	2	3.5	4	8	5.5	8
$N\rho^\dagger = 1/\rho^*$	0.25	0.27	0.25	0.3	0.45	1.05	1.0
Duration/ τ_{cr}	1.7	4	7-100	>100	4	~ 16	∞

\dagger normalized to $1/\rho^*$ for ARIES-RS, ITER-RC pulse length 3,600 s in driven $Q = 5$ regime.

Integration of Long-Pulse Advanced Tokamak Physics and Alpha Dominated Burning Plasmas, the critical issue for Advanced Toroidal Configurations, can be explored on FIRE.

It is anticipated that over the next ten years the ongoing world-wide advanced tokamak program (total funding $\sim \$1.2$ B) will develop the advanced tokamak understanding and techniques to improve confinement (e.g., H98) by 20% and β_N by at least 50%. An

experiment, such as FIRE, could then exploit these techniques to extend the range of burning plasma experiments and begin to address the critical issue of integrating of advanced tokamak physics with alpha dominated plasmas.

Fusion Technology Experience from FIRE

FIRE would also make significant contributions to the Fusion Technology and Materials Initiative of the Modular Strategy. FIRE will produce reactor-like fusion power density and neutron wall loading, but neither FIRE nor ITER-RC would produce the neutron fluence needed to provide data on neutron damage to structural materials (Table IV). Nonetheless, some information could be obtained from tests involving blanket modules.

Table IV. Fusion neutron parameters for Next Step Options compared to a reactor.

	FIRE	ITER-RC	ARIES-RS
Fusion Power Density (MWm^{-3})	10	0.5	6
Neutron Wall Loading (MWm^{-2})	3	0.6	4
Neutron Fluence (MW y m^{-2}), lifetime	< 0.01	~1	120

The lifetime neutron production in FIRE will be limited to 5 TJ ($3 \times 10^{-3} \text{ MW-y m}^{-2}$) to reduce damage to insulators in the toroidal field coil. Consideration will also be given to the use of low activation materials in various components to gain experience for the follow-on Advanced Fusion Integration Facility in the Modular Strategy. Remote handling will be implemented to maintain and replace components inside the vacuum vessel. Shielding inside the double walled vacuum vessel would allow hands-on work in the region outside the TF magnets.

High speed tritium pellet injectors with vertical injection paths inside the magnetic axis and lower speed pellets guided toward the inboard mid-plane will be implemented to improve plasma performance and to reduce tritium inventory. FIRE will also develop and test materials for plasma facing components (W and Be) that are compatible with the fusion reactor requirement of low tritium retention. A fast low inventory tritium re-circulating system will be developed to minimize on-site tritium inventory.

The combination of high magnetic field and advanced tokamak plasma regimes could lead to very attractive fusion reactor concept with high fusion power density. This emphasizes the importance of developing the full capability of high temperature superconductors with high critical fields and high strength structural materials for fusion applications.

Status of FIRE Interim Engineering Study

Detailed 3-D stress analyses have been carried out including the effects of electromagnetic loads, and diffusion of the current and temperature in the presence of nuclear heating. The TF copper stress is $\leq 76\%$ of the allowable stress and the temperature rise is within design allowables. The TF insulation shear stress is within allowables. A design configuration with a toroidal field flattop ≈ 18.5 s at 10 T or 12 s at 12 T has been developed.

The poloidal coils consist of a segmented OH solenoid with BeCu conductor and shaping coils using OFHC conductor. The poloidal coil stresses and temperatures are within the design allowables. The OH solenoid coil stress is only $\sim 40\%$ of the design allowable for BeCu. Higher conductivity copper alloys, with lower strength and cost, are being evaluated for the OH solenoid. The vacuum vessel is a double wall stainless steel vessel similar to that in the TPX and ITER designs. The inter space of the double wall will be

filled with shielding material to reduce the neutron activation outside the toroidal coil envelope, thereby allowing hands-on maintenance in the region outside the TF coils.

The plasma facing components (PFC) must withstand very high power densities while minimizing tritium retention. For the interim design, carbon is excluded as a PFC material due to the high retention of tritium experienced in TFTR and JET. While schemes might be developed to mitigate the carbon tritium retention issue in FIRE, the mission of FIRE is to develop a material that would also be compatible with the requirements of a high duty cycle reactor. The leading candidate for the first wall material is Be with inertially cooled tiles in the main chamber and Be coating on copper backing plates for stabilizing plates. The power density on the outer divertor plate without peaking factors or the effects of elms is estimated to be $\sim 25 \text{ MWm}^{-2}$ without a detached or radiative divertor. Tungsten rods mounted on Cu backing plates capable of withstanding 25 MWm^{-2} have been developed for ITER and are the leading candidate for the FIRE divertor plates. The outer divertor plates will be actively cooled during the pulse while the inner plates are cooled between pulses. Plasma modeling is underway to ensure detached or radiative divertor operation so that there will be some margin to accommodate the effects on peaking, elms and disruptions. The engineering analyses of FIRE are evolving rapidly. The most up comprehensive information can be found at <http://fire.pppl.gov>.

Cost and Schedule Considerations for a Next Step Burning Plasma Experiment.

Cost estimates have not been done for FIRE except to note comparisons with comparably sized devices, CIT (R = 2.14m, 11T) and BPX-AT (R = 2.0m, 10T), which had costs estimated to be in the range of \$700M for experiments located at the TFTR site with about \$200M of site credits. Some of the physical parameters that drive the costs are toroidal field magnet energy, plasma volume and plasma surface area are compared for an existing large tokamak and for potential Next Step Options in the following Table V.

Table V. Comparison of some important cost drivers for burning plasma devices.

	JET	IGNITOR	FIRE	CIT	BPX	ITER-RC	ITER-EDA
TF Coil Technology	H ₂ O Cu	30 °K Cu	LN BeCu	LN BeCu	LN BeCu	Nb ₃ Sn	Nb ₃ Sn
TF Magnet Energy (GJ)	1.6	4	4	8	8	41	100
Plasma Volume (m ³)	85	11	18	35	65	740	2000
Plasma Surface (m ²)	147	36	60	85	130	640	1200
Cost Range (\$B)	~0.5 FY84	~0.5	<1	~0.6 FY89	~1.5 FY92	~5	~10

The schedule to attain an MFE burning plasma test bed is an important consideration in the strategy and planning of the MFE program. Plans for the ITER-EDA required 15 years after the initiation of construction before D-T operation would be initiated; a 12 year construction period followed by three years of hydrogen and deuterium operation before D-T experiments. A similar time period would be required for ITER-RC. If ITER-RC construction were initiated in 2002, then D-T operation would begin ~ 2017 . A small compact high field tokamak like IGNITOR or FIRE is expected to have a construction period of ~ 7 years followed by 3 years of hydrogen and deuterium operation based on previous schedule estimates for CIT and BPX. If construction were initiated on IGNITOR or FIRE in 2002, then D-T operation could begin in ~ 2012 , which is ~ 5 years later than the initiation of similar inertial fusion burning plasma experiments using NIF.

Siting Considerations for a Next Step Burning Plasma Option

The siting requirements for a FIRE/IGNITOR class device is much reduced relative to that required for an ITER class device, thereby significantly reducing the time and cost. The lowest cost Next Step Option of the FIRE/IGNITOR class would be to utilize an existing site such as TFTR or JET. However, these sites might limit later upgrades, and might preclude a natural progression of follow-on devices. Consideration should be given to the possibility of a unified site for the development of fusion which would support not only the development of tokamak burning plasma experiments, but tests of burning plasmas in other magnetic configurations as well as providing an infrastructure for plasma based fusion technology facilities.

The Modular Pathway for Magnetic Fusion Energy

The Next Steps in the Modular Strategy beyond the existing programs and facilities could include a compact high field tokamak(s) of the IGNITOR/FIRE class, a superconducting high performance advanced tokamak of the JT-60SU class and specialized fusion technology facilities to address the first wall problem for MFE. The fusion technology facilities might include intense neutron sources for materials damage studies and facilities to investigate the viability of renewable first wall concepts such as liquid surfaces facing the plasma. These facilities would feed into an Assessment of Magnetic Fusion milestone in ~ 2015, which if successful would lead to the construction of an Advanced Fusion Integration Facility with characteristics similar to those of an attractive MFE reactor. In this scenario a commercial fusion power plant could be operating midway through the 21st century. A more detailed description of the Modular Strategy can be found on the World Wide Web at <<http://nso.ucsd.edu/chapter3.pdf>>.

High Leverage Activities and Issues

The initial FIRE studies have shown that the power handling capability of the divertor and first wall limit the pulse length in FIRE. Continued 3-D modeling of power and particle handling with experimental benchmarks will be essential in defining the divertor design. Engineering studies are needed to develop a vacuum vessel design capable of handling reactor level neutron power densities. These are generic fusion issues that can be addressed on FIRE. Experimental and theoretical studies to clarify the scaling of the L to H-mode power threshold and the H to L mode power threshold for plasmas significantly below the Greenwald density would be important in optimizing the design for both standard regimes as well as advanced reverse shear regimes. Much more work is needed to develop self-consistent advanced tokamak modes of operation and to evaluate stability to alpha driven instabilities in advanced tokamak configurations. More comprehensive 1 1/2-D simulations of standard and advanced regimes including burn control techniques are needed.

Summary

Exploration, understanding and optimization of alpha-dominated plasmas is a critical issue for all approaches to fusion. The tokamak is the most cost-effective vehicle to investigate alpha-dominated plasma physics, and its coupling to advanced toroidal physics for MFE. The performance of a burning plasma depends sensitively on the details of confinement, β -limits, density limits and edge plasma conditions. This uncertainty can only be reduced by studying actual alpha-dominated plasmas in the laboratory in conjunction with other advanced toroidal experiments and improved numerical simulations. The compact high field tokamak offers the possibility of addressing the important alpha-dominated plasma issues, many of the long pulse advanced tokamak issues and beginning the integration of alpha-dominated plasmas with advanced toroidal physics in a ~\$1B class facility.

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Appendix 1. Basic Parameters and Features of FIRE

R, major radius	2.0 m
a, minor radius	0.525 m
κ_{95} , plasma elongation at 95% flux surface	~1.8
δ_{95} , plasma triangularity at 95% flux surface	~0.4
q_{95} , plasma safety factor at 95% flux surface	>3
Bt, toroidal magnetic field	10 T with 16 coils, < 0.4% ripple @ OuterMP
Toroidal magnet energy	3.7 GJ
Ip, plasma current	~6.5 MA
Magnetic field flat top, burn time	≥ 10 s (=18.5 s at 10 T, Pfusion ~ 200 MW)
Pulse Repetition time	2 hr
ICRF heating power, maximum	30 MW
Neutral beam heating	None
Lower Hybrid Current Drive	None in baseline, upgrade for AT
Plasma Fueling	Pellet injection (≥ 2.5 km/s vertical launch inside mag axis, possible guided slower speed pellets)
First wall materials	Be tiles, no carbon
First wall cooling	Inertial between pulses
Divertor configuration	Double null, fixed X point, detached mode
Divertor plate	W rods on Cu backing plate (ITER R&D)
Divertor plate cooling	Inner plate-inertial, outer plate active - water
Fusion Power	~200 MW
Fusion Power Density (plasma)	~10 MW m ⁻³
Neutron wall loading	~ 3 MW m ⁻²
Lifetime Fusion Production	5 TJ (BPX had 6.5 TJ)
Total pulses at full field/power	3,000 (same as BPX), 30,000 at 2/3 Bt and Ip
Tritium site inventory	< 30 g, Category III Low Hazard Facility

Possibility of upgrading to 12T and 7.7 MA with a 12 s flat top has been identified and is discussed in the FIRE Feasibility Report (<http://fire.pppl.gov>).